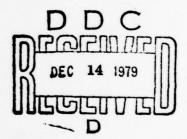


NAVAL POSTGRADUATE SCHOOL Monterey, California

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THESIS



WASTE HEAT RECOVERY UNIT DESIGN FOR GAS TURBINE PROPULSION SYSTEMS

by

Robert Meredith Combs

September 1979

Thesis Advisor:

P. F. Pucci

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Waste Heat Recovery Unit Design for Gas Turbine Propulsion Systems

by

Robert Meredith Combs
Lieutenant Commander, United States Navy
B.A., University of North Carolina, 1967
M.S., Naval Postgraduate School, 1973

Submitted in partial fulfillment of the requirements for the degree of

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from the

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Approved by:

Approved by:

Thesis Advisor

Second Reader

Chairman, Department of Mechanical Engineering

William M. Illa

Dean of Science and Engineering

ABSTRACT

A design model for a once-through waste heat recovery unit with a segmented fin-tube arrangement was developed along with a simple model of a combined gas and steam (COGAS) turbine propulsion system. These models were integrated and applied in a computer program written in FORTRAN IV for the IBM 360-67 computer. Waste heat recovery unit designs were produced and tested at off-design conditions. Using the space constraints and power requirements of a Navy destroyer-type ship, one design was selected and employed to make estimates of possible fuel savings to be realized through the application of a COGAS system.

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NOMENCLATURE

English Letter Symbols

A - Area (ft²)

Al - Estimated Area for Boiling in First Superheater
Pass (ft²)

A_b - Frontal Area Blocked by Tubes and Fins (ft²)

A_{ht} - Bare Tube Area (ft²)

A_f - Heat Exchanger Frontal Area (ft²)

A_{fin} - Fin Area (ft²)

A_{ff} - Cross-Sectional Area for Fluid Flow (ft²)

A^b
- Inside Area Required for Boiling in First
Superheater Pass (ft²)

Ash
i - Inside Area Required for Superheating in First
Superheater Pass (ft²)

A_{ip} - Inside Heat Transfer Area Per Pass (ft²)

A_{min} - Minimum Cross-Sectional Area for Gas Flow (ft²)

A OD - Outside Heat Transfer Area Per Pass (ft²)

A_{ti} - Total Heat Exchanger Inside Area (ft²)

A_{to} - Total Heat Exchanger Outside Area (ft²)

C - Constant

C_{bhp} - Correction Factor to Gas Turbine BHP for Duct Loss

C_{max} - Maximum Heat Capacity (Btu/hr-F)

C_{min} - Minimum Heat Capacity (Btu/hr-F)

C_{pf} - Specific Heat of Water/Steam (Btu/lbm-F)

C_{pg} - Specific Heat of Gas (Btu/lbm-F)

C_{sfc} - Correction Factor to Gas Turbine BHP for Duct Loss

```
Fin Outside Diameter (ft)
df
dfh
             Diameter of Fin Base (ft)
             Inside Tube Diameter (ft)
d<sub>i</sub>
do
             Outside Tube Diameter (ft)
             Fin Root Diameter (ft)
d_r
f
             Friction Factor
             Gas Flow Rate Per Square Foot (lbm/hr-ft2)
G
             Maximum Gas Flow Rate Per Square Foot (lbm/hr-ft2)
G_{\text{max}}
             Enthalpy of Steam at Turbine Inlet (Btu/lbm)
h<sub>1</sub>
             Turbine Exhaust Steam Enthalpy (Btu/lbm)
h<sub>2</sub>
             Turbine Exhaust Steam Enthalpy Assuming Isen-
h<sub>2s</sub>
             tropic Expansion (Btu/lbm)
             Enthalpy of Saturated Water (Btu/lbm)
hf
             Enthalpy of Water at Heat Exchanger Inlet (Btu/lbm)
hfl
             Enthalpy of Water at Heating Section Outlet
h<sub>f2</sub>
             (Btu/lbm)
             Enthalpy of Steam at Boiling Section Outlet
h<sub>f3</sub>
             (Btu/lbm)
             Enthalpy of Steam at Superheater Outlet (Btu/lbm)
h<sub>f4</sub>
             Enthalpy Increment for Boiling (Btu/lbm)
hfa
             Enthalpy of Heat Exchanger Feedwater (Btu/lbm)
hfw
             Heat Exchanger Inside Heat Transfer Coefficient
he
             in Heating or Superheating Section (Btu/hr-ft2-F)
htpf
             Heat Exchanger Inside Heat Transer Coefficient
             in the Two-Phase Region (Btu/hr-ft2-F)
j
             Heat Transfer Colburn j-factor
             Thermal Conductivity of Gas (Btu-hr-ft-F)
kg
             Thermal Conductivity of Steam/Water (Btu/hr-ft-F)
k,
```

Thermal Conductivity of Heat Exchanger Tube kw Wall (Btu/hr-ft-F) L - Fin Height (ft) Length of Cut from Fin Tip (ft) Tube Length (ft) L - Steam/Water Flow Rate (lbm/hr) mf - Gas Flow Rate (lbm/hr) m_a - Gas Flow Rate in Boiling Section of First Superheater Pass (lbm/hr) Gas Flow Rate in Superheating Section of First Superheater Pass (1bm/hr) Number of Passes n - Number of Transfer Units N, NTU - Number of Fins Per Inch Nf Number of Segments in One Fin N - Number of Tubes Per Row N_{t/r} P - Pressure (psia) - Steam Pressure at Steam Turbine Inlet (psia) Pı Steam/Water Pressure in Heat Exchanger (psia) Pf - Gas Turbine Horsepower Pat Steam Turbine Horsepower Pst Ptot Total System Horsepower - Heat Transfer Rate (Btu/hr) Q - Heat Transfer Rate in Boiling Section (Btu/hr) Q_b Heat Transfer Rate in Heating Section (Btu/hr) $Q_{\mathbf{h}}$ Heat Transfer in a Heat Exchanger Pass (Btu/hr)

Qsh

Heat Transfer Rate in Superheating Section (Btu/hr)

```
Qrb
             Required Heat Transfer Rate in Boiling Section
             of First Superheater Pass (Btu/hr)
             Heat Flux (Btu/hr-ft2)
q"
             Thermal Resistance (hr-ft<sup>2</sup>-F/Btu)
Rth
             Heat Exchanger Outside Resistance (hr-ft<sup>2</sup>-F/Btu)
R
             Entropy (Btu/lbm-F)
S
             Entropy of Steam at Turbine Inlet (Btu/lbm-F)
Sı
             Entropy of Saturated Water (Btu/lbm-F)
Sf
             Entropy Increment for Evaporation (Btu/lbm-F)
Sfa
             Tube Spacing Normal to Gas Flow (ft)
Sn
Sp
             Tube Spacing Parallel to Gas Flow (ft)
             Steam Temperature at Turbine Inlet (F)
T,
             Steam/Water Bulk Temperature (F)
Tfb
             Water Temperature at Heat Exchanger Inlet (F)
Tfl
             Water Temperature at Heating Section Outlet (F)
T<sub>f2</sub>
             Steam Temperature at Boiling Section Outlet (F)
T<sub>f3</sub>
             Steam Temperature at Superheating Section
T<sub>f4</sub>
             Outlet (F)
             Fin Thickness (ft)
tf
T<sub>g1</sub>
             Average Gas Temperature at Heat Exchanger Inlet (F)
T<sub>g2</sub>
             Average Gas Temperature at Boiling Section
             Inlet (F)
             Average Gas Temperature at Heating Section
T<sub>q3</sub>
             Inlet (F)
             Average Gas Temperature at Heat Exchanger
Tq4
             Outlet (F)
             Gas Bulk Temperature (F)
Tab
```

T_{qf} - Gas Side Film Temperature (F)

T - Temperature of Saturated Water (F)

T - Average Outside Tube Wall Temperature (F)

U - Overall Heat Transfer Coefficient (Btu/hr-ft²-F)

w_s - Fin Segment Width (ft)

W₊ - Steam Turbine Work (Btu/lbm)

W_{ts} - Isentropic Steam Turbine Work (Btu/lbm)

x - Steam Quality

x_a - Average Steam Quality

x₂ - Turbine Exhaust Steam Quality

x_{2s} - Turbine Exhaust Steam Quality Assuming Isentropic Expansion

Dimensionless Groups

N, - Nusselt Number

Pr - Prandtl Number

R - Reynolds Number

S₊ - Stanton Number

Greek Letter Symbols

ΔP - Pressure Change (psia)

ΔT - Temperature Change (F)

ε - Effectiveness

ε_b - Effectiveness of Boiling Section of First Superheater Pass

 ϵ_{oa} - Effectiveness Overall for a Heat Exchanger Section

 $\epsilon_{\rm p}$ - Effectiveness for a Heat Exchanger Pass

μ_b - Viscosity at Bulk Temperature (lbm/ft-hr)

```
μ<sub>w</sub> - Viscosity at Tube Wall Temperature (lbm/ft-hr)
η<sub>f</sub> - Fin Efficiency
η<sub>th</sub> - System Thermal Efficiency
η<sub>st</sub> - Steam Turbine Efficiency
ρ - Density (lbm/ft<sup>3</sup>)
ρ<sub>ℓ</sub> - Density of Saturated Water (lbm/ft<sup>3</sup>)
ρ<sub>ν</sub> - Density of Saturated Vapor (lbm/ft<sup>3</sup>)
```

I. INTRODUCTION

A. BACKGROUND

The U. S. Navy has made a commitment to gas turbine propulsion systems, with two classes of gas turbine ships entering the fleet (DD-963 and FFG-7) and one class proposed (DDG-47) at the time of this writing. The DD-963 class has two shafts with two General Electric LM 2500 gas turbines powering each shaft. The FFG-7 class is a single-shaft ship with two LM 2500 gas turbines. The DDG-47 class propulsion plant, as proposed, will be similar to that of the DD-963 class.

Currently, means for conserving fuel are being sought in all sectors of the economy and government. In most of our steam turbine-powered ships fuel conservation must be pursued largely through operating practices such as reduced steaming time or reduced speed when steaming. Several alternatives exist, however, for fuel consumption reduction for the gas turbine propulsion system. These alternatives involve combining another type of propulsion system with the gas turbine in order to reduce the overall fuel consumption by either operating the combined systems in parallel or by operating the less expensive system in the cruise mode. Some examples of these combinations are:

Gas Turbine and Diesel (CODOG, GODAG)

Gas Turbine and Steam (COGAS) (steam system not separately fired)

Gas Turbine and Steam (COSAG) (steam system separately fired)

The COmbined Gas turbine And Steam turbine (COGAS) system is probably the best of these alternatives with respect to fuel consumption, initial cost, maintenance, and manning requirements.

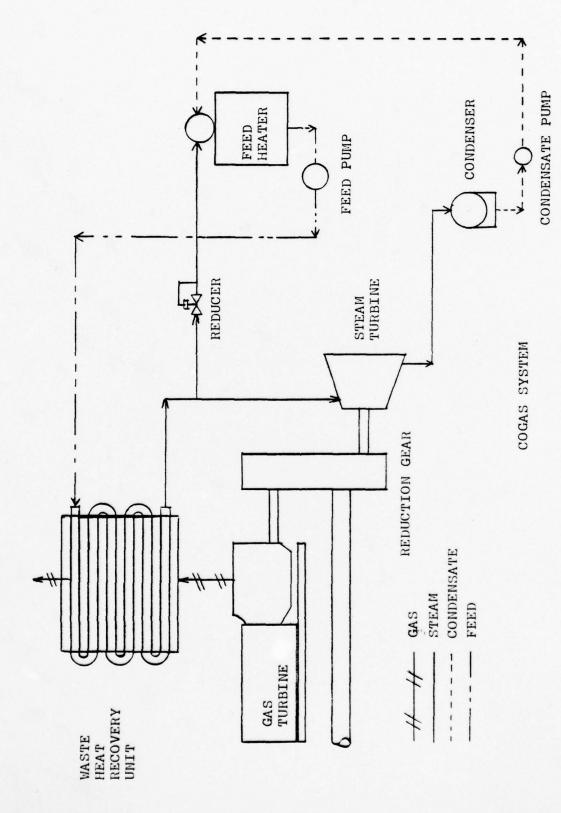
The COGAS ship propulsion plant uses the exhaust heat from a gas turbine to generate steam in a waste heat recovery unit (WHRU). This steam is used to drive a steam turbine which is operated in parallel with the gas turbine, for ship propulsion. A common reduction gear connects both turbines to the propeller shaft. Figure 1 illustrates the COGAS system.

Several studies have examined the potential of the COGAS system for improving propulsion plant fuel efficiency.

Giblon and Rolih [Ref. 1] studied the commercial ship application of COGAS. References 2 and 3 investigated the feasibility of the COGAS system for military ship application.

In all three studies the COGAS system was designed around a gas turbine brake horsepower of about 23,000. Additionally, all three employed a drum-type boiler as the waste heat recovery unit.

In this study, COGAS system designs were considered for a destroyer-sized ship with two shafts and two LM-2500 gas turbines for each shaft. One gas turbine was equipped with a WHRU. In the COGAS mode of operation the WHRU-equipped gas turbine was operated in parallel with the steam turbine,



The same of the same

FIGURE 1

powering one shaft. The other shaft was allowed to drag. It was assumed that the principal employment of the COGAS system would be for "cruise" conditions. That is, the COGAS system would be operated primarily for steady steaming. The horsepower range over which the COGAS system could be operated is, theoretically, limited only to the range of powers over which the gas turbine can be operated. Thus, the power range would vary from the COGAS system power output with the gas turbine at idle to the system power output attained with the gas turbine operating at its maximum continuous power rating.

When the COGAS system operating range is selected, the desired goal of fuel conservation must be balanced against system reliability and routine maintenance requirements. If only one gas turbine is equipped for COGAS operations, the system downtime will increase as the turbine is operated at higher power settings. In order to increase the time between major gas turbine maintenance requirements, two COGAS systems could be installed in a twin-shaft ship. The increased overall reliability which this redundancy would afford, however, would be at least partially offset by the higher initial cost, the increased manning requirements, and the added weight of two systems.

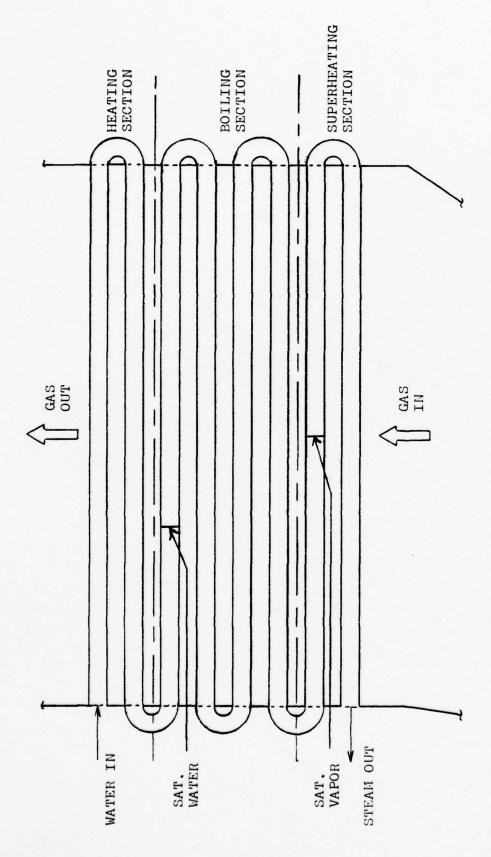
A once-through counter-cross-flow heat exchanger was selected as the WHRU. Reference 6 states some of the principal advantages of the once-through steam generator over the drum-type boiler. These advantages are as follows:

lower initial cost, faster response, more compactness, and lower operating cost. Additionally, the once-through unit provides a somewhat simpler model than the drum-type heat exchanger. A schematic representation of a once-through WHRU installed in the exhaust ducting of a gas turbine is shown in figure 2.

B. OBJECTIVES

There were five main objectives for this thesis.

- 1. Develop a design model for the once-through WHRU. This model was to size a WHRU and predict is performance given initial conditions such as feedwater inlet temperature, steam outlet temperature, WHRU operating pressure, inlet and outlet gas conditions, and gas flow rate.
- Consider several sets of initial conditions and design constraints (e.g., maximum frontal dimensions) and produce WHRU designs for each set.
- 3. Evaluate these designs and integrate them with a simple COGAS system model in order to test the design model and to develop a clearer understanding of the WHRU performance in the COGAS system.
- 4. From the evaluated designs, predict the performance of the COGAS system.
- 5. Provide a framework for future studies involving a detailed, complete COGAS system cycle analysis and optimization.



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ONCE-THROUGH WASTE HEAT RECOVERY UNIT

FIGURE 2

II. MODEL DESCRIPTION

A. OVERVIEW AND INITIAL CALCULATIONS

The waste heat recovery unit (WHRU) is modeled as a once-through counter-cross-flow heat exchanger. The model is applied in a computer program for use in heat exchanger design for a combined gas and steam (COGAS) turbine propulsion plant system. The same model could be adapted for use in a complete cycle analysis of the COGAS system.

The WHRU model is divided into three principal sections: heating, boiling and superheating. The specified initial conditions for the model are: (1) gas temperature into the heat exchanger (T_{g1}) , (2) minimum average gas exit temperature from the heat exchanger (T_{g4}) , (3) gas flow rate (\mathring{m}_{g}) , (4) water inlet temperature (T_{f1}) , (5) water/ steam pressure (P_{f}) . Useful background material for the model formulation was obtained from references 1-5.

Two simplifications should be noted at this point. First, the water-side pressure drop in the WHRU is neglected. Second, gas temperatures, evaluated at several points in the model, are average temperatures. Specifically, the average inlet and outlet gas temperatures for the heating and superheating sections and the average inlet and outlet gas temperatures for each pass in the boiling section are evaluated. In each of these calculations the gas temperature distribution is neglected. Clearly, even if the gas

turbine exhaust flow is uniform in temperature as it approaches the WHRU, the gas temperature will not be uniform after the first WHRU pass is encountered. Due to the varying gas-to-fluid temperature difference across each pass the gas temperature will be distributed non-uniformly after the first WHRU pass. One can, however, calculate the average gas temperature approaching a particular pass based on the heat release from the gas in the previous pass and the average gas temperature entering the previous pass. Averaged gas temperatures calculated in this manner are used throughout the model.

Prior to the heating section, some initial calculations are performed to determine the water/steam mass flow rate and to set the pinch point. In order to calculate the water/steam mass flow rate an energy balance is performed, using the starting conditions, as follows:

$$Q = \dot{m}_{q} C_{pq} (T_{q1} - T_{q4})$$

where C_{pg} is evaluated at the average gas temperature $T_{gavg} = (T_{g1} + T_{g4})/2$. The fluid mass flow rate is calculated from

$$\hat{m}_{f} = \frac{Q}{h_{f4} - h_{f1}}$$

where h_{f1} and h_{f4} are inlet and outlet fluid enthalpy

respectively. Intermediate fluid and gas temperatures are calculated as follows:

1. The heating section is assumed to heat the water from inlet conditions to the saturation temperature, T_{f2} . A heat balance is performed on the water side yielding a heating section heat transfer of

$$Q_h = \hat{m}_f (h_{f2} - h_{f1}).$$

The required average gas temperature entering the heating section is then calculated from

$$T_{g3} = T_{g4} + \frac{Q_h}{\dot{m}_g C_{pg}}$$
.

2. In the boiling section it is assumed that sufficient heat is added to produce saturated vapor at the outlet. An energy balance on the steam-side provides the total heat transfer in the boiling section,

$$Q_b = \dot{m}_f (h_{f3} - h_{f2})$$

where $h_{\mbox{\scriptsize f3}}$ is the enthalpy of saturated vapor at the pressure specified. The required average gas temperature entering the boiling section is

$$T_{g2} = T_{g3} + \frac{Q_b}{\dot{m}_g C_{pg}}$$
.

3. In the superheating section, the steam temperature is raised from the saturation temperature to the outlet temperature specified in the initial conditions. The heat transfer in the superheating sections is

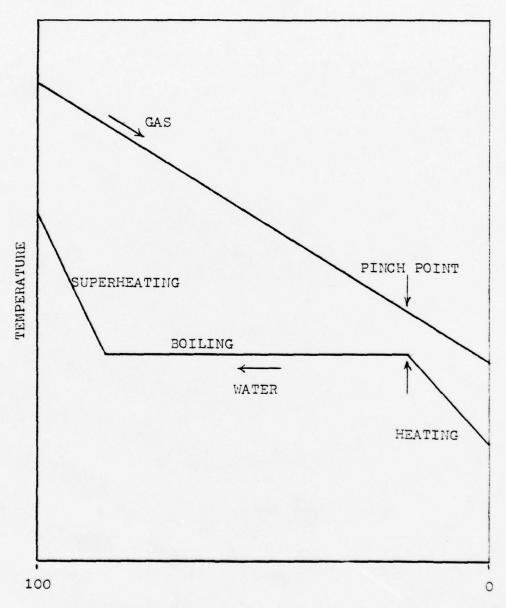
$$Q_{sh} = \dot{m}_f (h_{f4} - h_{f3})$$

where h_{f4} is the enthalpy of steam corresponding to the steam outlet temperature T_{f4} . The gas inlet temperature T_{g1} is known from the initial conditions.

The "pinch point", for the purposes of this model, is defined as the difference between the gas temperature entering the heating section and the water temperature leaving the heating section (saturation temperature). This temperature difference will normally correspond to the smallest temperature difference between gas and fluid in the heat exchanger. The only other likely location for the smallest temperature difference between gas and fluid is at the gas inlet, or superheater outlet. Figure 3 depicts the typical gas and fluid temperature distribution in the WHRU.

The model must provide some internal control over the pinch point temperature difference as defined above. This is desirable because the gas-fluid temperature difference at the fluid saturation point is indicative of the amount of heat transfer area which will be necessary to heat the incoming water to the saturation point. As the temperature

TYPICAL WHRU GAS-FLUID TEMPERATURE DISTRIBUTION



PERCENT OF TOTAL WHRU LENGTH

FIGURE 3

difference at the pinch point increases the heating portion of the heat exchanger becomes more efficient from the point of view of heat transfer area required. The minimum pinch point temperature difference is set at 25 F. After the interim temperatures are established the pinch point temperature difference is checked. If the difference is less than 25 F, the gas temperature at the heating section inlet is reset to

$$T_{q3} = T_{f2} + 25.$$

From the overall energy balance

$$C_{pg} \dot{m}_{g} (T_{g1} - T_{g4}) = \dot{m}_{f} (h_{f4} - h_{f1})$$

and the energy balance across the heating section

$$C_{pq} \dot{m}_{q} (T_{q3} - T_{q4}) = \dot{m}_{f} (h_{f2} - h_{f1}),$$

a revised gas outlet temperature may now be calculated from

$$T_{g4} = \frac{T_{g3} - \alpha T_{g1}}{1 - \alpha}$$

where

$$\alpha = \frac{h_{f2} - h_{f1}}{h_{f4} - h_{f1}}.$$

After this new gas inlet temperature is established, all initial calculations are performed again, to establish a new water/steam mass flow rate and to recheck the pinch point temperature difference. Once these calculations are complete, the geometric parameters for the heat exchanger must be specified.

B. GEOMETRY

A fin-tube with helically curved extended surfaces on circular tubes is assumed for this model. The fins are segmented. The tubes are configured in banks of one row each and the rows are staggered. The base tube surface is taken from Ref. 7. The description of the finned tubes is as follows.

 d_i = tube inside diameter = 1.86 in.

d_o = tube outside diameter = 2.00 in.

 d_r = fin root diameter = 2.00 in.

 N_f = fins per inch = 5.94

 ℓ = fin height = 1.015 in.

 $\ell_{\rm C}$ = length of cut from fin tip = 0.82 in.

 d_f = fin outside diameter = 4.03 in.

 t_f = fin thickness = 0.048 in.

 w_{c} = fin segment width = 0.17 in.

 $\rm N_{_{\rm S}}$ = number of segments in 360 degrees = 38 The finned tube configuration is shown in figure 4. The tube length, L, and number of tubes per row $\rm N_{_{\rm t/r}}$ are chosen by the designer according to the frontal area, $\rm A_{_{\rm f}}$,

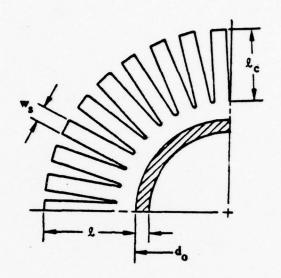


Figure 4: Segmented Fin-Tube Configuration

desired. The tube layout is shown below in figure 5. The center-to-center tube spacing in the transverse direction is 4.50 inches. The equilateral, staggered tube arrangement used in this model leads to a spacing normal to the gas flow, $S_{\rm n}$, of 4.50 inches and a spacing parallel to the gas flow, $S_{\rm p}$, of 3.90 inches as shown in figure 5. The heat exchanger height is established by the number of WHRU passes (rows) and the tube spacing parallel to the gas flow $(S_{\rm p})$.

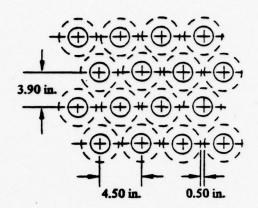


Figure 5: Model Tube Layout

In order to establish the minimum gas flow cross-sectional area the total "blocked" frontal area, $\mathbf{A}_{\mathbf{b}}$, of the heat exchanger must be calculated from

$$A_b = N_{t/r} L d_o + L N_f L N_{t/r} l t_f$$

and the minimum gas flow area is

$$A_{\min} = A_f - A_b$$

The total inside area available for heat transfer per pass is

$$A_{ip} = \pi d_i L N_{t/r}$$
.

The gas side surface area available per pass for heat transfer is the sum of the fin surface area and the bare tube surface area per pass. The fin surface area per tube is calculated from

$$A_{fin} = N_{f} L[N_{s}(2 \ell_{c} w_{s} + 2 t_{f} \ell_{c} + w_{s} t_{f}) - \frac{\pi}{2}(d_{fb}^{2} - d_{o}^{2})]$$

where $d_{fb} = d_f - 2 l_c$. The bare tube area per tube is

$$A_{bt} = \pi d_o L - \pi d_o t_f N_f L$$
.

Therefore, the total outside area per pass available for heat transfer is

$$A_{op} = N_{t/p} (A_{fin} + A_{bt})$$
.

The cross-sectional area for fluid flow is calculated from

$$A_{ff} = \frac{\pi}{4} d_i^2 N_{t/p}.$$

With the mass flow rates, terminal temperatures and heat exchanger geometry established, the remainder of the model may be solved for number of passes, actual interim temperatures, location of the fluid phase changes, and the gas side pressure drop.

C. HEATING SECTION

The gas-side Reynolds number for the heating section is calculated initially using the gas bulk temperature to find the gas properties. With this Reynolds number, a j-factor and a friction factor, f, are obtained from polynomials fit to the data for tube layout number 5 in Ref. 7 (fig. 5). The friction factor will be used later to calculate the gas side pressure drop in the heating section. The j-factor is related to the heat transfer coefficient h_g by the following relationship.

$$j = s_t P_r^{2/3}$$

By introducing

$$s_t = \frac{N_u}{R_e P_r}$$

the previous expression can be written as

$$j = \frac{N_u}{R_{eg} P_{rg}} P_r^{2/3} = \frac{N_u}{R_{eg} P_{rg}^{1/3}}$$

and

$$N_{u} = j R_{eq} P_{rq}^{1/3} ,$$

where

$$N_{u} = \frac{h_{g} d_{o}}{K_{g}}.$$

Therefore, a relationship may be written for the heat transfer coefficient as follows:

$$h_g = j \frac{K_g}{d_0} R_{eg} P_{rg}^{1/3}$$
.

The water-side heat transfer coefficient is calculated by using the Dittus-Boelter correlation

$$h_f = 0.023 \frac{K_f}{d_i} R_{ef}^{0.8} P_{rf}^{0.4}$$

where all properties are obtained at the bulk temperature of the water in the heating section. Using the tube wall resistance together with h_g and h_f , the overall heat transfer coefficient for the heating section may be written in terms of the inside area as

$$U_{oi} = \frac{\frac{1}{\frac{1}{b_{f}} + \frac{A_{ip} \ln(d_{o}/d_{i})}{2 \pi K_{w} N_{t/p} L} + \frac{A_{ip}}{A_{op}} \frac{1}{n_{t} n_{g}}}$$

where

$$\eta_{t} = 1 - (1 - \eta_{f}) \frac{A_{fin}}{A_{op}}.$$

The fin efficiency, n_{f} , is calculated from the expression

$$\eta_{f} = \frac{\tanh ML}{ML},$$

where

$$M = \sqrt{h_g P/KA}$$

and, if the fin is approximated by a set of rectangular strips extending from the tube wall, $L = \frac{d_f - d_o}{2}$. Now, the cross-sectional area, A, of a rectangular strip may be written as

$$A = w_s t_f$$

and the perimeter is

$$P = 2(w_s + t_f).$$

So, using known geometric parameters and the thermal conductivity of the fin metal, the parameter ML may be expressed as

$$ML = C \sqrt{h_g}$$

where

$$C = (\frac{d_{f} - d_{o}}{2}) \sqrt{\frac{2(w_{s} + t_{f})}{w_{s} t_{f} K}}$$
.

Now,

$$\eta_{t} = \left[1 - \left(1 - \frac{\tanh C \sqrt{h_{g}}}{C \sqrt{h_{g}}}\right) \frac{A_{fin}}{A_{op}}\right].$$

The number of passes required in the heating section is calculated, using the effectiveness-NTU method, in the following way.

 An average pass effectiveness for the heating section is calculated from the following expression for cross-flow effectiveness with both fluids unmixed obtained from Ref. 8,

$$\varepsilon_{p} = 1 - \exp\left[\frac{\exp(-NCn) - 1}{Cn}\right]$$

where

$$C = \frac{C_{\min}}{C_{\max}} = \frac{C_{pf} \stackrel{\text{in}}{=} f}{C_{pg} \stackrel{\text{in}}{=} g},$$

$$N = NTU = \frac{U_{oi} \stackrel{\text{A}}{=} ip}{C_{\min}},$$

$$n = N^{-0.22}.$$

Water and gas properties are taken at bulk temperatures.

An overall heating section effectiveness is calculated from

$$\varepsilon_{\text{oa}} = \frac{\left(\frac{1 - \varepsilon_{\text{p}} C_{\text{min}} / C_{\text{max}}}{1 - \varepsilon_{\text{p}}}\right)^{n} - 1}{\left(\frac{1 - \varepsilon_{\text{p}} C_{\text{min}} / C_{\text{max}}}{1 - \varepsilon_{\text{p}}}\right)^{n} - \frac{C_{\text{min}}}{C_{\text{max}}}}$$

where n = number of passes. This expression was obtained from Ref. 9. The overall effectiveness formulation was actually derived with the condition that fluids are mixed between passes. It can be shown [Ref. 9], however, that the error is not large when the expression is used for the case where fluids are unmixed between passes.

3. The expression for ε_{oa} is now used in an iterative fashion starting with n = number of passes = 1. Each time ε_{oa} is solved, the gas temperature into the heating section, T_{q3} , is found from

$$T_{g3} = \frac{\varepsilon_{oa} C_{min} T_{g1} - C_{max} T_{g4}}{\varepsilon_{oa} C_{min} - C_{max}}$$

which is derived from

$$\varepsilon_{\text{oa}} = \frac{C_{\text{max}}(T_{g_3} - T_{g_4})}{C_{\text{min}}(T_{g_3} - T_{f_1})}.$$

4. Once the inlet gas temperature is established for a particular number of passes, an energy balance may be

performed to solve for the total heat transfer which would take place in the heating section for that number of passes.

$$Q_{h} = \dot{m}_{g} C_{pg} (T_{g3} - T_{g4})$$

5. The enthalpy of the water at the outlet of the heating section for a particular iteration may be found from

$$h_{fL} = h_{f2} + \frac{Q_h}{\dot{m}_f},$$

and this yields the temperature of the water at the outlet, \mathbf{T}_{f2} , for the number of passes under consideration.

- 6. The outlet water temperature, T_{f2} , may be checked to see if it exceeds the saturation temperature.
- 7. This set of calculations is performed until T_{f2} exceeds the saturation temperature. This naturally means that boiling begins in the last pass of the current total number of passes. Initiation of boiling will be treated in the boiling section of the model. Therefore, the heating section ends with the pass prior to that which initiates boiling. The results of the above calculations are: (a) The total number of passes contained in the heating section, (b) the new gas temperature at the inlet to the heating section T_{g3} , and (c) the new water outlet temperature T_{f2} .

With these new heating section terminal temperatures an average outside wall temperature for the section may be calculated from

$$T_{wo} = T_{gb} - (\frac{U_{oi} A_{ti}}{h_{g} A_{to}}) (T_{gb} - T_{fb})$$

where A_{ti}/A_{to} are total inside/outside areas for the section and T_{gb}/T_{fb} are the new gas/fluid bulk temperatures for the section. The expression for T_{wo} is derived from the following formulation for heat transfer in the heating section,

$$Q = \frac{T_{gb} - T_{fb}}{\sum_{h} R_{th}} = \frac{T_{gb} - T_{wo}}{R_{o}}$$

which reduces to

$$T_{wo} = T_{gb} - \frac{R_o}{\sum R_{th}} (T_{gb} - T_{fb})$$

where

$$R_o = \frac{1}{\eta_t h_q A_{to}}$$

and

$$\sum R_{th} = \frac{1}{U_{oi}^{A}_{ti}}$$
.

The gas-side film temperature is

$$T_{gf} = \frac{T_{gb} - T_{wo}}{2}$$
.

This gas-side film temperature is now introduced at the beginning of the calculations for the heating section, to replace the gas bulk temperature. All calculations are performed again with \mathbf{T}_{cf} .

The gas-side pressure drop in the heating section may now be calculated using the previously obtained friction factor, f, from the correlation contained in Ref. 7. The gas-side pressure drop is

$$\Delta P_{g} = \frac{2f G_{\text{max}}^{2} N_{\text{t/r}} (\frac{\mu_{\text{w}}}{\mu_{\text{b}}})^{0.14}}{\rho}$$

where

$$G_{\max} = \frac{\dot{m}_g}{A_{\min}}$$

 $N_{t/r}$ = number of tubes per row

ρ = gas density

 $\mu_{\mathbf{w}}$ = gas viscosity at wall temperature

μ_b = gas viscosity at bulk temperature.

D. BOILING SECTION

The boiling section is solved pass-by-pass since most of the section will involve two-phase flow on the cold side and the inside heat transfer coefficient will change with quality, x, and heat flux, q". The correlation for the two-phase region inside heat transfer coefficient selected

for this model is that recommended by Tong [Ref. 10] for both nucleate boiling and forced convection. The equation for the two-phase flow heat transfer coefficient was given by Schrock and Grossman in Tong [Ref. 10] as

$$\frac{h_{TPf}}{h_{\ell}} = B\left[\frac{q''}{Gh_{fg}} + A\left(\frac{1}{X_{tt}}\right)^{n}\right].$$

The constants are given by Wright [Ref. 10]: $B = 6.70 \times 10^3$, $A = 3.5 \times 10^{-4}$, n = 0.66. The heat transfer coefficient assuming a total liquid flow is

$$h_{\ell} = 0.023 \frac{K_{\ell}}{d_{i}} \left[\frac{d_{i} G(1-x)}{\mu_{\ell}} \right]^{0.8} \left[\frac{C_{p\ell} \mu_{\ell}}{K_{\ell}} \right]^{0.1},$$

and the Martinelli parameter is

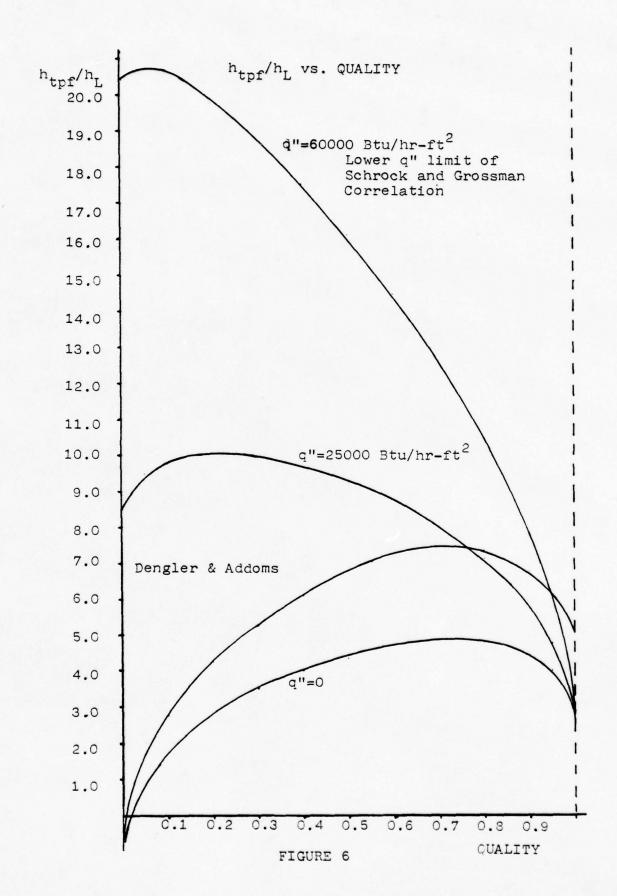
$$\frac{1}{x_{tt}} = \left[\frac{x}{1-x}\right]^{0.9} \left[\frac{\rho_{\ell}}{\rho_{v}}\right]^{0.5} \left[\frac{\mu_{v}}{\mu_{\ell}}\right]^{0.1}.$$

The limits of the data for this correlation are

quality:
$$0.05 - 0.57$$

heat flux: $6.0 \times 10^4 - 1.45 \times 10^6$ BTU/hr-ft².

In this model, heat flux in the boiling section will be at levels considerably below 6×10^4 BTU/hr-ft² and the full range of quality must be considered. Therefore, in order to observe the performance of the Schrock and Grossman correlation at lower heat flux and quality above 0.57 a plot was made (fig. 6) of the ratio $h_{\rm tpf}/h_{\rm 2}$ vs. quality



where h, is the heat transfer coefficient from the Dittus-Boelter correlation for water at saturated liquid conditions. The correlation of Dengler and Addoms as given in Tong [Ref. 10] for entirely forced convection vaporization is included for comparison. Tong [Ref. 10] indicates that low heat flux and high water-vapor mixture velocity favor the forced convection mechanism. After a review of the information available in Tong, it is not entirely clear whether the forced convection mechanism or the nucleate boiling mechanism is dominant for the relatively low flow velocities and low heat flux of this model. In any case, the Schrock and Grossman correlation applied at low heat flux represents a type of compromise between the entirely forced convection assumptions of Dengler and Addoms and the "mixed" assumption of Schrock and Grossman. When the Schrock and Grossman correlation is applied under the conditions of very low heat flux and quality (x < 0.05), as in the first pass of the boiling section of this model, it can be seen that the ratio $h_{tof}/h_{\boldsymbol{2}}$ becomes less than one. This is both unrealistic and computationally difficult to handle. Therefore, in the boiling section, the model assumes that h_{tpf} = h₂ for the first pass or for any pass where x < 0.05. This assumption will produce a more realistic but still conservative design.

One other simplification should be explained prior to discussion of the actual model calculations for the boiling section. Since the boiling section calculations are performed

for one complete pass at a time, the average quality, $\mathbf{x}_{\mathbf{a}}$, in a particular pass is used as the "local" quality to compute the inside heat transfer coefficient from the Schrock and Grossman correlation.

The first pass in the boiling section, as indicated in the calculations for the heating section, will, in general, involve both heating water to the saturation temperature and the initiation of boiling. From the calculations for the last pass of the heating section we have the following quantities for the first pass of the boiling section: water inlet temperature $(T_{\rm fin}^1)$, average gas outlet temperature $(T_{\rm gout}^1)$. The gas side heat transfer coefficient, $h_{\rm g}$, is obtained, using the average gas temperature in the boiling section, in the same way as for the heating section.

A rough estimate for the gas temperature into the first pass must be obtained in order to begin calculations for that pass. This is accomplished by calculating a rough overall heat transfer coefficient, U_{oi}^1 , for the pass using the tube wall resistance, h_g , and neglecting inside resistance. A pass effectiveness, ϵ_p^1 , is then calculated assuming that only boiling takes place in the pass. The expression for effectiveness for fluids unmixed between passes for C = 0 becomes

 $\varepsilon_{p} = (1 - \exp(-N))$

where N = NTU. Using $\varepsilon_{\rm p}$ calculated from this expression, the rough gas temperature for the first pass is

$$T_{g_{in}}^{l} = \frac{\varepsilon_{p}^{l} T_{fin}^{l} - T_{gout}^{l}}{\varepsilon_{p}^{l} - 1}$$

Since this pass has been simplified by allowing the inside heat transfer coefficient to be computed by the Dittus-Boelter correlation this initial guess for $\mathbf{T}_{g_{in}}^{1}$ is not essential. It would, however, become important if we were attempting to "split" the pass with two inside heat transfer coefficients, one for heating and one for boiling. Instead, the inside heat transfer coefficient, \mathbf{h}_{f}^{1} , is calculated for the entire pass using the Dittus-Boelter correlation with water conditions corresponding to the average water conditions in the heating section of the pass, that is,

$$T_{f_{avg}}^{l} = \frac{T_{f_{in}}^{l} + T_{satf}}{2}$$
.

With this inside heat transfer coefficient, an expression for the overall heat transfer coefficient for the first pass may be written,

$$U_{\text{oi}}^{1} = \frac{\frac{1}{\frac{1}{h_{\text{f}}^{1}} + \frac{A_{\text{ip}} \ln(d_{\text{o}}/d_{\text{i}})}{2 \pi K_{\text{w}} N_{\text{t/p}} L} + \frac{A_{\text{ip}}}{A_{\text{op}}} \frac{1}{h_{\text{q}}^{1} n_{\text{t}}}}}$$

The pass effectiveness, ϵ_p^1 , is now calculated in the same manner as previously described. With ϵ_p^1 , the average gas

temperature in is calculated from

$$T_{g_{in}}^{l} = \frac{\varepsilon_{p}^{l} C_{min} T_{f_{in}}^{l} - C_{max} T_{g_{out}}^{l}}{\varepsilon_{p}^{l} C_{min} - C_{max}}$$

The pass heat transfer may be calculated from

$$Q_p^1 = \dot{m}_g C_{pg} (T_{g_{in}}^1 - T_{g_{out}}^1)$$
.

The expression for out let enthalpy from the pass is

$$h_{\text{fout}}^1 = h_{\text{fin}}^1 + \frac{Q_p^1}{m_f}$$

and outlet quality is calculated from

$$x_{out}^1 = \frac{h_{fout}^1 - h_{satf}}{h_{fg}}$$
.

In order to determine the location of the interface between heating and boiling the total inside area devoted to heating in the first pass is calculated from

$$A_{ih}^{1} = (\frac{h_{satf} - h_{fin}^{1}}{h_{fout}^{1} - h_{fin}^{1}}) A_{ip}$$

Subsequent fluid passes in the boiling section are calculated until the quality at the outlet of a pass is found to be greater than 1.0. When this occurs, the boiling section is allowed to end with the last pass for which $x_{out} \leq 1.0$. A "mixed" pass where both boiling and superheating

takes places will be calculated in the superheating section of the model.

After the first pass, boiling section fluid passes are calculated in the following manner.

- 1. The steam quality at the outlet of the previous pass becomes the inlet quality for the current pass, \mathbf{x}_{in} . The average gas temperature at the inlet to the previous pass becomes the outlet average gas temperature, $\mathbf{T}_{\mathbf{g}_{\text{out}}}$, for the current pass.
- 2. Using the last overall heat transfer coefficient calculated for the previous pass, $U_{\mbox{oi}}$, approximate values of NTU and $\epsilon_{\mbox{p}}$ are calculated.
- 3. With this approximate $\boldsymbol{\epsilon}_p$ the average gas temperature into the current pass is calculated from

$$T_{g_{in}} = \frac{\epsilon_p T_{f_{sat}} - T_{g_{out}}}{\epsilon_p - 1}$$

- 4. Using this gas temperature in, $T_{g_{in}}$, the pass heat transfer, Q_p , is calculated. This allows the calculation of enthalpy out, h_f , and quality out, x_{out} , as well as the average quality in the current pass, x_a .
- 5. The inside heat transfer coefficient, h_{tpf}, may now be calculated,

$$h_{tpf} = B\left[\frac{Q_p/A_{ip}}{Gh_{fg}} + A\left(\frac{1}{x_{tt}}\right)^n\right] h_{\ell}$$
,

where the Martinelli parameter $\frac{1}{x_{tt}}$ is calculated using average quality, x_a , and all other terms are as previously described.

- 6. A new overall heat transfer coefficient is now calculated from which a new pass effectiveness can be calculated.
- 7. This new pass effectiveness yields a new average gas temperature into the pass from which a new pass heat transfer may be calculated.
- 8. The new pass heat transfer is compared with the previously calculated pass heat transfer. If the two heat transfer calculations do not agree to within 5% the entire set of calculations is repeated.
- 9. When the pass heat transfer calculation converges, the final quality at the outlet of the pass is calculated. If the quality is less than 1.0 another pass is calculated for the boiling section.
- 10. If the quality is 1.0, the boiling section ends with the current pass. If the quality out exceeds 1.0 the boiling section ends with the previous pass.

Calculations for the average gas film temperature and gas-side pressure drop are performed in the same manner as for the heating section.

E. SUPERHEATING SECTION

The first pass of the superheating section will, in general, involve both boiling and superheating. The inside heat transfer coefficients will be quite different for the

boiling and superheating portions for the pass, and, for this reason, the pass will be "split" to allow more accurate calculation of the heat transfer in these two regions. An outline of the calculation scheme is as follows:

- Calculate the gas-side heat transfer coefficient for the section in the same manner as for the previous two sections.
- 2. Estimate the average gas temperature into the first pass. This is only a rough guess for $\mathbf{T}_{g_{in}}$, to begin the calculation.
- 3. Calculate the required heat transfer in the boiling portion

$$Q_{rb} = \dot{m}_f (h_{f_{in}} - h_{satv})$$

where h_{fin} is the enthalpy out of the last pass of the boiling section and h_{satv} is the enthalpy of saturated vapor.

- 4. Using $Q_{\rm rb}$ and the average quality in the boiling portion of the first pass, calculate the inside heat transfer coefficient, $h_{\rm tpf}$, using the Schrock and Grossman correlation, as in the boiling section of the model. This, together with the gas-side heat transfer coefficient and the wall resistance, will yield an overall heat transfer coefficient for the boiling section, $U_{\rm oi}^{\rm b}$.
- 5. The calculation of the area required for the boiling portion of the pass is performed in an iterative scheme as follows.

- a. An initial estimate for the required boiling area,
 Al, is made.
- b. The mass flow rate of the gas over the boiling portion is then

$$\dot{m}_g^b = \frac{Al}{A_{ip}} \dot{m}_g .$$

c. An effectiveness for the boiling portion may be calculated from

$$\varepsilon_{b} = \frac{Q_{rb}}{C_{min}^{b}(T_{g_{in}} - T_{f_{sat}})}$$

where

$$c_{\min}^b = \dot{m}_g c_{pg}.$$

d. Using the previously calculated overall heat transfer coefficient, the estimated boiling area and the consequent gas-side heat capacity, NTU is calculated from

$$NTU = \frac{U_{oi}^{b} Al}{C_{min}^{b}}.$$

e. A "test" effectiveness, ϵ_b^t , can be found by applying this NTU in the relationship for effectiveness

$$\varepsilon_b^t = 1 - \exp(NTU)$$
.

f. The two effectiveness calculations, ϵ_b and $\epsilon_b^t,$ are compared.

- (1) If ε_b^t is greater than ε_b , then the original estimate for the boiling area, Al, was too large for the heat transfer required and the specified gas temperature into the pass. So, the estimate for the boiling area is decreased and a new Al is established.
 - (2) If ε_b^t is less than ε_b , Al is increased.
 - g. A new gas-side heat capacity is calculated from

$$C_{\min}^b = \frac{Al}{A_{ip}} \dot{m}_g C_{pg}$$
.

h. A new boiling portion effectiveness is calculated using the latest boiling area estimate

$$\varepsilon_{\rm b} = \frac{Q_{\rm rb}}{C_{\rm min}^{1} (T_{\rm g_{in}} - T_{\rm f_{sat}})}.$$

- i. As before, an NTU is calculated with the new Al. This generates a new "test" effectiveness, ϵ_b^t , which is compared with ϵ_b . If ϵ_b and ϵ_b^t are not equal, a new Al is calculated based on the comparison.
- j. These calculations are continued until $\epsilon_b = \epsilon_t$. The current Al is then set equal to A_i^b .
- 6. Once the area required for boiling, A_{i}^{b} , for a particular average gas inlet temperature has been established, the following first pass quantities can be calculated:
 - a. A_i^{sh} = area available for superheating

$$A_i^{sh} = A_{ip} - A_i^b$$

b. \dot{m}_g^b = gas flow rate over the boiling portion

c. \dot{m}_b^{sh} = gas flow rate over the superheating portion

d. $T_{g_{out}}^{b}$ = gas temperature out of the boiling portion

$$T_{g_{out}}^b = T_{g_{in}} - \frac{Q_{rb}}{\dot{m}_g^b C_{pg}}$$

$$T_{g_{out}}^{sh} = \frac{A_{ip} T_{g_{out}} - A_{i}^{b} T_{g_{out}}^{b}}{A_{i}^{sh}}$$

(The weighted average of T_{gout}^{sh} and T_{gout}^{b} must equal the T_{gout} previously calculated.)

7. Since the heat transfer to the cold side must satisfy an energy balance involving the average temperatures of the gas, the expected heat transfer in the superheating portion may be calculated from the heat release on the gas side

$$Q_p = \dot{m}_g C_{pg} (T_{g_{in}} - T_{g_{out}}),$$

and the required heat transfer in the superheating portion as

$$Q_{sh} = Q_p - Q_{rb}$$
.

- 8. The enthalpy and temperature of the steam out of the first pass may be calculated from the assumed heat transfer in the superheating portion, $Q_{\rm sh}$.
- 9. The steam properties for the superheating portion may now be found. These properties, along with h_g and wall resistance, will yield an overall heat transfer coefficient, $U_{\text{OI}}^{\text{sh}}$, for the superheating portion. The Dittus-Boelter correlation is applied to calculate the inside heat transfer coefficient.
- 10. The heat capacities on the gas and fluid sides are calculated, using the current gas mass flow rate over the superheating portion, $\dot{m}_g^{\rm sh}$, to calculate the gas heat capacity. The heat capacities along with $U_{\rm oi}^{\rm sh}$ and $A_{\rm i}^{\rm sh}$ yield the effectiveness for the superheating portion of the pass, $\varepsilon_{\rm sh}$.
- 11. A new average gas temperature into the pass may now be calculated from the superheating portion effectiveness and the superheating portion heat transfer required to satisfy the original heat balance from the expression

$$T_{g_{in}}^* = T_{f_{in}} + \frac{Q_{sh}}{\epsilon_{sh} C_{min}^{sh}}$$
.

This temperature, $T_{g_{in}}^{\star}$, is a measure of the temperature which would be required to produce the originally specified Q_{sh} under the actual conditions of the heat transfer characteristics of the superheating portion.

- 12. If the $T_{g_{1n}}^*$ is the same as the originally specified average gas temperature into the pass, $T_{g_{1n}}$, then the heat transfer in the superheating portion, Q_{sh} , is possible under the current distribution of area between boiling and superheating and the heat balance is satisfied between steam and gas sides for the specified gas temperature in. In this event, the calculations for the first pass of the superheating section are complete.
- 13. If $T_{g_{in}}^*$ is less/greater than the current $T_{g_{in}}$ the average gas temperature into the pass is increased/decreased and the entire set of calculations is performed again until $T_{g_{in}}^* \doteq T_{g_{in}}$.
- 14. The second and subsequent superheating section passes are calculated in much the same way as in the heating section. That is, an overall pass effectiveness is calculated for a specified number of passes, using the multipass effectiveness relationship from Kays and London [Ref. 9].
- 15. The average steam-side heat transfer coefficient, h_f , is calculated using the Dittus-Boelter correlation with steam properties at steam bulk temperature for the remainder of the superheating section. The overall heat transfer coefficient and the average pass effectiveness, ε_p , are then calculated.
- 16. The formulation for overall effectiveness with the number of passes, n, variable, is

$$\varepsilon_{\text{oa}} = \frac{\left(\frac{1-\varepsilon_{\text{p}} C_{\text{min}}/C_{\text{max}}}{1-\varepsilon_{\text{p}}}\right)^{n} - 1}{\left(\frac{1-\varepsilon_{\text{p}} C_{\text{min}}/C_{\text{max}}}{1-\varepsilon_{\text{p}}}\right)^{n} - \frac{C_{\text{min}}}{C_{\text{max}}}}.$$

As in the heating section this expression is used in an iterative fashion, beginning with n = 1.

17. Each time $\epsilon_{\rm oa}$ is solved, the gas temperature into the superheating section is calculated from

$$T_{g_{in}} = \frac{\varepsilon_{oa} C_{min} T_{f_{in}} - C_{max} T_{g_{out}}}{\varepsilon_{oa} C_{min} - C_{max}}$$

where T_{f} is the temperature of the steam into the second pass of the superheater and T_{g} is the average gas temperature out of the second pass of the superheater. This gas temperature in is compared with the originally specified gas temperature into the heat exchanger, T_{g1} .

18. If the calculated gas temperature in, \mathbf{T}_{gin} , is less than \mathbf{T}_{gl} the number of passes is increased by one and the calculation is performed again. If \mathbf{T}_{gin} exceeds \mathbf{T}_{gl} , the superheater is allowed to stop with the previous pass.

Calculations for the average gas film temperature and the gas-side pressure drop are performed in the same manner as for the heating and boiling sections.

F. MATCHING SUPERHEATER GAS INLET TEMPERATURE

The model calculations thus far lead to a waste heat recovery unit design for which the gas temperature at the

inlet is, in general, lower than that specified in the initial conditions. This condition occurs because the superheater ends with the last complete pass calculated for which the entering gas temperature is less than or equal to the originally specified WHRU inlet temperature. This outcome is, of course, unsatisfactory since the inlet gas temperature is an independent quantity which is a function of the horse-power setting on the gas turbine. An iterative scheme is employed for matching the T calculated in the superheating $g_{\rm in}$ section with the $T_{\rm gl}$ specified in the initial conditions.

Since the model does not allow the calculation of fractional passes and since the scheme for the calculation of superheater passes will not allow inclusion of a pass which would require a gas inlet temperature higher than that specified in the initial conditions, the final gas inlet temperature calculated for the WHRU will generally be lower than that initially specified. In order to match this superheater gas inlet temperature with that specified initially, the heat exchanger gas outlet temperature is allowed to rise. Each time the gas outlet temperature is increased, the entire waste heat recovery unit calculation is performed again, and the calculated superheater gas inlet temperature is compared with the gas turbine exhaust temperature. When a match is achieved the design is fixed.

G. OFF-DESIGN CALCULATIONS

Once a particular design has been selected the designer must test that design at several off-design points. A design will define the following WHRU characteristics:

Dimensions (length, width, height)
Operating pressure
Superheater outlet temperature
Fin-tube configuration.

The off-design calculation requires that the selected WHRU design performance be predicted for a gas inlet temperature and flow rate different from that which was used to produce the selected design. The design model can be used in an iterative fashion to make this calculation. All model calculations are made as prescribed in the previous sections, with the exception of the pinch point calculations which are not performed.

The off-design procedure requires that the designer fix the WHRU frontal dimensions, operating pressure, fintube configuration and minimum gas outlet temperature. A design is then produced for a gas inlet temperature and flow rate at an off-design point. This design is checked to determine whether it conforms to the height dimension of the WHRU designed at the gas conditions of the off-design point. If the height dimension is not matched then the number of WHRU passes must be adjusted until a match with the design-point WHRU is achieved. The number of WHRU passes

may be altered by either adjusting the WHRU gas outlet temperature or the superheater outlet steam temperature. The effect of either of these adjustments is to change the steam flow rate and the heat transfer rate. It would be possible to adjust the steam flow rate and allow the superheater steam outlet temperature to remain fixed. However, for the method of this model, the computation time required for this means of control would be large. actual procedure used produces designs relatively quickly which closely approximate the results which would be obtained by a fine control on steam flow. Each time the superheater steam outlet or gas outlet temperature is adjusted, a new design is produced. This procedure is continued until a design is produced for which the height (number of passes) equals that of the design point WHRU. When the WHRU height at the off-design gas conditions is equal to that of the design point WHRU, the gas inlet temperature is matched with the gas inlet temperature specified for the off-design point, using the procedure described in Section E.

H. COGAS SYSTEM OUTPUT MODEL

The COGAS system output model calculates performance parameters for the combined steam and gas turbine system for a specified gas turbine input power. The WHRU model provides a steam flow rate, pressure, and temperature for a specified set of gas turbine exhaust gas conditions which correspond to a particular gas turbine horsepower setting.

This WHRU output is applied in a simple Rankine cycle to calculate the steam-side power output. The gas-side pressure drop calculated in the WHRU model is used to arrive at a revised gas turbine horsepower. By combining these two power outputs, a COGAS system power can be calculated. Other performance indicators such as specific fuel consumption, thermal efficiency and steam turbine share of the load are also calculated in the COGAS system output model.

1. Rankine Cycle

The following conditions are assumed for the Rankine cycle calculations:

- a. No line losses
- b. Steam turbine efficiency = η_{st} = 0.85
- c. Condenser pressure = 2.0 psia (4 in Hg)
- d. Feedwater heater pressure = 15 psia
- e. Feedwater temperature = 200 F
- f. Pumping power required is neglected
- g. Fuel LHV = 18400 Btu/lbm

The following input conditions are received from the WHRU model: steam turbine inlet pressure $(\mathtt{P_1})$, steam turbine inlet temperature $(\mathtt{T_1})$, steam flow rate $(\dot{\mathtt{m}}_{\mathtt{f}})$, gas turbine exhaust pressure drop $(\Delta\mathtt{P_{gas}})$. From $\mathtt{P_1}$ and $\mathtt{T_1}$ the turbine inlet enthalpy $(\mathtt{h_1})$ and inlet entropy $(\mathtt{s_1})$ can be found. The turbine exhaust steam quality, assuming isentropic expansion, $\mathtt{x_{2s}}$, is calculated from

$$x_{2s} = \frac{s_1 - s_f}{s_{fg}},$$

where

s_f = entropy of saturated water

s_{fq} = entropy increment for evaporation.

The steam turbine exhaust enthalpy assuming isentropic expansion, h_{2s} , may now be calculated from

$$h_{2s} = h_f + X_{2s} h_{fg}$$

where

 h_f = enthalpy of saturated water

 h_{fq} = enthalpy increment for evaporation.

The isentropic turbine work is

$$W_{ts} = h_1 - h_{2s} ,$$

and the actual steam turbine work is calculated from

$$W_t = \eta_{st} W_{ts}$$
.

The actual turbine exhaust enthalpy and quality are

$$h_2 = h_1 - W_t$$

and

$$x_2 = \frac{h_2 - h_{2f}}{h_{fg}}$$
.

In this model it is assumed that heating steam for the feed-water heater is provided, via a reducing station, from the main steam line. The fraction of the steam mass flow rate from the WHRU required for the feedwater heater is

$$m = \frac{h_{fw} - h_2}{h_1 - h_2}$$

where

 $h_{fw} = enthalpy of the feedwater$

h₂ = enthalpy of the condensate at feedwater heater pressure.

Therefore, the steam turbine power output is

$$P_{st} = (1-m) \dot{m}_f W_t.$$

2. Gas Turbine Performance Calculations

The original gas turbine horsepower, exhaust gas flow rate, and exhaust gas temperature inputs to the WHRU model were hand-calculated using figure 4 of Ref. 11 and figures 1, 6, and 8 of Ref. 10. The assumptions used to calculate the WHRU model inputs were:

Ambient temperature = 100 F

Ambient pressure = 14.696 psia

Humidity = 0.0

Fuel LHV = 18400 Btu/lbm

Inlet loss = 4.0 in. H_2O

Exhaust loss = 6.0 in. H_2O

In the COGAS system output model, the gas turbine horsepower correction factor for the gas-side pressure drop in the WHRU (BHP for 6" loss/BHP for WHRU loss) is found by solving

$$C_{\rm bhp} = 1.0125 + 0.002125 \Delta P_{\rm gas}$$
,

where $C_{\rm bhp}$ = BHP for 6" loss/BHP for WHRU loss. This relationship was found by extending the duct loss relationship of fig. 7, Ref. 11 linearly from the point of 6 in. H₂O exhaust duct loss already assumed. The final gas turbine horsepower is

$$P_{gt} = \frac{P_{gt}^*}{C_{bhp}}$$

where Pgt is the input gas turbine horsepower. The total COGAS system horsepower, Ptot, is found by adding the steam turbine and final gas turbine horsepowers.

In order to calculate the gas turbine specific fuel consumption fig. 4 of Ref. 11 is entered with the final

gas turbine horsepower, and the s.f.c. is read from the propeller law curve superimposed on that figure. The s.f.c. correction factor for exhaust loss in the WHRU, $C_{\rm sfc}$, is found in the same manner as $C_{\rm bhp}$ from fig. 6 of Ref. 11 where

 $C_{sfc} = (s.f.c. \text{ for total exhaust } \Delta P)/(s.f.c. \text{ for 6" exhaust } \Delta P)$

and the gas turbine specific fuel consumption is

The specific fuel consumption for the combined system is calculated by first finding the fuel consumption rate of the gas turbine

The COGAS system s.f.c. is then calculated from

s.f.c._{COGAS} =
$$\frac{\dot{m}_{fuel}}{P_{tot}}$$

To allow the direct comparison of the COGAS system with the all gas turbine system the specific fuel consumption of the gas turbine at the new, higher COGAS system power, s.f.c. $_{gt}^*$, is calculated in the same manner as s.f.c. $_{gt}$.

The thermal efficiencies for the gas turbine at input power, the COGAS system, and the gas turbine at COGAS system power are calculated from the relationship

$$\eta_{th} = \frac{2545}{\text{s.f.c. LHV}}$$
.

Additionally, the steam turbine share of the load is calculated from $P_{\text{st}}/P_{\text{tot}}$.

III. RESULTS AND CONCLUSIONS

A. BACKGROUND

The foregoing model was applied in a computer simulation program written in FORTRAN IV for the IBM 360-67 computer. A listing of this program appears in Appendix A. Additionally a set of supporting programs was written for water, steam, and air properties. A listing of this set of programs appears in Appendix B.

In order to test the model and develop an understanding of the behavior of the WHRU, a set of designs were produced for a variety of initial conditions. These designs were then reviewed, and an analysis of the model behavior was performed. After completion of the model analysis, several of the designs were selected for observation at off-design conditions. The off-design simulations were produced for gas turbine input powers corresponding to ship speeds of 9, 16, and 20 knots, which represents the entire range of gas turbine input powers considered in this thesis. Finally, two designs were selected for detailed testing at off-design conditions. These latter two designs were tested at gas turbine input horsepowers corresponding to speeds of 9 to 20 knots, at one knot increments.

B. DESIGN VARIABLES

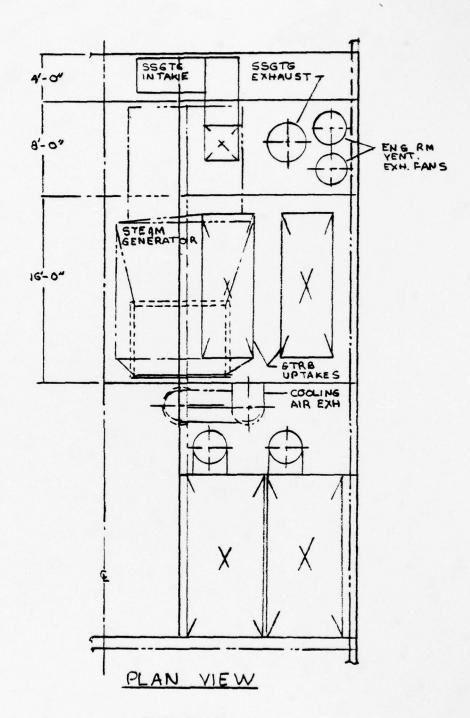
The following set of design variables was selected to produce the basic set of designs.

- 1. WHRU operating pressure: Three WHRU operating pressures of 400, 600, and 800 psia were selected for design production.
- 2. WHRU geometric scale: In order to test the model response to a range of fin-tube sizes, designs were produced for the basic fin-tube configuration described in the geometry subsection at 1.0, 0.75, and 0.50 scale.
- 3. Frontal dimensions: The approximate WHRU space constraints for a DD-963-type engineroom are shown in figures 7, 8 and
- 9. Consistent with these constraints, frontal dimensions of 12' x 12' and 12' x 15' were selected for the initial design set.
- 4. Gas turbine input power: The gas turbine input horsepower determines the input gas conditions, temperature and
 flow rate, for the WHRU. Since the most advantageous use
 of the COGAS system was assumed to be for "cruise" speed
 conditions, the range of gas turbine input horsepower considered corresponds to the gas turbine power required for
 a ship speed range of 9 to 20 knots, with the gas turbine
 operating alone. The three gas turbine input powers selected
 for the production of WHRU designs are shown in Table I.

Gas Turbine Input Powers

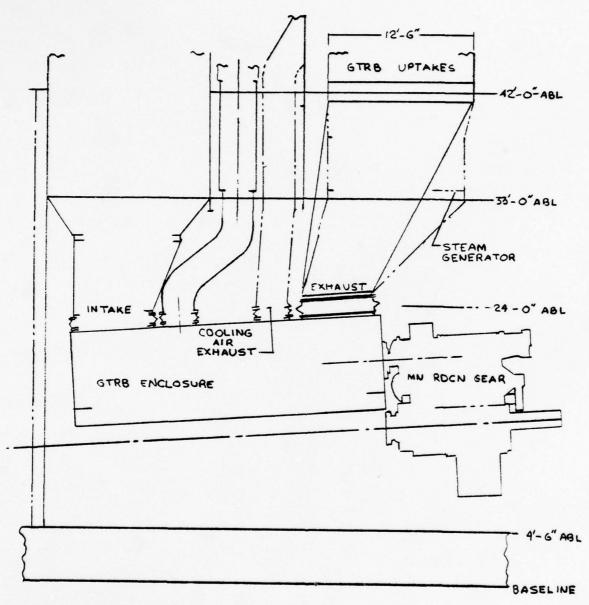
GTHP	Approx. Speed (kts)	Temperature (F)	Flow Rate (lbm/hr)
16421	20	849	407589
8526	16	742	328641
1684	9	689	159731

Table I



ENGINEROOM

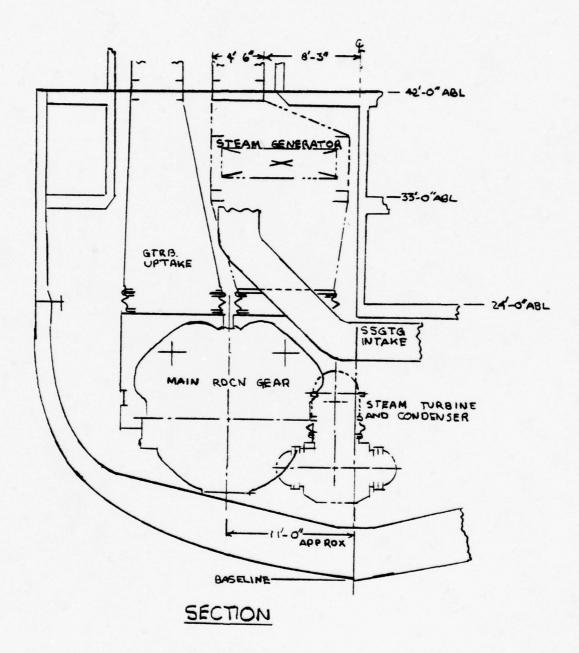
FIGURE 7



ELEVATION

ENGINEROOM

FIGURE 8



ENGINEROOM

FIGURE 9

- WHRU gas outlet temperature: The WHRU gas outlet temperature is fixed at 400 F. Reference 3 states that the principal cause of "hot" corrosion in the WHRU would be due to the formation of H2SO4 from an expected concentration of SO3 of up to 50 parts per million. Reference 13 states that dew point condensation of vapor in the exhaust gas becomes a problem for corrosion if the stack temperature is depressed below 250 F. Therefore, a minimum average gas outlet temperature of 400 F is considered to be reasonably safe from the aspect of gas-side corrosion prevention. It should be further noted that the outlet gas temperature calculated by the program is an average temperature, based on the heat release from the gas. Therefore, the actual temperature of the gas in the stack will be cooler than 400 F in some locations due to the non-uniform distribution of the gas temperature as it leaves the WHRU. It should further be noted that, although this temperature is a fixed design variable for design production, it will vary somewhat from 400 F in response to the program calculations for setting the minimum pinch point and for matching the gas inlet temperature with that specified in the initial conditions.
- 6. Superheater outlet steam temperature: The target WHRU superheater outlet steam temperature is 650 F. This temperature will also vary somewhat in response to steam flow rate changes brought about by the program calculations to match

the gas inlet temperature with that specified in the initial conditions.

- 7. WHRU water inlet temperature: The WHRU water inlet temperature is fixed at 200 F.
- 8. The other major COGAS system parameters are fixed as follows:

Condenser pressure: 4 in. Hg

Steam turbine efficiency: 0.85

Feedwater heater pressure: 15.0 psia

Fuel LHV: 18400 Btu/lbm.

C. THE DESIGN SET

A set of 54 designs was produced for the combination of design variables just discussed. The array of design variable combinations is described in Table II. The summary computer output pages for the results of each design run are presented in Appendix C.

As discussed in Section A, the purposes for producing this design set were to test the model and to promote an understanding of the likely behavior of a WHRU for a range of conditions. To this end, the following set of output variables was considered.

1. WHRU output

- a. height (number of passes)
- b. gas inlet temperature
- c. gas outlet temperature
- d. steam flow rate

WHRU DESIGN COMBINATIONS AND DESIGN RUN INDEX

X 15'	Scale=0.50	run #52	run #43	run #34	run. #53	run #44	run #35	run #54	run #45	run #36
Front: 12' X 15'	Scale=0.75	run #49	run #40	run #31	run #50	run #41	run #32	run #51	run #42	run #33
	Scale=1.0	run #46	run #37	run #28	run #47	run #38	run #29	run #48	run #39	run #30
12.	Scale=0.50	run #25	run #16	run #7	run #26	run #17	run #8	run #27	run #18	run #9
Front: 12' X 12'	Scale=0.75	run #22	run #13	run #4	run #23	run #14	run #5	run #24	run #15	run #6
121	Scale=1.0	run #19	run #10	run #1	run #20	run #11	run #2	run #21	run #12	run #3
	Pressure	400	009	800	400	009	800	400	009	800
	GTHP		16421			8526			1684	

TABLE II

- e. gas side pressure drop
- f. pinch point temperature difference
- g. heat transfer rate
- 2. COGAS system output
- a. gas turbine horsepower (including loss from the WHRU gas-side pressure drop)
 - b. steam turbine horsepower
 - c. COGAS system horsepower
 - d. steam turbine share of the load
 - e. specific fuel consumption
 - (1) s.f.c. of COGAS system
 - (2) s.f.c. of gas turbine at COGAS system horsepower
 - f. thermal efficiency
 - (1) η_{+h} of COGAS system
- (2) η_{th} of gas turbine at COGAS system horsepower Clearly, several of these variables are related, such as s.f.c. and η_{th} , and no additional information is provided by studying all variables in a closely related group. Therefore, the following subset of output variables was selected for analysis.
- 1. WHRU height
- 2. Steam flow rate
- 3. Gas-side pressure drop
- 4. Pinch point temperature difference
- 5. WHRU heat transfer rate
- 6. WHRU gas outlet temperature

- 7. Steam turbine horsepower
- 8. COGAS system horsepower
- 9. COGAS specific fuel consumption

The above output variables are presented in tabular form using the format of Table II. Table II also serves as an index for the set of basic designs. Additionally, the significant trends in the variables are presented graphically. Where the trend of the results was ascertained to be the same for the two frontal dimension sets, only the values for the 12' x 12' front were presented graphically. Where clarity was better served, only one scale was plotted as representative of the trend described.

Effect of Scaling.

The only significant trends noted with respect to scaling were a decrease in WHRU height with a decrease in scale and the same trend for gas side pressure drop (see Tables III and IV). The trends are shown in figures 10 and 11.

The basic fin-tube dimensions of the model were scaled by factors of 0.75 and 0.50. For any scale with constant frontal dimensions, the total inside and outside areas remain the same. That is, for a constant length tube, the scaled inside/outside area (A_i^S/A_o^S) is proportional to the full scale areas (A_i/A_o) with the scale factor, s, as the constant of proportionality. Hence

$$A_i^s = SA_i$$
 and $A_0^s = SA_0$.

WHRU HEIGHT [ft]

	91									
X 15'	Scale=0.50	1.5	1.8	2.0	1.5	1.5	1.5	1.1	1.1	1.0
Front: 12' X 15'	Scale=0.75	2.7	3.4	3.7	2.9	2.9	2.7	2.4	2.2	2.0
	Scale=1.0	4.6	5.5	5.9	4.9	4.9	4.6	3.9	3.6	3.3
12.	Scale=0.50	1.5	2.0	2.1	1.6	1.6	1.5	1.3	1.1	1.1
Front: 12' X 12'	Scale=0.75	2.9	3.7	3.9	3.2	3.2	2.9	2.4	2.2	2.2
떠	Scale=1.0	4.9	6.2	8.9	5.2	5.5	4.9	4.2	3.9	3.6
	Pressure	400	009	800	400	009	800	400	009	800
	GTHP		16421			8526			1684	

TABLE III

GAS SIDE PRESSURE DROP [in $\mathrm{H}_2\mathrm{O}$]

X 15'	Scale=0.50	2.5	3.0	3.3	1.6	1.6	1.7	0.3	0.3	0.3
Front: 12' X 15'	Scale=0.75	2.7	3.5	3.7	1.9	2.0	1.9	0.4	0.4	0.4
	Scale=1.0	3.3	4.0	.4.3	2.4	2.4	2.4	0.5	0.5	0.5
12.	Scale=0.50	3.5	4.9	5.3	2.7	2.8	2.5	9.0	0.5	0.5
Front: 12' X 12'	Scale=0.75	4.4	5.6	0.9	3.2	3.3	3.1	0.7	9 ° 0	9.0
141	Scale=1.0	5.3	6.7	7.8	3.8	4.1	3.7	8.0	8.0	0.8
	Pressure	400	009	800	400	009	800	400	009	800
	GTHP		16421			8526			1684	

TABLE IV

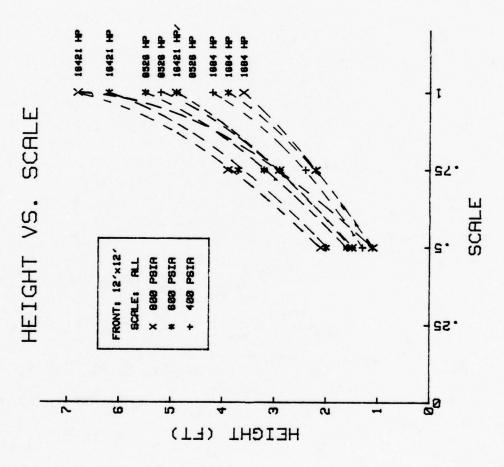


FIGURE 10

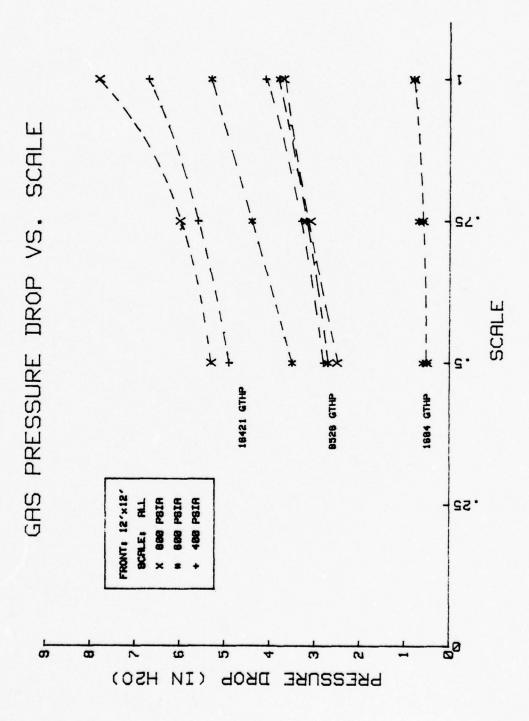


FIGURE 11

Since constant frontal dimensions are to be maintained, the number of tubes per row is scaled up by the scale factor, so

$$A_{ip}^{s} = \frac{N_{t/p}}{s} s A_{i}$$
 and $A_{op}^{s} = \frac{N_{t/p}}{s} s A_{o}$,

where $N_{\text{t/p}}$ is the number of tubes per pass. Therefore, the scaled outside and inside areas for a pass for constant frontal dimensions are the same as the full scale areas. Now, the scaled cross-sectional area for fluid flow on the inside will be,

$$A_{ff}^{s} = \frac{\pi}{4} s^{2} d_{i}^{2} \frac{N_{t/p}}{s} = s A_{ff}$$
.

So the scaled Reynolds number will be

$$R_e^s = \frac{\dot{m}_f s d_i}{s A_{ff} \mu} = \frac{\dot{m}_f d_i}{A_{ff} \mu}$$

which is equal to the Reynolds number for the unscaled geometry. It can also be shown that the outside Reynolds number remains constant with scaling. Recalling that the Dittus-Boelter correlation was used to calculate the inside heat transfer coefficient for the single phase regions and used with a multiplier for the two phase heat transfer coefficient and assuming constant fluid properties, the Nusselt number remains constant

$$N_u = 0.023 R_e^{0.8} P_r^{0.4} = Const. = C.$$

So, the scaled inside heat transfer coefficient

$$h_f^s = \frac{K}{s d_i} C = \frac{C}{s}$$

increases with a decreasing scale factor. Similarly, for the scaled gas-side heat transfer coefficient,

$$h_g^s = j \frac{k}{s d_o} R_e P_r^{1/3} = \frac{C}{s}$$
,

an increase is seen with a decreasing scale factor.

Therefore, in addition to a decrease in height attributable to a scaling down of the fin-tube dimensions, there is also an improvement in heat transfer which results in a further reduction in height by elimination of passes. This trend is supported by the results.

Recalling the relationship used to calculate the gasside pressure drop,

$$\Delta P_g = \frac{2f G_{\text{max}}^2 N_{\text{t/r}}}{\rho} (\frac{\mu_{\text{w}}}{\mu_{\text{b}}})^{0.14},$$

it can be shown that the scaled gas-side pressure drop is inversely proportional to the scale factor,

$$\Delta P_g^s = \frac{C}{s},$$

where C is a constant based on the assumption of constant gas properties between scales. For the same number of passes, then, an increase in gas-side pressure drop could be expected. However, since the number of passes is decreased with decreasing scale, a net decrease in gas-side pressure drop was experienced (Fig. 11).

Some differences in pinch point with scale were observed in Table V, but no consistent trend could be established. It was expected that pinch point AT would remain fairly constant with scale for fixed pressure and input gas conditions. That result was apparent to some extent, particularly in the range of high gas temperature and low steam pressure. This finding is consistent with the manner in which the pinch point AT is established. That is, the program fixes an initial pinch point ΔT only when the rough pinch point ΔT is less than 25 F in the initial calculations. At the lower pressures and higher gas temperatures this mechanism would not be operative. Also, the final and initial pinch point AT calculations are based on the average gas temperatures at the inlet to the pass where the ΔT is calculated. Therefore, the actual pinch point may be either lower or higher than the one calculated, depending on the actual gas temperature distribution at the inlet to the pass. The pinch point AT will be discussed at greater length in the analysis of the effects of pressure.

PINCH POINT AT [F]

	91									
X 15'	Scale=0.50	62.4	42.0	30.7	36.9	31.5	30.4	36.2	29.8	84.2
Front: 12' X 15'	Scale=0.75	64.8	45.8	36.4	36.4	31.6	30.5	29.9	9.03	47.7
	Scale=1.0	64.4	38.7	32.5	36.9	32.7	31.2	42.6	37.3	35.0
12.	Scale=0.50	71.9	48.4	36.0	41.1	36.7	34.8	39.9	33.0	30.9
Front: 12' X 12'	Scale=0.75	71.5	40.7	32.9	41.5	37.1	36.1	33.6	54.9	53.0
드	Scale=1.0	71.9	37.2	32.0	42.4	27.1	36.8	30.1	41.8	39.6
	Pressure	400	009	800	400	009	800	400	009	800
	GTHP		16421			8526			1684	

TABLE V

Effect of Pressure.

The most important effect of pressure on the model performance arises from the calculations which establish the minimum pinch point temperature difference. As related in the model description, the minimum pinch point ΔT is set at 25 F. The WHRU outlet gas temperature is adjusted in the initial model calculations in order to ensure this minimum AT. The initial model calculations establish the steam flow rate from a simple energy balance involving the gas inlet and outlet temperatures (T_{q1}, T_{q2}) , the gas flow rate, the water inlet temperature (T_{f1}) , the required steam outlet temperature (T_{f4}) , and the steam pressure. Tentative interim gas temperatures for the heater inlet, T_{q3} , and boiling section inlet, $T_{\alpha 2}$, are also established in this calculation set. In order to establish the minimum pinch point AT, the model tests the interim heater gas inlet temperature against the criterion

$$T_{g3} \geq T_{f2} + 25$$

where T_{f2} is the temperature of saturated water at the pressure specified. If T_{g3} is less than T_{f2} + 25 then T_{g3} is set equal to T_{f2} + 25 and a new gas outlet temperature is calculated as follows,

$$T_{g4} = \frac{T_{g3} - \alpha T_{g1}}{1 - \alpha}$$

where

$$\alpha = \frac{h_{f2} - h_{f1}}{h_{f4} - h_{f1}}.$$

As an aid to understanding the behavior of the model, it is useful to predict the WHRU gas inlet temperature at which this pinch point calculation becomes operative for a particular pressure. This is accomplished by establishing a "critical" heater gas inlet temperature, T_{g3}^{\star} , for each pressure considered,

$$T_{g3}^* = T_{f sat}^{+ 25}$$
,

where $T_{\rm f}$ sat is the temperature of saturated water at the pressure specified. The ratio α can also be solved for each pressure considered, based on a constant water inlet temperature of 200 F and a constant superheater outlet temperature of 650 F,

$$\alpha = \frac{h_f - h_1}{h_4 - h_1}$$

where h_f = enthalpy of saturated water at the pressure under consideration. Finally, assuming a minimum WHRU gas outlet temperature of 4-0 F the minimum WHRU gas inlet temperature at which the pinch point calculation comes into effect may be calculated as follows,

$$T_{gl}^* = \frac{T_{g3}^* - (1 - \alpha)400}{\alpha}$$
.

Table VI summarizes these calculations for each of the pressures considered in the design set.

Minimum Gas Inlet Temperature for Pinch Point Calculation

Pressure (psia)	T _{g3} (F)	<u>α</u>	T _{gl} (F)
400	470	.219	720
600	497	.262	770
800	543	.299	878

Table VI

Now the pressure at which the pinch point calculation becomes operative for each gas turbine input power considered is predicted. The pressure for which the pinch point calculation begins to adjust gas outlet temperature is listed below for each gas turbine input power considered, in Table VII.

Pressure At Which Pinch Point Calculation Takes Effect

Gas Turbine Input Power	gl (F)	Pressure (psia)	T _{gl} (F)
16421	849	800	878
8526	742	600	770
1684	689	400	720

Table VII

It should be recalled that the outlet gas temperature is also adjusted by the iterative technique employed to match the model-calculated gas inlet temperature with the gas inlet temperature of the initial conditions, once the design is established. This is a relatively minor adjustment, however, and is never greater than 10 F. These adjustments to WHRU gas outlet temperature are apparent in the values of Table VIII and are displayed graphically for the 12' x 12' frontal dimentions and 0.75 scale in Fig. 12.

The final calculated pinch point for each of the design sets reflected the influence of the initial pinch point calculation. These results were shown in Table V and Figure 13. It is re-emphasized here that the calculated pinch point ΔT is useful only as an indicator of what the actual pinch point might be for a particular heat exchanger design. This is true because the model neglects the possibility of a gas temperature distribution across the inlet of a WHRU pass and, instead, uses the average gas temperature for calculations.

There are two other trends in the design results which emanated directly from the control exercised by the model over the pinch point ΔT and the resulting gas-fluid temperature distributions in the designs produced. These trends were apparent when the effects of pressure on WHRU height and WHRU heat transfer/steam flow rate were examined.

WHRU GAS OUTLET TEMPERATURE [F]

151	Scale=0.50	405.0	400.8	414.2	405.1	436.5	459.9	420.0	452.4	485.5
Front: 12' X 15'	Scale=0.75	405.5	402.3	415.0	401.5	435.0	465.1	409.6	449.4	484.0
	Scale=1.0	400.5	405.0	419.0	401.5	431.0	462.9	409.6	450.9	485.5
12.	Scale=0.50	409.0	401.5	414.2	401.5	434.4	467.4	409.6	458.0	482.5
Front: 12' X 12'	Scale=0.75	405.5	407.5	421.0	401.5	433.5	465.9	412.6	456.5	482.5
[4]	Scale=1.0	405.5	404.5	415.0	403.5	430.5	464.4	410.5	449.4	483.0
	Pressure	400	009	800	400	009	800	400	009	800
	GTHP		16421			8526			1684	

TABLE VIII

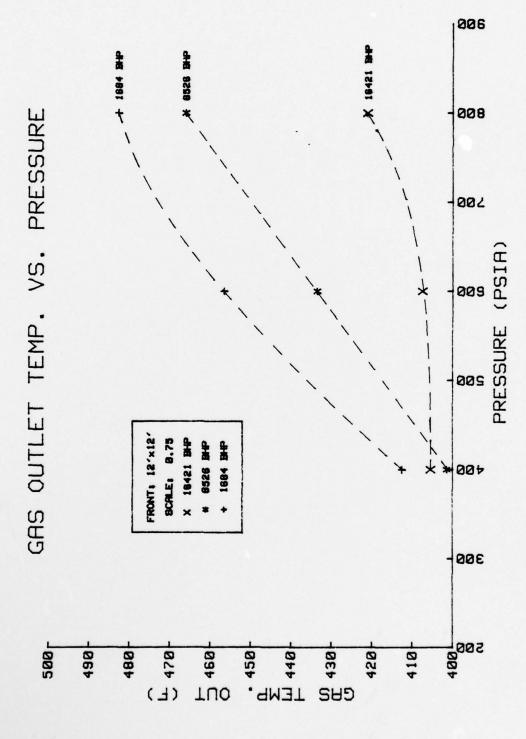


FIGURE 12

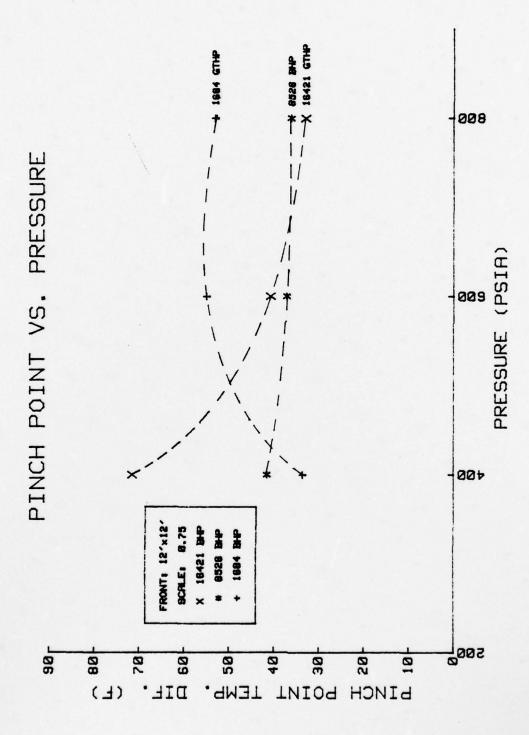


FIGURE 13

The effects of pressure on WHRU heat transfer and steam flow rate are shown in Figures 14 and 15 respectively. Tables IX and X list the actual values obtained for WHRU heat transfer and steam flow rate for the designs produced. WHRU heat transfer and steam flow rate directly reflected the adjustment of the WHRU gas outlet temperature to maintain the minimum pinch point ΔT . That is, as the WHRU outlet gas temperature was raised, the heat transfer rate and steam flow decreased. The small increase shown in Figures 14 and 15 in heat transfer and steam flow rate for 16421 gas turbine input power at the 0.50 scale reflects only a minor adjustment difference in $T_{q_{out}}$ for matching $T_{q_{in}}$ between 400 psia and 600 psia.

The relationship of WHRU height to WHRU pressure is slightly more complex. Figures 16, 17, and 18 demonstrate the approximate gas-fluid temperature distribution along the total length of the WHRU for the 0.75 scale at the three pressures and input horsepowers considered. The general trend observed in these diagrams of decreasing gas-fluid temperature difference with increasing pressure is representative of all the designs produced. This decrease in gas-fluid temperature difference, taken by itself, would produce larger heat exchangers with increasing pressure. This trend may be observed for the 12' x 12' front at the high gas turbine input horsepower in Figure 19. At the medium and low gas turbine horsepowers, however, the WHRU

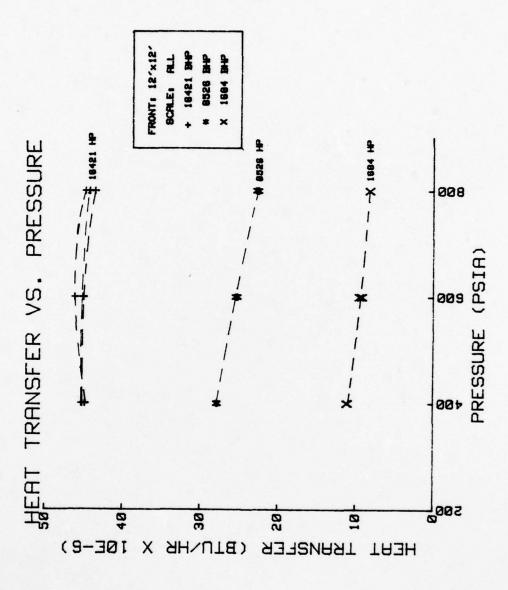


FIGURE 14

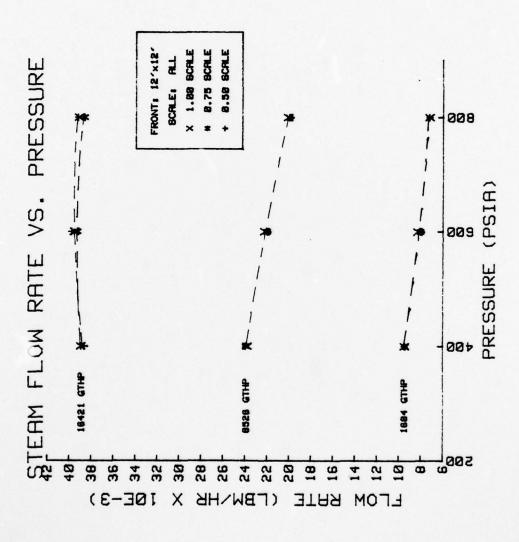


FIGURE 15

WHRU HEAT TRANSFER RATE [Btu/hr]

X 15'	Scale=0.50	45221999	45741675	44518908	27482604	25009580	23160974	10697984	9396176	8126315
Front: 12' X 15'	Scale=0.75	45211810	45680537	44304924	27959133	25198549	22635149	11133251	9523961	8174234
	Scale=1.0	45588830	45221999	43836197	27885189	25527190	22807685	11137244	9464062	8110341
12.	Scale=0.50	44773652	46118695	44763462	27876973	25173901	22462461	11125264	9160573	8194200
Front: 12' X 12'	Scale=1.0 Scale=0.75	45130292	44987636	43540695	27745516	25280709	22569421	11017446	9240438	8226146
(E)	Scale=1.0	45283138	45079343	44223406	27753732	25486109	22815901	11073352	9527954	8170241
	Pressure	400	009	800	400	009	800	400	009	800
	GTHP		16421			8526			1684	

TABLE IX

STEAM FLOW RATE [1bm/hr]

X 15'	Scale=0.50	38086	39818	39189	23698	21789	20426	9176	8184	7149
Front: 12' X 15'	Scale=0.75	38942	39693	39124	23945	21894	20052	9524	8286	7201
	Scale=1.0	39369	39455	38770	23945	22174	20212	9524	8235	7149
12.	Scale=0.50	38643	39758	39189	23945	21964	19892	9526	7992	7253
Front: 12' X 12'	Scale=0.75	38942	39239	38597	23945	21997	19999	9425	8044	7253
E-1	Scale=1.0	38942	39499	39124	23807	22207	20106	9494	8286	7236
	Pressure	400	009	800	400	009	800	400	009	800
	GTHP		16421			8526			1684	

TABLE X

TEMPERATURE DISTRIBUTION DIAGRAMS

SCALE: 0.75 FRONT: 12'X12' GTHP: 16421

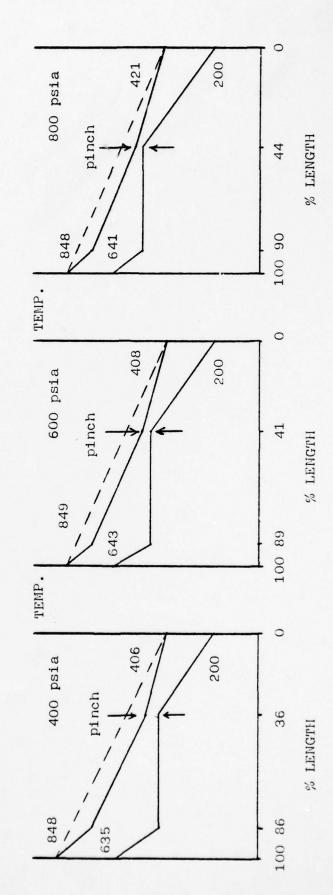
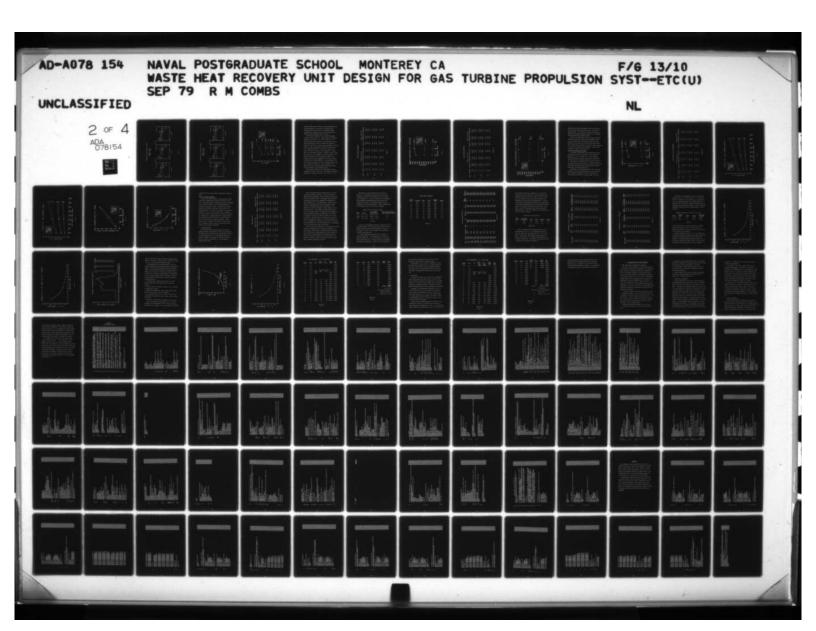
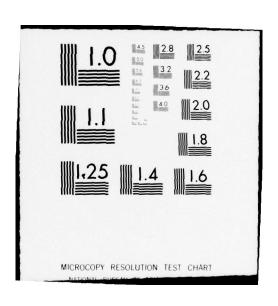


FIGURE 16





TEMPERATURE DISTRIBUTION DIAGRAMS

The Market Co.

SCALE: 0.75 FRCNT: 12'X12' GTHP: 8526

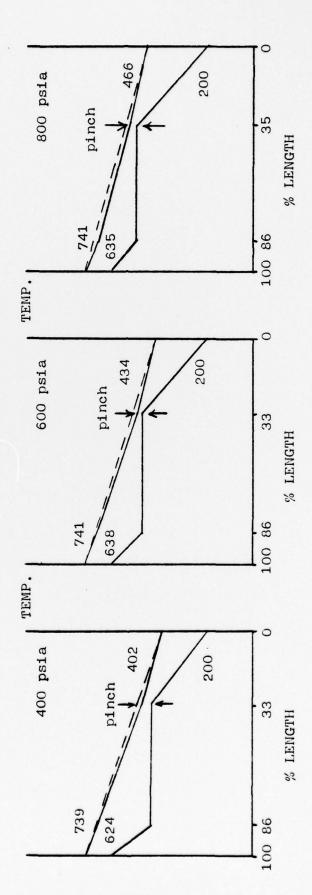


FIGURE 17

TEMPERATURE DISTRIBUTION DIAGRAMS

The state of the state of

SCALE: 0.75 FRONT: 12'X12' GTHP: 1684

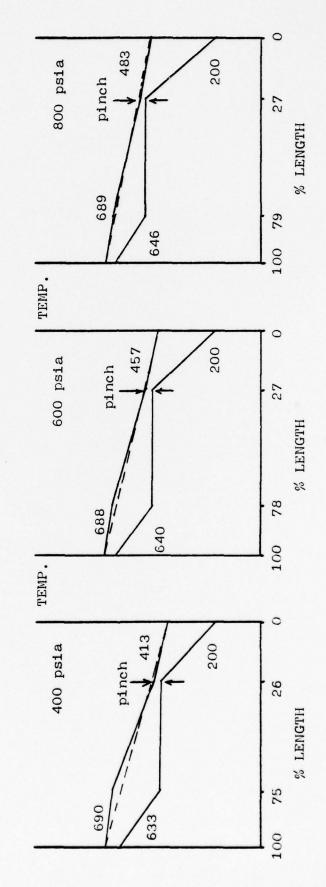


FIGURE 18

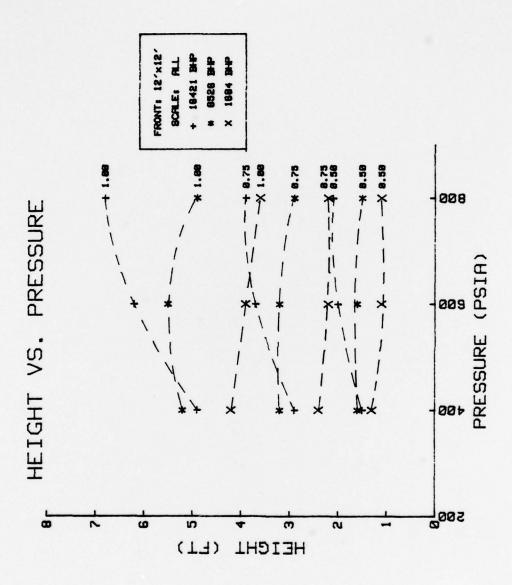


FIGURE 19

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height remained fairly constant or actually decreased with increasing pressure. This trend is explained by the decreasing heat transfer rate with increasing pressure attributable to the pinch point calculation adjustment to WHRU gas outlet temperature shown in Figure 12.

The design set results for steam turbine horsepower output are given in Table XI. These results are presented graphically for the 12' x 12' front in Figure 20. Two separate trends were identified. The steam turbine horsepower demonstrated an overall increase with increasing pressure for the high gas turbine input horsepower. Although there is a small net decrease in WHRU heat transfer rate with increasing pressure at the high gas turbine input power, the steam is rejected to the condenser at a lower quality for the higher pressures. Therefore, there is less heat rejection in the condenser for higher pressures. This better performance of the high pressure systems in the Rankine cycle more than compensates for the small decrease in WHRU output at these pressures. For the medium and low gas turbine input powers the trend of decreasing WHRU output with increasing pressure (Fig. 20) was dominant in the Rankine cycle also, producing systems of decreasing steam turbine horsepower with increasing pressure.

The design set results for the COGAS system combined horsepower are given in Table XII. The results are displayed graphically in Figure 21 for the 12' x 12' front. It is

STEAM TURBINE HORSEPOWER

X 15'	Scale=0.50	4881	5154	5211		2914	2814	2707	1134	1055	948
Front: 12' X 15'	Scale=0.75	4822	5168	5195		2965	2832	2641	1181	1072	926
	Scale=1.0	4849	5099	5133		2957	2861	2670	1184	1062	949
121	Scale=0.50	4733	5232	5227	•	2954	2828	2623	1177	1028	954
Front: 12' X 12'	Scale=0.75	4805	5081	2100		2931	2838	2629	1161	1040	962
(L)	Scale=1.0	4822	5072	5205		2943	2862	2656	1111	1011	955
	Pressure	400	009	800		400	009	800	400	009	800
	GTHP		16421				8526			1684	

TABLE XI

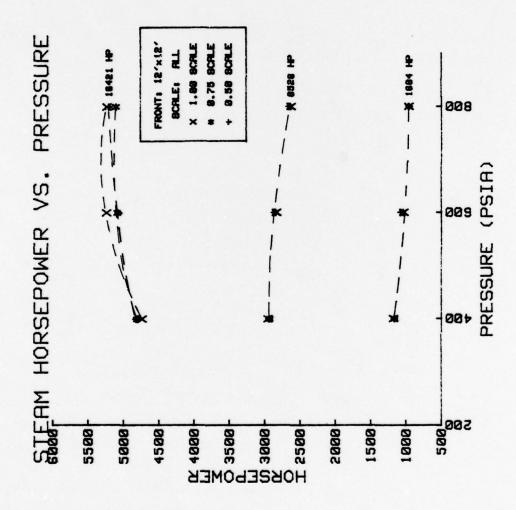


FIGURE 20

COGAS SYSTEM HORSEPOWER

X 15'	Scale=0.50	20974	21272	21318	11306	11205	11098	2796	2717	2610
Front: 12' X 15'	Scale=0.75	20949	21269	21287	11351	11218	11029	2843	2734	2618
	Scale=1.0	20956	21181	21205	11336	11239	11049	2846	2724	2611
12!	Scale=0.50	20831	21286	21267	11328	11201	10999	2839	2690	2616
Front: 12' X 12'	Scale=0.75	20874	21112	21116	11296	11201	10996	2822	2701	2623
	Scale=1.0	20861	21066	21162	11297	11211	11013	2832	2733	2616
	Pressure	400	009	800	400	009	800	400	009	800
	GTHP		16421			8526			1684	

TABLE XII

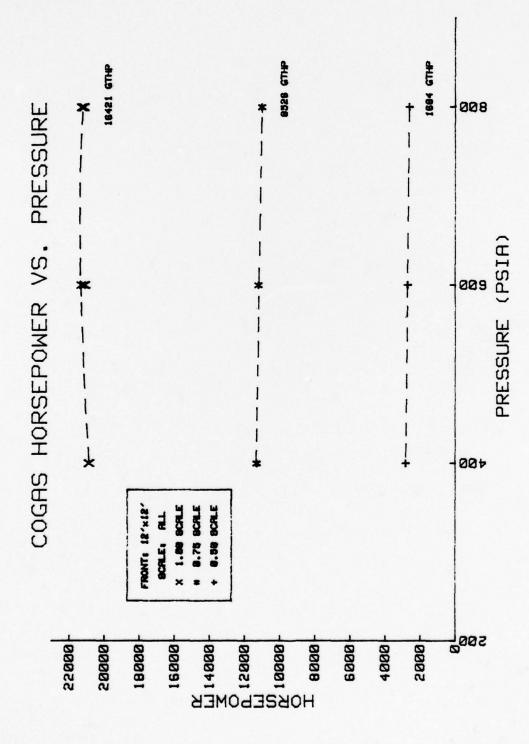


FIGURE 21

apparent that the system horsepower output trend followed that for steam turbine horsepower output. This was the expected result. This trend is modified only slightly by additional gas turbine horsepower losses due to a changing gas-side pressure drop across the WHRU.

Finally, the system specific fuel consumption followed closely the results for steam turbine horsepower output. That is, slightly better systems were observed at lower pressures for the medium and low gas turbine input powers and a slightly better system was produced at higher pressures for the high gas turbine input horsepower. These trends are shown in Figure 22 and Table XIII.

Effect of Gas Turbine Input Power.

An increase in WHRU height with increasing gas turbine input power was noted in the results for the design set produced (see Fig. 23 and Table III). This increase in WHRU height generally followed the increase in WHRU heat transfer rate with increasing gas turbine input power, Fig. 24. This trend is modified only by a slightly increasing outside heat transfer coefficient with increasing gas turbine input power (see calculations for gas-side heat transfer coefficient in the model description).

As expected, the COGAS system specific fuel consumption improved (Fig. 25) with increasing gas turbine input power. This improvement represents the trend of improvement in the gas turbine itself with increasing power, since the

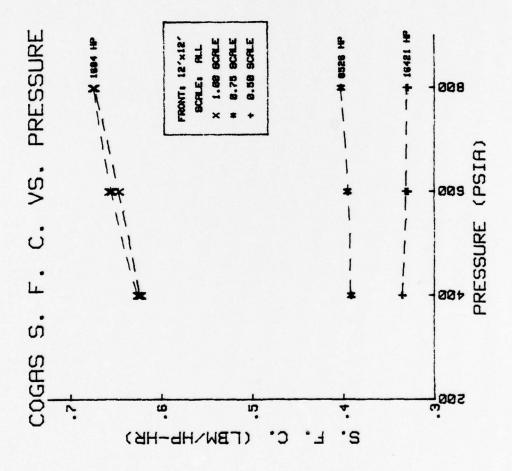


FIGURE 22

COGAS SPECIFIC FUEL CONSUMPTION

Front: 12' X 15'	Scale=0.50	.334	.329	.329	.392	.396	. 400	.632	.650	.677
	Scale=0.75	.335	.329	.329	.391	.395	.402	.621	.646	.675
	Scale=1.0	.334	.331	.330	.391	.395	.401	.621	.648	.677
121	Scale=0.50	.336	.329	.329	.391	.396	.403	.622	.657	.675
Front: 12' X 12'	Scale=0.75	.335	.331	.331	. 392	.396	. 403	.626	.654	.673
표]	Scale=1.0	.335	.332	.330	.392	.395	.402	.624	.646	.675
	Pressure	400	009	800	400	009	800	400	009	800
	GTHP		16421			8526			1684	

TABLE XIII

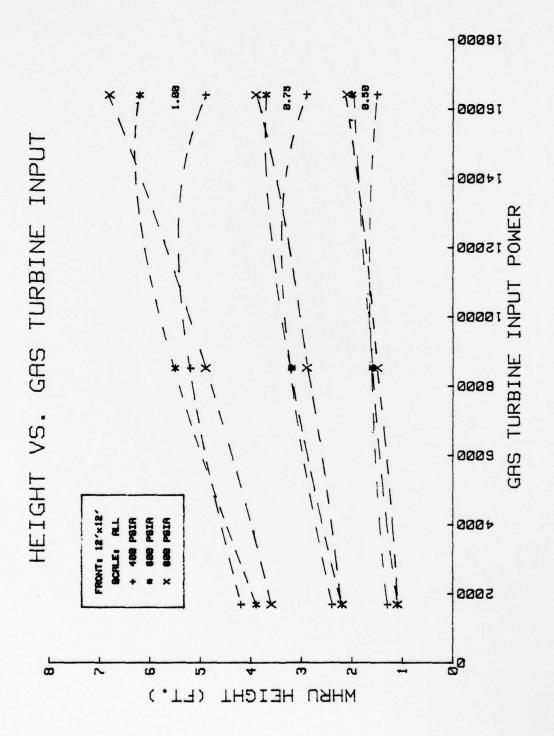


FIGURE 23

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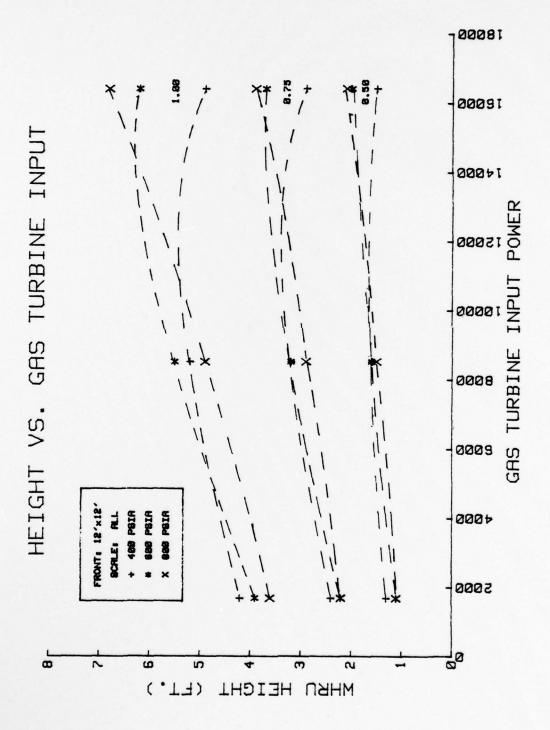


FIGURE 23

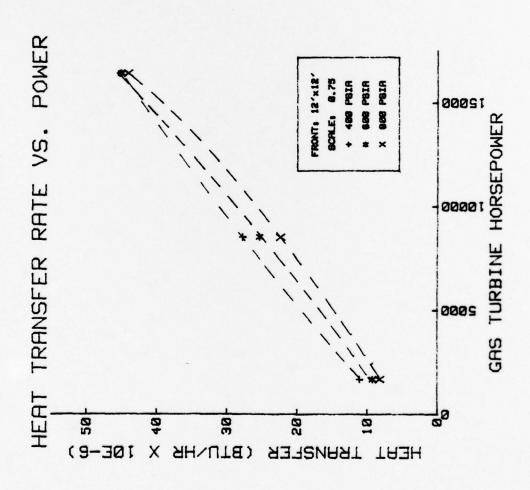


FIGURE 24

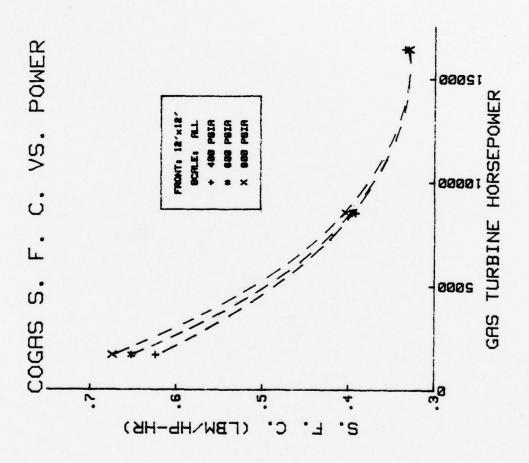


FIGURE 25

contribution of the steam system decreases with increasing power.

Effect of Frontal Dimensions.

The only significant trends for changing frontal dimensions were in WHRU height and volume (see Tables III and XIV). The expected result of decreased height with increased frontal area was observed. The gas-side pressure drop follows this decrease in height. The WHRU volume showed a significant increase for increased frontal area for all designs produced. This result is consistent with the model formulation. That is, as the frontal area is increased and the tube length is held constant the area for fluid flow is increased with a consequent decrease in Reynolds number and inside heat transfer coefficient. The same result is seen in the outside heat transfer coefficient. As the frontal area is increased, the minimum flow area for the gas is increased, causing a drop in the gas side Reynolds number and heat transfer coefficient.

D. OFF-DESIGN RESULTS

The off-design results were produced using the same computer simulation program used to produce the design set. The method used for off-design runs was described in Section F of the model description. As the computer program is presently designed, the designer must manually adjust the inputs to produce an off-design run. The procedure is reviewed briefly below.

WHRU VOLUME [ft³]

Front: 12' X 15'	Scale=0.50	270.0	324.0	360.0		270.0	270.0	270.0	198.0	198.0	180.0
	Scale=0.75	486.0	612.0	0.999		522.0	522.0	486.0	432.0	396.0	360.0
	Scale=1.0	828.0	0.066	1062.0		882.0	882.0	828.0	702.0	648.0	594.0
Front: 12' X 12'	Scale=0.50	216.0	288.0	302.4	•	230.4	230.4	216.0	187.2	158.4	158.4
	Scale=0.75	417.6	532.8	561.6		460.8	460.8	417.6	345.6	316.8	316.8
	Scale=1.0	705.6	892.8	979.2		748.8	792.0	705.6	604.8	561.6	518.4
	Pressure	400	009	800		400	009	800	400	009	800
	GTHP		16421				8526			1684	

TABLE XIV

First, the designer selects a WHRU design to be investigated at off-design conditions. Once this design has been selected, the pressure, frontal dimensions, height and scale of the WHRU are fixed. The designer then enters the gas flow rate and gas inlet temperature corresponding to the off-design point to be investigated. A design is produced with these gas conditions and the physical characteristics of the WHRU design under consideration. designer then checks the number of passes (height) for the resulting design. If the number of passes does not match that of the selected design, the WHRU gas outlet temperature and/or superheater steam outlet temperature are adjusted to increase or decrease the number of passes until a match is achieved. Once the physical characteristics of the offdesign point WHRU match those of the design-point WHRU, the gas inlet temperature is matched with the initial conditions, and the performance of the selected WHRU design is established for the off-design point under consideration.

In order to test the feasibility of the procedure described above and to demonstrate the off-design performance of a wide variety of WHRU designs, ten WHRU designs were selected for off-design runs. These designs are listed in Table XVI.

None of the full-scale designs was considered because the heights of the designs produced at that scale were, for the most part, either too large or borderline according to the space limitation described in Figure 9.

The results of these off-design runs are given in Table XVII. The summary output pages for each of these off-design runs along with the design-point runs are provided in Appendix D. In terms of specific fuel consumption, the performance difference between the design sets considered was not large. The performance range for fuel consumption is even less significant. Table XV demonstrates the performance range for the designs considered.

WHRU Off-Design Performance Ranges

Power	s.f.c.	<pre>fuel consump- tion (lbm/hr)</pre>	approx. fuel consump- tion difference (gal/hr)
high	.329340	6992.8 - 7019.3	3.9
medium	.391403	4429.2 - 4439.7	1.5
low	.615658	1764.6 - 1767.5	0.4

Table XV

Since the fuel consumption comparison showed very little difference between the ten designs considered and since all designs considered satisfied the dimensional constraints of figures 7, 8, and 9, only two designs were selected for additional off-design runs.

For these additional off-design runs, a pressure of 600 psia was selected. This pressure did not produce the smallest designs but it is a steam pressure with which the Navy has some experience in terms of materials requirements, maintenance, and operation. A scale of 0.75 was selected

WHRU DESIGNS CONSIDERED

Design Run #	Pressure	Scale	Front	Design Power	Height
5	800	.75	12x12	med	2.9
14	600	.75	12x12	med	3.2
16	600	.50	12x12	high	2.0
22	400	.75	12x12	high	2.9
24	400	.75	12x12	low	2.4
35	800	.50	12x15	med	1.5
40	600	.75	12x15	high	3.4
41	600	.75	12x15	med	2.9
53	400	.50	12x15	med	1.5

TABLE XVI

WHRU OFF-DESIGN RESULTS

Fuel	6999.1 4431.4 1765.4	7003.1 4430.1 1765.2	6992.8 4429.7 1765.8	7009.1 4429.2 1766.6	7004.3 4439.2 1766.4	6997.5 4439.7 1765.6	7001.9 4431.1 1764.6	7019.3 4432.3 1767.5	6999.3 4435.6 1767.1
Steam	800	009	400	400	800	009	009	400	009
Gr s.f.c.	.398	.387 .478 .858	.396 .479 .857	.401 .481 .860	.394	.387 .478 .860	.392 .479 .863	.393 .478 .853	.395 .479 .864
COGAS s.f.c.	.337	.329 .391	.335 .394 .620	.340 .400	.334	.329	.332 .395	.334 .392 .615	.334 .396 .632
盘	20769 10996 2683	21286 11331 2838	20874 11243 2848	20615 11073 2822	20971 11098 2705	21269 11297 2825	21090 11218 2801	21016 11307 2874	20956 11201 2796
Height	2.9	2.0	2.9	2.4	1.5	3.4	2.9	1.5	3.2
Front/Scale	12x12.1 .75	12×12 .50	12x12.1 .75	12x12.1	12x15	12x15.2 .75	12x15.2 .75	12x15	12x12.1 .75
GT Power	16421 8526 1684								
Run #	4(0) 5 6(0)	16 17(0) 18(0)	22 23(0) 24(0)	22 (0) 23 (0) 24	34 (0) 35 36 (0)	40 41(0) 42(0)	40 (0) 41 42 (0)	52 (0) 53 54 (0)	13(0) 14 15(0)

TABLE XVII

which yields a tube outside diameter of 1.5 inches and a fin spacing of about 8 fins/inch. The rationale for this selection was that a scale of 0.50 with 1.0 inch OD tubes and a fin spacing of 12 fins/inch would probably be too susceptible to both inside and outside fouling. In order to achieve the closest possible comparison, the design-point for both designs selected was for the gas conditions corresponding to the medium (8526 BHP) gas turbine input horsepower. Both frontal areas were used for these detailed off-design runs. Table XVIII summarizes the characteristics of the two designs selected.

Final Design Characteristics

design run #	GT input design point	scale	front	pressure	height
14	8526	0.75	12 x 12	600	3.2
41	8526	0.75	12 x 15	600	2.9

Table XVIII

Table XIX summarizes the performance results for the COGAS system with the 12' x 12' front WHRU and Table XX gives the results for the system with the 12' x 15' front WHRU. In both cases, the performance characteristics of the gas turbine alone, at the COGAS system horsepower, are provided for comparison. The summary output pages for each of these runs are provided in Appendix E.

PERFORMANCE OF 12'x12' FRONT WHRU

TABLE XIX

PERFORMANCE OF 12'x15' FRONT WHRU

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Steam	40.7	38.9	36.9	33.5	31.2	28.4	27.6	25.2	25.8	25.9	24.3	23.6	23.3
GT fuel use (at COGAS HP)	2418.9	2536.6	2634.3	3158.8	3639.4	4100.7	4769.3	5373.6	6195.5	6916.9	7566.7	8259.9	11844.5
COGAS fuel use	1776.2	1910.7	2043.1	2571.1	3018.3	3404.5	3892.0	4434.8	5088.5	5640.5	6165.9	7006.4	8186.2
GT s.t.c. (at COGAS HP)	.863	.829	.801	.672	.589	.545	.505	.479	.449	.431	.423	.392	.463
COGAS s.f.c.	.630	.624	.621	.551	.489	.452	.412	.395	.369	.352	.345	.332	.320
COGAS	2802	3061	3290	4681	6175	7530	9440	11218	13808	16038	17889	21085	25582
GTHP (input)	1684	1895	2105	3158	4316	5474	6947	8526	10421	12105	13790	16421	20000

TABLE XX

The specific fuel consumption curves vs. brake horsepower for the 12' x 12' front and the 12' x 15' front are
plotted in figures 26 and 27 respectively. The difference
in s.f.c. performance between the two WHRW designs considered was not significant. Geometric considerations were
therefore used in selecting the better of these two designs.
A geometric comparison of the two WHRU designs is given in
Table XXI.

Geometric Comparison of the Final Two Designs

Front	Frontal Area	Height	Volume	Total Out- side Area
12' x 15'	181.9	2.9	528.96	49586.4
12' x 12'	144.8	3.2	464.64	42776.5

Table XXI

It was concluded that, since both designs met the height constraint of figure 9, the 12' x 12' front was the better choice because of the significantly lower volume and total outside area requirements.

After the selection of the 12' x 12' front WHRU as the final design, estimates were made of the possible COGAS fuel savings for a DD-963-type destroyer over 1000 hours of operation. The NAVSEC Standard Destroyer Profile (Fig. 28) was used to determine the number of hours a destroyer-type ship spends at each speed during 1000 hours operation.

FIGURE 26

FIGURE 27

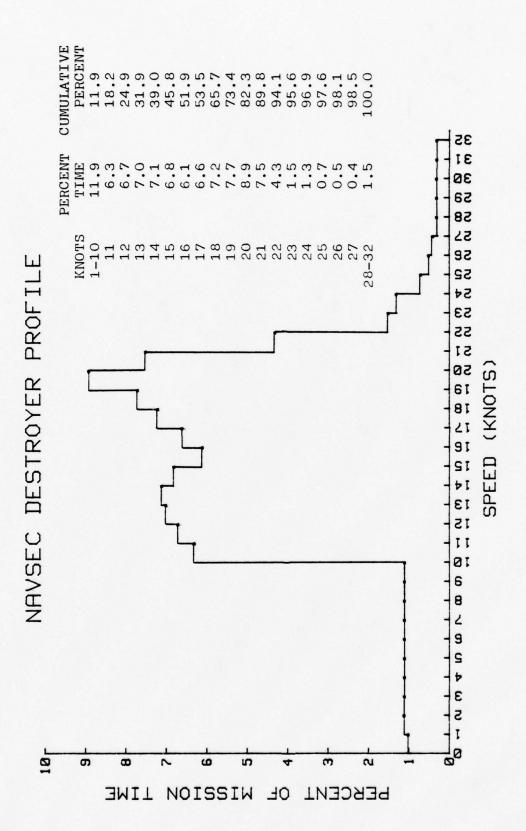


FIGURE 28

Figure 29 was used to obtain the shaft horsepower requirements for each speed. Finally, figure 30 was used to obtain the s.f.c. of the gas turbine operating alone.

Two estimates of fuel savings were made. The first estimate assumed that the COGAS system would be operated for speeds of 5 to 20 knots and would be secured outside that range. The second estimate employed the COGAS system for speeds of 5 to 23 knots. For the latter operating range, the criterion for the high COGAS speed was an imposed maximum gas turbine horsepower input of 20000 BHP. Both fuel savings estimates are based on the following assumptions and simplifications:

- 1. The COGAS mode of operation implies the use of one engine (COGAS mode) on one shaft with the other shaft dragging.
- 2. The gas turbine is assumed to operate at idle (1000 BHP) at speeds below 8 knots.
- 3. Maneuvering combinations, when two main engines would normally be on the line, are not considered.
- 4. In the speed range of 21 to 27 knots, in the pure gas turbine mode, one engine per shaft is used, with two shafts on the line.
- 5. From 28 to 32 knots four gas turbines are on the line.

 Table XXII provides the estimates of s.f.c. and fuel

 consumption for COGAS between 5 and 20 knots and for pure

 gas turbine for all speeds. The total estimated fuel savings

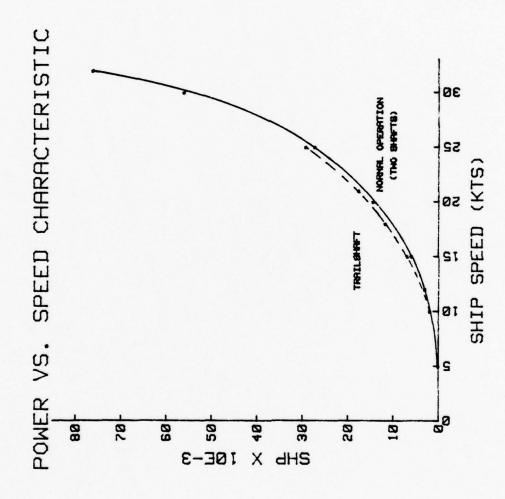
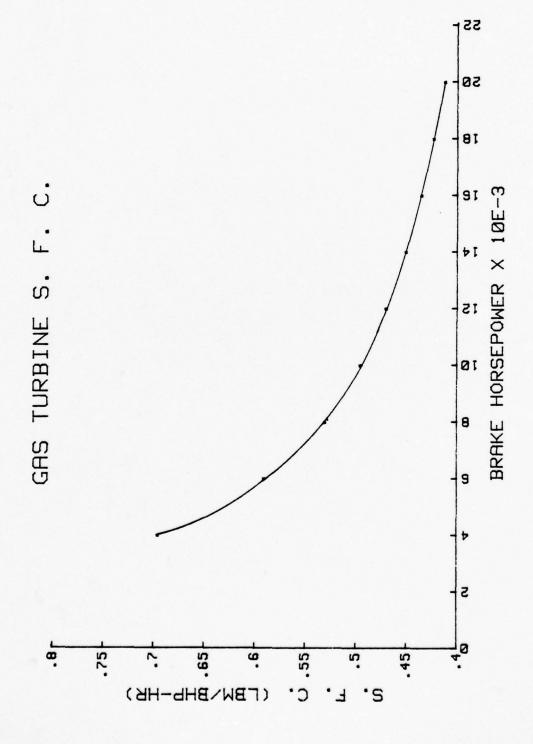


FIGURE 29





COGAS PERFORMANCE: 5 to 20 KNOT RANGE

Speed	Hours	ВНР	COGAS s.f.c.	GT s.f.c.	COGAS	GT CONS
1	10					17510
2	12.1					21187
3	12.1					21187
4	12.1	GT	est. avg.	est. avg	•	21187
5	12.1	IDLE at	.800	1.751	9680	21187
6	12.1	1000			9680	21187
7	12.1				9680	21187
8	12.1				9680	21187
9	12.1	1684	.750	1.100	15282	22414
10	12.1	1895	.705	1.070	16165	24534
11	63	2105	.680	1.000	90178	132615
12	67	3158	.618	.820	130760	173500
13	70	4316	.560	.700	169187	211484
14	71	5579	.512	.610	202808	241626
15	68	7368	.460	.550	230471	275563
16	61	8947	.426	.515	232497	281070
17	66	10421	.400	.489	275114	336327
18	72	12316	.380	.460	339666	407906
19	77	14210	.365	.440	399372	481435
20	89	16526	.350	.433	514785	636862

TABLE XXII
Page 1

Speed	Hours	ВНР	COGAS s.f.c.	GT s.f.c.	COGAS	GT CONS
21	75	17368		.519		676049
22	43	20000		.495		425700
23	15	22105		.482		159819
24	13	25263		.463		152058
25	7	28684		.448		89953
26	5	32631		.435		70972
27	4	37895		.418		63360
28	3	44210		.482		62928
29	3	51580		.460		71180
30	3	58947		.444		78517
31	3	69474		.427		88996
32	3	78947		.415	4774897	98289 5429976

12.1% savings
over 1000 hrs operation
655088 lbm savings

or 96336 gal. dist. fuel

TABLE XXII
Page 2

over 1000 hours of operation was 12% which is roughly equivalent to 96000 gallons of distillate fuel.

The estimates of s.f.c. and fuel consumption for pure gas turbine and for COGAS for the 5 to 23 knot speed range are given in Table XXIII. The total estimated 1000-hour fuel savings for this COGAS operating range was 19% which translates to approximately 152000 gallons of distillate fuel.

E. CONCLUSIONS

The waste heat recovery unit model and the accompanying simple COGAS system output model provide the basic framework for additional studies of the application of the COGAS system to U. S. Navy gas turbine powered ships. The model, as presently formulated, provides a reasonable estimate of WHRU size required for the fin-tube configuration considered.

Estimates of the COGAS system performance in the 5 to 20 knot range and the 5 to 23 knot range are encouraging. Even considering the assumptions involved in making the fuel savings estimates, it is likely that a COGAS version of a DD-963-type ship would consume on the order of 300000 to 450000 gallons less fuel in one year of operation than the current DD-963 class ships.

The most probable COGAS system would be one which would be designed to operate in non-maneuvering situations for either speed range considered above. That is, a system which would be employed for maximum fuel savings in the cruise mode.

COGAS PERFORMANCE: 5 t0 23 KNOT RANGE

Speed (kts)	Hours	ВНР	COGAS s.f.c. (1bm/ hp-hr)	GT s.f.c. (1bm/ hp-hr)	COGAS CONS (1bm)	GT CONS (1bm)
1	10					17510
2	12.1					21187
3	12.1	OT TOLD	TCT 1170	DOM 1170		21187
4	12.1	GT IDLE at	.800	1.751		21187
5	12.1	1000			9680	21187
6	12.1				9680	21187
7	12.1				9680	21197
8	12.1				9680	21187
9	12.1	1684	.750	1.100	15282	22414
10	12.1	1395	.705	1.070	16165	24534
11	63	2105	.680	1.000	90178	132615
12	67	3158	.618	.820	130760	173500
13	70	4316	.560	.700	169187	211484
14	71	5579	.512	.610	202808	241526
15	68	7368	.460	.550	230471	275563
16	61	8947	.426	.515	232497	281070
17	66	10421	.400	.489	275114	336327
18	72	12316	.380	.460	339666	407906
19	77	14210	.365	.440	399372	481435
20	89	16526	.350	.433	514785	636862

TABLE XXIII

Page 1

Speed	Hours	ВНР	COGAS s.f.c.	GT s.f.c.	COGAS	GT CONS
21	75	18421	.340	.519	469735	676049
22	43	20842	.335	.495	300229	425700
23	15	23368	.324	.482	113568	159819
24	13	252263		.463		152058
25	7	28684		.448		89953
26	5	32631		.435		70972
27	4	37895		.418		63360
28	3	44210		.482		63928
29	3	51580		.460		71180
30	3	58947		.444		78517
31	3	69474		.427		88996
32	3	78947		.415		98289
			Totals:		4396861	5429976
			1		19.0% savings	
			fuel	. saved i	n 1000 hrs	operation
					1033115 lbm	
			or		.51928 ga.	dist. fuel

TABLE XXIII

Page 2

During maneuvering and high speed operations the gas turbines would be operated alone with the waste heat recovery unit dry. Because of the relatively low gas turbine exhaust temperatures involved, it is not expected that damage would occur in the WHRU when operated dry.

IV. RECOMMENDATIONS FOR FURTHER RESEARCH

A. WHRU DESIGN MODEL IMPROVEMENT AND EXPANSION

The type of control imposed on the WHRU design model of this thesis was essentially the adjustment of the steam flow rate to maintain a superheater steam outlet temperature of 650 F at the pressure specified. This steam flow rate control was further extended to accommodate the maintenance of a minimum pinch point ΔT of 25 F. Further investigation of WHRU design should include the effects of allowing the superheater outlet steam temperature and/or pressure to "float" with changing gas turbine exhaust conditions. The combination of controls on the superheater outlet pressure, temperature, and flow rate could lead to improved WHRU output while still maintaining an acceptable minimum pinch point temperature difference.

In order to increase the precision of the model and lead to increased knowledge of the gas temperature distribution in the WHRU, the present model could be modified for a "fine mesh" approach. That is, instead of solving one pass at a time, each pass could be divided into a number of segments. The solution could then proceed using either the finite difference or finite element method.

Other possible model improvements are as follows:

 Include the calculation of fluid/steam-side pressure drop.

- 2. Additional fin-tube configurations should be considered for possible improvement of the heat transfer characteristics and the weight and space requirements of the WHRU.
- 3. Consideration of inside and outside heat transfer surface fouling should be given when investigating possible fin-tube configurations.
- 4. Working fluids other than water should be investigated for possible enhanced thermodynamic characteristics at a minimum cost in system maintainability.

B. COGAS MODEL IMPROVEMENTS

After the waste heat recovery unit, the steam turbine and condenser should have the highest priority for modeling. Both of these units were modeled as "black boxes" in this model. The modeling or performance mapping of "state of the art" steam turbines for application in the COGAS model would allow the designer to further refine the estimate of system performance for various WHRU outputs of steam temperature, pressure, and flow rate. The inclusion of a steam turbine model would also allow the designer to make size and weight estimates for that component. The same benefits would be derived from the inclusion of a condenser model in the COGAS system. As the condenser pressure is reduced, the system performance should improve. The improvement must, however, be weighed against the increased condenser size necessary at the reduced pressure for constant steam and cooling water

conditions. A condenser model would allow the designer to make these comparisons.

In the model of this thesis, pumping power for the condensate and feedwater was assumed to be negligible. In the case of the condensate pump, this is probably not a bad assumption since it is likely that electric pumps could be used, and the cost to the ship's electrical output would not be large. The feedwater pump, however, would probably be steam turbine driven at some cost to the COGAS system output. The required feed pump pumping power for various loads should be mapped and included in the model.

Finally, the likely engineroom machinery layout for the COGAS system should be described in enough detail that the lengths of piping runs, number of turns, and location of valves could be estimated. The inclusion of this feature in the model would allow the designer to address pressure drop and heat losses between components. This feature would also contribute to the COGAS system weight and space prediction.

C. SYSTEM OPTIMIZATION

Since the COGAS system is operated with a relatively small heat source, optimization should be attempted in the design of the system. The technique of non-linear programming could be applied to a COGAS system optimization where an important system output parameter, say specific fuel consumption, is expressed as a function of the system design

variables such as component weight, component dimensions, and gas turbine backpressure. This function is called the objective function, and it is maximized or minimized subject to constraints which are also expressed as functions of the design variables. These constraint functions may be either linear or non-linear and express some parameter limit not to be exceeded, such as WHRU or condenser total volume.

For a system of the complexity of the COGAS system a "local" optimization appro would probably have to be adopted. That is, each of the major sub-models (WHRU, steam turbine, and condenser) could be optimized using local constraints. Then the entire system could be optimized using linking variables, such as enthalpy, flow rates, and temperatures between components. The process would be repeated as many times as necessary to achieve the final system optimization. One available computer-based system using the technique of non-linear programming is the COPES/CONMIN program [Ref. 14].

APPENDIX A MAIN PROGRAM LISTING

ESTABLISHES GAS FLOW, INPUT S AND DIMENSIONS OF SCALE, NUMBER T IME I NPUTS CALCULATES GAS TEMP. IN STEAM TEMP. CUT. AND NECESSARY FOR THE SUPERHEATING SECTION OF THE WATER TEMP. CUT, AND SECTION OF THE HEAT THIS PROGRAM IS THE MAIN, OR CALLING, PROGRAM IN A SET OF PROGRAMS USED TO DESIGN A ONCE-THROUGH WASTE HEAT EXCHANGER TO PROVIDE STEAM FOR A COMBINED GAS AND STEAM (COGAS) PROPULSION SYSTEM. THE FOLLOWING SUBPROGRAMS ARE USED IN CONJUNCTION WITTHE MAIN PROGRAM. GIVEN ENTHALPY 캶 SUBROUT IN E OPTM: ADJUSTS HEAT EXCHANGER GAS OUTLET TEMP. IN ORDER TO MATCH GAS INLET TEMP. TO THAT ORIGINALLY SPECIFIED. SUBROUTINE FINE: CALCULATES FIN EFFICIENCY GIVEN GEOMETRIC FROM GEOI AND GIVEN CURRENT HEAT TRANSFER CCEFFICIENT. DUTPUT SUBROUT INE BOILL: CALCULATES GAS TEMP. IN, STEAM QLALITY AND NUMBER OF PASSES NECESSARY FOR THE BOILING SECTION OF HEAT EXCHANGES. SIGNER GIVEN INPUTS OF GAS TEMP. IN AND OLT, STEAM TEMP. OUT, STEAM PRESSURE. SUMMARY PE RUN C SUBROUTINE GEOT: CALCULATES ALL NECESSARY AREAS FOR A FIXED FIN-TUBE CONFIGURATION GIVEN INFUTS OF TUBES PER ROW, AND TUBE LENGTH. ш CALCULATES TEMPREATUR ONE-PAGE, OFF-LINE AS TEMP. INT · • 67 COMPUTER DES,OPT INTERACTIVE AND OF THE IBM 360-6 THE TERMINAL. CALCULATES G NECESSARY FOR PRODUCES ED, DD, NDR SUBROUT INES TEMP/TEMP1: AND PRESSURE. IMPLICIT REAL*4(L LOGICAL OPA,OP, RE SUM=. FALSE. OPT=. FALSE. SUBROUTINE SUPI: NUMBER OF PASSES HEAT EXCHANGER. SUBRDUTINE HBAL: STEAM FLOW RATE WATER TEMP. IN, SUBROUTINE SATI: NUMBER OF PASSES EXCHANGER. FOR EACH DE SIGN HE PROGRAM IS FAR ING SYSTEM FE PROMPTEC AT

*

00=.FALSE. 6C=4.1538E8 PITM=2116.368 TCM=26. FI=3.1416 FFI=025 RR=53.34 RCONV=459.69 FFT=025 CS=00T= FALSE. WRITE(690) FORMAT(10°, SUPRESS ALL OUTPUT?!) FORMAT(10°, GEOMETRIC SCALING?!) "IS THIS A DESIGN RUN?")
DES ENTER GT HORSEPOWER. 1) SHIP SPEED. 1) ENT ER SSPD GC=4.1538E8 PATM=2116.368 FCM=26.16.368 FF1=.3 FF0=.98 FFT=.025 RCONV=459.69 PP=25. WRITE(6.198) FCRMAT(100'ENT FCRMAT(61196) FCRMAT(61196) FCRMAT(61196) FCRMAT(61196) (68.1) (61196) (5,1195) CNSTANTS 198 161 961 56 92 96 16 46

```
TGB1=(TG3+TG4)/2.
DPGT=0.
TGF1=TGB1
CALL SATI(GG,GF,TGF1,TGB1,EFFSA,TF2,TFB1,TCM,FG,PF1,TG3,TG4,TF1,
XR,TWO,GGM,LT,UF,DI,HDSAT,DPA,SCALE,IPSA,DPT,ANTR,L,SUM,REFS)
                                  CALL HBAL(TG1,TG2,TG3,TG4,TF1,TF2,TF3,TF4,GG,GF,OPA,PF1,OPT,

XOD)

TG1P=TG1

TG2P=TG2

TG3P=TG3

TG4P=TG4

TF1P=TF1

TF2P=TF2

TF3P=TF3

TF4P=TF4
                                                                                                                                                                                                                                                                                                                                                               CALL BOIL1(GG, GF, TG2, TG3, TF2, TF3, TFB, TGF, FG, PF1, HF3, X3, TGB, XTW0, GGM, R, OPA, SCALE, IPB, OPT, TGIBI, AIH, SUM)
                                                                                                                                                                                                                              VGW=VISG(TWD)
VGB=VISG(TGB1)
TGFR=TGF1+RCONV
VCLG=RR*TGFR/PATM
VCLG=RR*TGFR/PATM
DFG=12.*FGFR/PATM
DFG=12.*FGFR/PATM
DFG=12.*FGFR/PATM
DFG=12.*FGFR/PATM
DFG=12.*FGFR/PATM
DFG=12.*FGFR/PATM
DFG=12.*FGFR/PATM
DFG=14.00.70.24
WRITE(6,150) DFG
FORMAT(00.70.7F2=1,F6.2)
FORMAT(10.70.7F2=1,F6.2)
                                                                                                                                        CALCULATIONS FOR SATUFATOR
                  MAKE INITIAL CALCULATIONS
                                                                                                                                                                                                                                                                                                                                              CALCULATIONS FOR BOILER
                                                                                                                                                                                                               GAS SIDE PRESSURE DROP
                                                                                                                                                                                                                                                                                                                                                                                          GAS SIDE PRESSURE DRUP
                                                                                                                                                                                                                                                                                                                                                                                                                                        Σ
                                                                                                                                                                                                                                                                                                                                                                                                            V GW=V IS G(TWD)
VGB =VI SG(TGB)
T GFR =T GF +R C GNV
V CLG=RR*T GFR/PAT
FORM AT ( F4 . 1 )
26
C
C
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                                                                                                                                                                                                                                                                                                                          25005
                                                                                                                               2002
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COC

EXERTER REPORT OF COLUMN REPORT OF COLUM CALL HBAL (TGIP, TG2P, TG3P, TG4P, TF 1P, TF 2P, TF 3P, TF 4P, GG, GF, OPA, PF1, XCFT, OD)
TG 1= TG1P
TG2= TG2P
TG3= TG3P
TG4= TG4P
TF 1= TF1 P
TF 2= TF2P
TF 2= TF3P
TF 2= TF3P
TF 2= TF3P CALL SUPI(66,6F, TG1, TG2, TF3, TF4, FG, PF1, X3, HFCUT, TGINS, XTGB, TWO, TGF, GGM, OPA, SCALE, IFR, IPS H, TG1, TF4, CPT, IPT, IPB, IPSA, XAIB, SUN, R, R, EFSH, REPERFORM INITIAL CALCULATIONS WITH NEW GAS TEMP. OUT VGW=VISG(TWC)
VGB=VISG(TGB)
T (FR=TGF+RCONV
VCLG=RR*TGFR/PATM
VCLG=R*TGFR/PATM
VCLG=C, *FG*GGM**2*R*VOLG/GC)*(VGW/VGB)**.14
DPGT=D GT*DPGT/144*)
DPGT=27.7*(DPGT/144*)
MR ITE(6.190) 3PG
IFT=IPSA+IPE+IPSH
IF(0PT) GG TG 29 DPG=(2.*FG*GGM**2*R*VOLG/GC)*(VGW/VGB)**.14
DFGT=DPGT+DFG
IF(DPA) GO TO 26
WRITE(6,190) DPG
FCRMAT('0','DPG=',F5.1) MRITE(6, 192)
READ(5, 52) OPT
READ(5, 52) OPT
I F (.NOT .0PT) G3 T0 28
CALL OPTM(15) FTG1, FG4P, CS, OK, TINC)
WRITE(6, 1000) FG1P, TG4P
FGRMAT(10, 2F7, 1)
I F (OK, EQ. 0.) 30 T0 28 CALCULATIONS FOR SUPERHEATER GAS SIDE PRESSURE DROP MATCH GAS TEMP. IN 1000 192 58 COC COC

```
SUBROUTINE HBAL (TG1,TG2,TG3,TG4,TF1,TF2,TF3,TF4,GG,GF,OPA,PF1,OPTX))
                                                                           CALL POWER(PF1, TF4,GF, DPGT, HPGT, PT, HPTO, STS, GTSFC, XOASFC, SFCT, GTTH, OATH, THT, ET, PCON, PHTR)
WRITE(6,203)
FORMAT(10,1)SUMMARY OUTPUT?
READ(5,204)SUM
FORMAT(14)
FORMAT(14)
                                                                                                                                                                                                      WRITE(6,300)
FORWAT('0', ENTER INITIAL CONDITIONS')
WRITE(6,301)
               CALCULATE COGAS SYSTEM DUTP UT
                                                                   SLMMARY OUTPUT FOR THE RUN
                                                                                                                                                                                            STARTING CONDITIONS
                                                                                                                                                                  1061CAL OPA, NPT, OC
PP=25.
TF1=200.
IF(OPT) GO TO 2
60 TO 20
HP GT 0= HP GT
                                          203
                                                    204
                                                                                                                   201
                                                                                                                                                                                                            300
                                                                                                                                                                                                                       301
                                                                                                                                                                                                                                                      304
                                                                                                                                                                                                                                 302
                                                                                                                                                                                                                                            303
                                                                                                                              40
```

INTERMEDIATE TEMPERATURES/HEAT TRANSFER RATES OVERALL HEAT TRANSFER/FLUID FLOW RATE CALCULATE GAS AND WATER PROPERTIES T GB= (T G1+T G4)/2. C PG=SPECG (TGB) CALL HCW(PF 1, TF 1, HF 1) CALL SS (PF1, F4, HF4, SS 4, VOL F4) WRITE(61305)
FORMAT(1001 GAS FLOW RATE?!)
READ(51306)
FORMAT(F8.1)
TF1=200
WRITE(61307)
FORMAT(1001 TF4?!)
READ(51308)
FORMAT(1001 PF?!)
FORMAT(1501 PF1) TF3=TF2 CALL SS(PF1,TF3,HF3,SSS,VOL) OB=GF*(HF3-HF2) TG2=(QB+GG*CPG*TG3)/(GG*CPG) QMAX=GG*CPG*(TG2-TF2) EFFB=QB/OMAX GF=Q/(HF4-HF1) TF2=TSL(PF1) TFB1=(TF1+TF2)/2. HF2=HSL(TF2) OSAT=GF*(HF2-HF1) CALL GF*(HF2-HF1) CALL GOTH(PF1-TFB T G3=(QST+GG*CPG* QMAX=GF*CPF1*(TG3 EFSA=QSAT/QMAX SUP ER HE A TER SATURATOR BCILER

10 10 10

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SLBROUTINE OPTM(TGIP,TGI,TG4P,CS,CK,TINC) LOGICAL CE OK=1. CHECK CURRENT GAS TEMP. IN WITH ACTUAL F4 HF4, SSS, VOL. PF 3) 7683,CP CALL SS(PF1, TF4 0SH=GF*(HF4-HF3 TFB3=(TF3+TF4)/ CALL COS(PF1, TF QWAX=GF*CPF3*(T EFFSH=QSH/QWAX SET PINCH PCINT DIF = TG 1P-TG 1 DIFA = ABS(DIF) IF(DIFA - LE - 1 - 5 IF(DIFA - LE - 8 -) IF(DIFA - LE - 8 -) 110 100 120 130 140

JUJ

CCC

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S

SUBROUTINE CUT(SUM, HPGTO, TG1P, GG, ANTR, L, IPT, IFSA, IPE, XAIH, IPS I, A IB, TG3, TG4P, TF IP, TF2, TG2, TG1B, TG1, XAIH, IPS I, A IB, TG3, TG4P, TF IPP, HPT C, STS, GT S FC, XA S FC, S FCT, GTTH, OA TH, TH T, SCALE, CD, ET, PCON, PHTR, REFS, REFSH, XS S PD)

XOA SFC, S CT, GTTH, OA TH, TH T, SCALE, CD, ET, PCON, PHTR, REFS, REFSH, XS S PD)

LOGICAL SUM, OD

P 1=3, 14, 16

CALL GE OIL ANTR, L, AMIN, DO, AFF, DI, AIP, ANTP, AOF, SN, SF, AFFR, OPA

X, SCALE, OPT, SUM, DFF, FPP, DFB, LABB, FINC, AFINT, LF, TF, AKRP)

HEI = (I PT * AN RP-I) * SP+OTF

DOI = DO*12.

L 11 = DI * 12.

F F 1 = FF / 12.

F F 1 = FF / 12.

F F 1 = AIB / (PI*DI*ANTR*2.)

B 1 = AIB / (PI*DI*ANTR*2.)

P 2 = T G IB I - TF 2.

P 2 = T G IB I - TF 2.

P 2 = T G IB I - TF 2. TGI, IPSA, IPB,

12001 110 ರಾಗಾ S

IF(CS.LT.0.) TINC =. 5*TINC TG4P=TG4P+TINC CS=DIF GO TO 20

INCREASE GAS TEMP DUT

DECREASE GAS TEMP. DUT

IF (CS. GT. 0.) TINC=.5 *TINC CS= DIF GO TO 20 OK = 0. GC TO 20 WRITE(6100) FORMAT(10. 'CLOSE ENDUGH?') FORMAT(10. 'CLOSE ENDUGH?') FORMAT(14) IF (CE) OK = 0. IF (CE) OK = 0. IF (CE) OK = 0. IF (CE) OK = 0.

CLOSE ENOUGH?")

WHIROUSSO EXERESE EXERES EXERCISES E PER PASS: 30) HPGT 0.5SPD"

1. 6X, BRAKE HORSEPOWER: ',2X,F7 1
PPROXIMATE CORRESPONDING SHIP SPEED: ',2X,F4.1,2X,'KTS') "IIX" TUBE/ FIN ARRANGEMENT: ", 35X, "INSIDE AREA /PASS:", TUBES TE(81140) TG1P. CULLES TUMBING SHIP SPEED: ',2X,F4.1,2X,' F1 1 6X, EXHAUST GAS TEMPERATURE: ',2X,F6.1,2X,' F1 1 1 6X, EXHAUST GAS FLOW RATE: ',2X,F8.1,2X,' LBM/HR', E18,160)
E18,160)
AT(//2X,' HEAT EXCHANGER GECMETRY')
E18,170) ANRP
E18,170) ANRP
E18,170) ANRP E(8:110) AT ('11',45x, 'WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN') E(8:120) AT(///2x,'GAS TURBINE') E(8:130) HPGTO,SSPD 6X, "HEAT TRANSFER SURFACE")

1) DJI AOP
111X, OUTSIDE TUBE DIAMETER: ",2X, F4.1,2X, IN.",
DE AREA /PASS: ",2X,F7.1,2X, SQ.FT.!) E(8,186) L AT('',11X', LENGTH:',2X', F4.1,2X', FT.'') (8,190) W,A NTR (1,11X', WIDTH:',3X, F4.1,2X', FT.'',38X', NUMBER OF (8,195) HEI INSIDE TUBE DIAMETER: ,2X, F4.1,2X, 'IN.') (111,47x, WASTE HEAT RECOVERY UNIT DESIGN RUN!) (8 200) IAT (195) HEI E(8197) L AT (127, 420) TURBINE 1)
TO SSPD CONH= 2 . 04 *PC3 N SAT=TSL(PF1) FORMATION THE CONTROL OF CONTROL X TETERONE TOOOT TOOOT TOOOT TOOOT TOOOT TOOOT TOOOT TOOOT TOO WAIT TO RM 180 130 140 150 091 170 200 210 230 2252 190 220 195 161

Y

WHR 04 BLO WEITE (8 430) PT PCONH UNB INE HORSEPOWER: '2X,F7.1'

WHR 04820 WHR 04820 WHR 04820 RESURE: '2X,F4.2' ZX, '11'

WARTE (8 435) ET SESURE: '3.7.F4.2', ZX,F4.2')

WHR 04830 WHR 04850 WHR 04870 WHR 05020 WHR 0

CALL GEO1 (ANTR, L, AMIN, DO, AFF, DI, AIP, ANTP, AOP, SN, SP, AFR, OPA, XSCALE, OPT, SUM, DTF, FPF, DFB, LTAB, FINC, AFINT, LF, TF, ANRP)
IF (OP) GO TO 6
WRITE(6, 90) TGF
FORMAT(10, 1 TGF = 1 F7, 1)
CALL HCW(PF, TF1, FF1, FF1) GAS SIDE HEAT TRANSFER COEFFICIENT GAS SIDE REYNOLDS NUMBER (DO) PROGRAM FOR HEATING SECTION GGM=GG/AMIN VG=VISG(TGF) VG=VG**.00036 REG=(GGM*D0)/VG IF(OP) GO TO 7 WRITE(61100) REG FORMAT(100, 'REG=',F8.1) (6 90) TGF T(00' TGF=' F7.1) HCW(PF,TF1, FFIN) CALL SEGS1(REG, CJ, FG) SATURATOR GEOMETRY FORMAT (10. F7.1)
TGB=[TG3+TG4) /2. WAITE (6,90) TGF TFB=(TF 1+TF2)/2.

SOU

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2

100

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85

46

SOU

PASSES REQUIRED ARG**N-C) -CMAX*TG4)/(EFF*CMIN-CMAX) FF 2) / 2. (HC*TAI) / (HG*TAD)) * (TGB-TFB) TO 14 WALL TEMP.=", F7.2) OF S ATURATOR EFFECT IVENESS/NUMBER 'PASS EFF. = , F4.31 NO. PASSE S=' ,12) ARG=(1.-EFFP*C)/(1.-EFFP)

DC 10 N=1,15

TF2S=TF2T

TGS=TGI

EFFS=EFF

IP=N

EFF=(ARG**N-1.)/(ARG**N-C)

TGI=(EFF*CMIN*TFI-CMAX*TG4)

DC=G&CPG*(TGI-TG4)

HF0=HFIN+QL/GF

TF2T=TF2-5

CONTINUE
IF(TF2T*GT*TF2) GQ TO 15

CONTINUE
IF=EFFS

TF2=TF2S

TF3=TGIS

R=ANRP*IP

TAI=IP*AIP B=(EXP(A) EFFP=1 -E IF(OP) GO WRITE(6) FORMAT(10 DIFA=ABS/ IF(DIFA-1 TCF=TGF+1 GO TO 5 IF(OPA) WRITE(6 FORMAT(14000E 630 20 160 150 10

1 TO 95 (0) HEI, VOLSA , SAT. HEIGHT=", F4.1, 4X, SAT. VOLUME=", F8.2) (REG, CJ, FG) 8-.00334741588638*ALDG(REG) -.0771218846786*ALDG(REG) SUBROUTINE FINE (FINC, HG, AOP, AFIN, EF)
C1=FINC *SQRT(HG)
C1N=-C1
TML=(EXP(C1)-EXP(C1N))/(EXP(C1)+EXP(C1N))
EF=TML/C1
WRITE(6,100) EF WRITE(6165) TG3 FORMAT(10', 'REVISED GAS TEMP. IN=',F5.1) LT=L*R HEI=SP*(R-1.)+DO VOLSA=HEI*AFR VOLSA=HEI*AFR IF(DPA) GO TO 95 WRITE(6,170) HEI, VOLSA FORMAT(10', 'SAT. HEIGHT=',F4.1,4X, 'SAT. \ ETURN

SUEROUT IN E TEMP 1 (PF, TFO, HFO)

TINC=10.

CALL HCW (PF, TFO, HTEST)

DIF=HFO-HTE ST

DIF=ABS (DIF)

IF (DIFA-LT. •5) GO TO 46

IF (DIFA-LT. •5) GO TO 45

IF (DIFA-LT. •0.) GO TO 45

IF (DIFI-LT. •0.) TINC=•5*TINC

TFC=TFO+TINC

DIFI=DIF
GO TO 40

RETURN

END SUBROUT INE SEGS1 C J=, 0396176C8371 F G= 1,08824815212-RETURN END 165 170 95 ပပပ 40 45 46 JUU SOO

SAT01930 SAT01940 SAT01950 SAT01960

FCRMAT ('0', 'FIN EFFICIENCY=', F5.3)
ET=1.-(1.-EF)*(AFIN/AOP)
HG=ET*HG
RETURN
END

CALL GEO! (ANTR, L, AMIN, DO, AFF, DI, AIP, ANTP, AOP, SN, SP, AFR, OPG

I F(NP) GO TO 81

NRITE (6,80) PF, TFO

FORMAT(00, PF=', F5.1,3X, TFO=', F6.2)

TCM=26.

C1=.66.

C1=.66.

A=3.46-4

B=6.7E3

A=AIP

CALL TCCW(PF, TFO)/2.

CALL TCCW(PF, TFO) TCL)

CALL TCCW(PF, TFO, TCL)

CALL TCCW(PF, TFO, TCL)

CALL TCCW(PF, TFO, TCL)

TCL=TCL*16-3 PROGRAM FOR BOILING SEC TION BUILER GEOMETRY

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BBQ 1000 BBQ CR = CD/ DI HOA = 1. / ((AI P* AL OG (DR) / (2.*PI*T C P* ANT P*L)) + (AIP/ AOP) * (1./HG)) OVERALL HEAT TRANSFER COEFFICIENT (ROUGH, NEGLECTING INSIDE) GAS SIDE HEAT TRANSFER COEFFICIENT 5.J, FG J=', F5.4,3X,' F=', F3.2 | F(DP) GO TO 8 |RITE(6,150) HOA |ORMAT(100, HO(ROUGH) = 1, F6.2) PF, TEO, VOLF 1 GAS SIDE RE WOLDS NUMBER S EGS 1 (REG, CJ, FG) PASS EFFECTIVENESS GIN+TGOU) /2 CM IN=CP 6*66

120

BB011001175000 BB011001175000 BB01100117500 CONDITIONS IN HEATING SECTION OF FIRST PASS OVERALL HEAT TRANSFER COEFFICIENT (HEATER) DI)*(REF **.8) *(PRF **.4) FLUID SIDE HEAT TRANSFER COEFFICIENT TGI(1)=(EFFP*TFI-TGO(1))/(EFFP-1. RCUGH GAS TEMP. INTO FIRST PASS ROUGH FIRST PASS HEAT TRANSFER ", PASS EFF.=", F4.31 OF(1)=66*CPG*(TGI(1)-TGO(1)) FLUID SIDE REYNOLDS NUMBER ... ULF ... (VOLF *VF *GC) , 'REF= , F8 . 1) TFBH, CPF) TCCW IP E, TEBH, TCF 'HF=' , F6.21 VI SCHITFBH , VF) TFBH (TF1+TF0) IF(0P) GO WRITE(6,16 FCRMAT(10 WR ITE(61) FCRMAT (10

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8011011450 () -1.) / (C*SN) (P(B1) FP*CMIN*TFI-CMAX*TGD(1))/(EFFP*CMIN-CMAX) CPG*(TGI(1)-TGO(1)) HOS AT=1 ./ ((1 ./ HF)+(A1 *ALOG(DR)/(2.*PI*TCM*ANTP*L)) X+(A1P/AOP)*(1./HG)) EFFH=ORH/(CMIN*(TGI(1)-TFI)) RA=.5 CMIN=CPF*GF CMAX=CPG*GG C=CMIN/CMAX AN=HOSAT* AIP/CMIN SN=AN**(-.22) A=-AN**(-.22) A=-AN**(-.22) A=-AN**(-.22) A=-AN**(-.22) A=-AN**(-.22) A=-AN**(-.22) A=-AN**(-.22) A=-AN**(-.20) A=-AN** INSIDE HEAT TRANSFER COEFFICIENT IF (XA(IP).GT..05) GN TO 2500 HTPF=HF IP= IP +1
ANTU=HO *A I P/ (CP G * G G)
EFFP=PA SSB (ANTU)
GF (IP) = (EFFP*TFO-TGO(IP)
QF (IP) = (CP G* G G) * (TGI (IP)-TFO(IP) + (TGI (IP)-TFO(IP SUES EQUENT FLUID PASSES

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190

5 00

189 CC 200 409 409

```
[P]=1
(IP), 1GI(IP), HFO(IP), X(IP), HC
 DI *GFA /( VI SL*GC) ) **. 81
2500
    3000
                             250
                               260
                                 270
                            240
                                   280
                   48
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X T GB .TWO.TINE SUPIGG. GF.TGIN, TGOU, TFI, TFO, FG, PF, X3, HFOL I, TGINS, XTGB .TWO.TGF.GGW. OPA, SCALE, I PR, IP, TGI, TFG, OPT, IPT, IPB, IPSA, IPPLICIT REALF4(L)

LGGICAL OP.CPA, OPG, OD.OPT, SUM

IF (NOT.OD) IPR=10

IF (NOT 'FC'I) JAIP'ANTP'AOP'SN'SP'AFR'OPG'SCALE' PROGRAM FOR SUPERHEATING SECTION SUP ER HEATER GEOME TRY OP G= .TRUE. WRITE(6105) FORMAT(00; 17 CALL GEOI (AN DR=DD/D1 GFA=GF/A CALL TCC CALL TCS 105 100

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SSCUPPODE STANDS SSCUPPOD SCUPPODE STANDS SSCUPPODE STAND HL= .023*(TCL/DI)*((DI*GFA/(VISL*GC))**.8)

X*((CPL*VISL*GC)/TCL)**.4

HTPF=(B*(1.-XA)**.8)*((QRB/(AI*GFA*HFG))

X+.001*((XA/(1.-XA))**.594))*HL

HC=I./((I./HTPF)*(AI*ALGG(DRI/(2.*PI*TCM*ANTP*L))+(AIP/AOP)*(1./H SECTION 1f(1.6E.2) CD TD 11
TG[1=TGOU+1.2*(QRB/(GC*CPG))
IF(X3.LT..08) TG[1=TGOU+1.0]*(QRB/(GG*CPG))
IF(X3.GT..5) TG[1=TGOU+1.5*(QRB/(GG*CPG)) INSIDE HEAT TRANSFER COEFFICIENT (BOILING BOILING GUESS GAS TEMP. IN (FIRST PASS ROUGH FIRST PASS HEAT TRANSFER CALCULATE AREA REQUIRED FOR XG)) EFF8=QR 8/ (CM INB*(TG11-TF1)) AN=HO*A1/CMINB EFFT=PASSB(AN) DIFPP=DIF DIFPP=DIF DIF=EFFT—EFFB DIFABS (DIF) IF (DIFALE.01) GO TO 30 IF (DIFPP-LT.0.) RA=.5*RA AI=AI-RA*AI CMINB=AI/AIP*GG*CPG GC TO 10 IF (DIFPP-LT.0.) RA=.5*RA AI=AI+RA*AI CMINB=AI/AIF*GG*CPG IP=1 IF(OP) GO TO 9 WRITE(61140) HG FORMAT(10°,'HG=',F6.2) CMINB=CPG*6G QP1=CMINB*(TG11-TG0U) A1=AIP RAT= 1 IF(X3.GT..8) RAT=.15 IF(X3.LT..1) RAT=.05 30000 400

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CALL SS(PF, TFO, HTF4, SSS,RSS)
HF01=HSV+QS H/GF
IF(OP) GO TC 36
WRITE(6, 188) FF0 1
FCRMAT('0', 'ENTHALPY OUT OF FIRST PASS=', F6.1) T FO1=T FO-((FT F4-HF01)/(HTF4-HSV))*(TFO-TFI)) (201) TEMP. OUT (FIRST PASS)=",F5.1) FI)/2 ,TFB,TCS1) FLUID PROPERTIES FOR SUPERHEATING SECTION REQ. FCR BOILING=", F6.2) ESTIMATE FLUID TEMP. OUT (FIRST PASS) PASS WITTE(6 185) AIB FCRMAT(10 '4' AREA REQ. FCR BOILL OP 1= 66 *C P6 * (TGI 1- TGOU) OS H= OP1 - ORB AIS = AIP - AIP GGS = AIP - AIP *GG TGOB = TGI 1 - QRB/ (GGB*CPG) GGS = GG-GGB IF(AIS GT.O.) GO TO 33 TGOS = TGII GO TO 34 TGOS = TGII - QRB TGOS = TGII - QRB TGOS = TGII - QRB TGII = TGII + 20. SUPERHEAT ING SECT ION OF FIRST CALL TEMP(PF, TF01, HTEST, HF01) STEAM CONDITIONS (FIRST PASS) FIND ACTUAL FLUID TEMP. OUT FB, GSS, SS S, ROS WRITEL WRITEL FORMATI TFB=(TF CALL TC CALL SS VOLSI=1

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/HF1)+(AI S*ALOG(DR)/(2.*PI*TCM*ANTP*L)) BB=(EXP(AA)-1.)/(C*SN)
EFS=1.-EXP(BB)
IF(OP) GO T C 47
WRITE(6,220) EFFS
FORMAT(100, PASS EFF. S/H SECTION=",F4.3) PRF1 = (VI S1 * C PS1 / T CS1) * G C HF1 = .023*(TCS1/DI)*(REF1**.8)*(PRF1**.4) IF(DP) GO TO 70 WRITE(6,200) HF1 FORMAT(10', 'HF1 = ',F6.2) DF=DO/DI HO1=1./((1./HF1)+(AIS*ALOG(DR)/(2.*PI X+(AIP/AOP)*(1./HG)) IF(OP) GO TC 49 WRITE(6,210) HO1 FCRMAT(10:, HO(FIRST PASS/SH)=',F6.2) FLUID SIDE HEAT TRANSFER COEFFICIENT UF1=GF*VOLS1/AFF REF1=(UF1*DI)/(VOLS1*VIS1*GC) IF(OP) GO TC 48 WRITE(6190) REF1 FORMAT(10, 'FIRST PASS RE=',F9.1) OVERALL HEAT TRANSFER COEFFICIENT CALCULATE NEW GAS TEMP. IN TGI 1 T= TF I + QSH/ (EF FS * CMIN) CMINT=CPS1*GF CWAXT=CPG*GGS CPIN=AMINI (CMINT, CMAXT) CMA X=AMA XI (CMINT, CMAXT) C=CMIN/CMAX ANTU=HOI*AI S/CMIN SN=ANTU**(- .22) AA=-ANTU**(- .22) CALL VISS (PF.T FB.VISI) VISI=VISI*2.778E-11 CALL CPS (PF.TFB, CPSI) PASS EFFECT IVENESS R EYNOL DS NUMBE 2000 2000 8 JUU

./HF2)+(AIP*ALOG(DR)/(2.*PI*TCM*ANTP*L)) 1*(1./HG)) TC 63 TEMP. INTO FIRST S/H PASS=", F6.1) .0.) RAT=.75*RAT 80.) RAT=.75*RAT RAT*DIFA FLUID SIDE HEAT TRANSFER COEFFICIENT OVERALL HEAT TRANSFER COEFFICIENT SUBSEQUENT PASSES TG02=TG11 TG1TS=TG11 TF8=(TF01+TF0)/2. IF (DIFA EQ IF (DIFT - LT IF (DIFT - CT IF (DIFT - GT QT = GG + CP G + IF (QP) GG + FORMAT (0 + RA = -5 GO TO 19 HO=1./((1. X+(AIP/AOP) IF(OP) GO

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/ (ARG**N-C) FO 1-CMAX *T GO 2) / (EFF *CM IN-CMA >) PA SSES P SUPERHEAT ER EFFECT IVENESS IN UMBER 1.1 GO TO 61260) EFFP ALL TEMP (P F, TF 4S, HT EST, HFO)
C TO 57
L=66*CP G*(16ITS-1602)
FO=HFO1+QL/GF
F4S=TF4 FEMP(PF, TF 4S, HTEST, HFO) .-EFFP*C)/(1.-EFFP) 60 TO 80 1 GO TO 500 WRITE(6,250) HD FCRMAT(101,1H0=1,F6.2) F=EFFS = GG *CP G*(TGITS- TG02) = C=HF01+QL/GF = 4S=TF4 LIM. EQ. 0) GO TO 88 PASS EFFECT IVENESS CMIN=CPS2*GF CMAX=CPG*GG C=CMIN/CMAX IF (0PT) GQ TO 00 50 N = 1,8 EFFS = EFF TGI TS = TGI TG[= (EFF WRITE(6.295 FORMAI(6.295 IF(IP-EG-1) IF(IP-EG-1) IF(IP-EG-2) IF(IP-EG-2) IF(IP-EG-2) 250 CCC 63 20005 295 50 56 80 58

ARG=(1.-EFFP*C)/(1.-EFFP)

TG=(4RG**LIM-1)/(ARG**LIM-C)

TG=(4RG**LIM-1)/(ARG**N-C)

TG=(4RG**LIM-1)/(ARG**N-C)

TG=(4RG**N-L)/(ARG**N-C)

TG=(4RG**N-L)/(ARG**N-C)

TG=(4RG**N-L)/(TG=(4RG**N-L)/(TG=(4RG**N-C)

TG=(4RG**N-L)/(TG=(4RG**N-C)

TG=(4RG**N-L)/(TG=(4RG**N-C)

TG=(4RG**N-L)/(TG=(4RG**N-C)

TG=(4RG**N-L)/(TG=(4RG**N-C)

TG=(4RG**N-C)/(TG=(4RG**N-C)

TG=(4R

SOURCE STORY SOURCE STORY SOURCE STORY SOURCE STORY SOURCE STORY SOURCE STORY SOURCE S

SUBROUT INE TEMP (PF, TF 0, HTEST, HF 0)

TINC=10

DIF 1=0

CALL SS (PF, TFO, HTEST, SSS,RSS)

DIF = AB S (D IF)

IF (D IF ALT 0.5) GO TO 46

IF (D IF 1.1.0.1) GO TO 45

IF (D IF 1.1.0.1) GO TO 45

IF (D IF 1.1.0.1) TINC=.5*TINC

TFC=TFO+TINC

DIF 1=D IF

GC TO 40

IF (D IF 1.0.1) TINC=.5*TINC

FFO=TFO-TINC

FFO=TFO-TINC

B IF 1=D IF

GC TO 40

RETURN 46 8 000

RETURN

```
GEOI (ANTR, L, AM IN, DO, AFF, DI, A IP, ANTP, ADP, SN, SP, AFR, CPA, OTF, FPF, OFB, LTAB, FINC, AFINT, LF, ANRP)
                                                                                                                                                                                 UBES/ROW=", F3.0,4X, 'TUBE LENGTH=", F3.0)
       GEOMETRY PREGRAM FOR RECTANGULAR SEGMENTED FINS
                                                                                                           ROW DESIRED .)
                                                                                                        FCRMAT('0', 'ENTER NO. TUBES PER ROW DESIR

FCRMAT(F3.0)

WRITE(6.82)

FORMAT('0', 'ENTER TUBE LENGTH DESIRED')

F AD(5, 82)

F AD(5, 82)

F AD(5, 82)

F AD(5, 84)

F ANTR L

F OPA | GO 10 90

WRITE(6, 84) ANTR L

FORMAT('0', 'NO. TUBES/ROW=', F3.0, 4x, 'TUBE
                                                                                                                                                                                                                                                                                                                                   PASS
                                                              90
                                                              GO TO
                                                                                                                                                                                                                                                                                                                                   PER
                                                                                                                                                                                                                                                                                                                                  NUMBER OF TUBES
                                                                                                                                                                                                                                                                                                                                                   ANTP = AN RP *ANTR
O TF = LF * 2 • + 00
                                                                                                                                                                                                SET DIMENSIONS
                                                                                                                                                                                                                                                                                                                                                                          FRUNTAL AREA
                                               LCGICAL DPA
PI=3.1416
IF (OPT OR S
WRITE(6100
F) = 3.1416
WRITE(6,801
                                                                                                                                                                                                                       DC=.166
DI=.15
TW=.01
                                                                                                                                                                                                                                                                                                                      CM=26
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AOP=ANTP*(AFIN+ABT)
IF(OPA.OR.SUM) GO TO 94
WRITE(6,87) AOP,AIP
FORMAT(10:,OUT. AREA/PASS=',F7.2,3X;'IN. AREA/PASS=',F7.3) AF IN=(TABS * (2 **LTAB*WTAB+2 **TF*LTAB+WTAB*TF) X+(PI/2 *) *(DFB**2-DO**2))*FPF*L AFINT=ANTP*AFIN AWIN=AFR-AB IF(OPA.OR.SUM) GO TO 93 WRITE(6,86) AMIN FCRMAT("0","MIN. FLOW AREA(GAS SICE)=",F7.3] *(WTAB+TF)/(WTAB*TF*TCM))**.5) W) GO TO 120 FINC CONST. FOR FIN EFF.=", F6.2] AFR=(SN*(ANTR-1.)+CTF)*L IF(OPA.OR.SUM) GO TO 92 WRITE(6,85) AFR FGRMAT('0', FRONTAL AREA=', F6.1) AB=ANTR *L *DO+FPF *L*ANTR*LF* 2. *TF GEOMETRY FOR FIN EFFICIENCY ABT =P1 * D0 * L -P1 * D0 *T F * FPF *L AFF=(P1/4.)*D1**2*ANTP MIN. FLOW AREA FOR GAS BLOCK ED FRONTAL AREA AREA FOR FLUID FLOW PASS OUTS IDE AR EA PASS INSIDE AREA A I P=P I *D I *L *AN TP BARE TUBE AREA FIN AREA

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GE000970 GE000980

RETURN

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POWER (PF, TSH, GF, DPG T, HPGT, PT, HPTC, STS, GTSFC, DASFC, SFC, THT, ET, PCON, PHTR)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  POWER DUT OF STEAM TURBINE = ", F7.1)
                                                                                                                                            , P ( 10) , H( 10) , S( 10) , V( 10) , X( 10)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                CALL SS(P(1), T(1), H(1), S(1), V(1))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               CALL HCW (P F, T FEED, HFEED)

$25=$(1)

$(2)=T$L(P(2))

CALL SS P(2), HC (2)

$2F=$5L(P(2))

$2F=$5L(P(2))

$2F=$5L(P(2))

$2F=$5L(P(2))

$2F=$5L(P(2))

$2F=$5L(P(2))

$2F=$5L(P(2))

$2F=$1L(2)

$2
                        PROGRAM FOR COGAS SYSTEM DUTPUT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     TURBI NE/CONCENS ER
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     GAS TURBINE
                                                                      XT. GTTH. DAT
IMPLICIT R
DIMENSION
SPACE
PERSION
P(1) = TSH
P(1) = PF
P(2) = 2
ET = 8
K(1) = 1
HPCNV = 254
LBTU = 0012
TFEED = 2002
HV = 18400
PHTR = 150
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                FORMAT ( 10
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                STATE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                9000
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BAL000520
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         **(PT/HPTO)
3350) STS
100, STEAM TURB. SHARE=', F5.1,2X,' PER CENT'
                                                                                                                                                                                  .000335*HP+4.81953E-8*HP**2-3.6366E-12
17E-16*HP**4-2.037E-21*HP**5
+.002125*DPGT
                                                                                                                    X6.41
STS-100.*(P)
WRITE(6.350)
FORMAT( 10.*
ETURN
                                                                                                                                          350
                                                                                                  250
                 150
                                   200
                                                                                                                   300
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BE ERT 1ES SHOULD ERT IES SHOULD Z GI VEN THE CALLING INSTRUCTIONS FOR EACH SUBPROGRAM ARE GITHE COMMENTS SECTION OF EACH SUBPROGRAM.

2. ALL CALLING TEMPERATURES ARE FAHRENHEIT.

3. WHERE SEPARATE SUBPROGRAMS FOR SATURATE WATER PROPEUSED.

4. WHERE SEPARATE SUBPROGRAMS FOR COMPRESSED WATER SARE NOT PROVIDED, THE SUBPROGRAMS FOR SATURATE. Z

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THIS SET OF SUBPREGRAMS
TRANSPORT PROPERTIES OF

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MATER

STEAM,

STEAM PROPERTIES HAVE BEEN TESTED FOR TEMPERATURES FOR WATER AND STEAM PROPERTIES HAVE BEEN TESTED FOR TEMPERATURES UP TO 1000F AND FOR A PRESSURE RANGE OF 1 PSIA TO 800 PSIA. THE VALUES Y 1000F STEAM TABLES WITHIN I.O PERCENT IN ALL CASES EXCEPT THE STEAM TRANSPORT PROPERTIES WHERE THE ERROR WAS LESS THAN 3.0 PERCENT ESS THAN BEEN TO STEAM TAMOSPHERIC PRESSURE FOR A TEMPERATURE RANGE OF TO 1500 F. AGREEMENT TO WITHIN 5.0 PERCENT OF THE VALUES IN THE KEENAN AND KAYE GAS TABLES WAS OBTAINED. ESTR ICT IONS

MAL CONDUCTIVITY (BTU/HR-FT-F) D IMENSION A (7) A (2) = .012999832 A (2) = .0000271167 A (4) = 2 .1052 E-11 A (5) = 3 .745E-14 A (5) = 3 .7745E-14 A (7) = 1 .27737E-20 RATUPE TCG COMPUTE

FUNCT ION TCG(T

œ AI

OF

90

FUNCTION PRANDG(T)

PRAND COMPUTES PRANDTL NUMBER OF AIR GIVEN TEMPERATURE

DIMENSION A(7)

PRANDG=0.

A(1)=.71905671

A(2)=-.0C013516.2

A(3)=-.00000009119.2

A(4)=9.5113E-10

A(5)=-1.56672E-12

A(6)=-1.11772E-15

A(7)=-3.0463E-19

CO 5 I= 1.7

K=I-1

PRANDG=PRANDG+A(I)*T**K

RETURN

FUNCT ION V ISG(T)

VISG COMP UTE S VI SCOSI TY ((LBM/SEC-FT) X1 0E7)

AIR GIV EN T EMPERATURE

DIMENS ION A(6)

TR=T+459.69

VISG=0.

A(1)=-32.28.39

A(2)=-4768-954

A(3)=-0000521402

A(4)=-000000396954

A(5)=-1.524776-10

A(6)=2.2720 IE-14

D(C)=1.524776-10

A(6)=2.2720 IE-14

VISG=V ISG+A(I)*TR***

w 000 000

=1-1 CG=TCG+A(I)*T**K ETURN ND

V.

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APPENDIX B

This appendix contains the program listings for the subroutines called by the WHRU design program and the COGAS model to obtain steam, water, and air properties. References 15 and 16 provide relationships for use in calculating the thermodynamic properties of steam and water. The relationships of Ref. 15 for the thermodynamic properties of steam were used in Subroutine SS of this appendix.

The remainder of the subroutines for steam, water and air properties were obtained by fitting polynomials to the values for those properties found in References 17 and 18.

In all cases, the polynomial coefficients were obtained using a "canned" program for least squares regression provided with the Hewlett-Packard System 9845 Computer installed in the Naval Postgraduate School Mechanical Engineering Department.

FUNCTION SPECG(T)

SFECG COMPUTES SPECIFIC HEAT (BTU/LBM-F) OF AIR

GIVEN TEMPERATURE

DIFFNSI GN A (6)

SPECGE SPECGE SPECIFIC HEAT (BTU/LBM-F) OF AIR

A (3) = -.00000 17494

A (3) = -.00000 17494

A (4) = 5.5502E-11

A (5) = -.00000 17494

A (5) = -.00000 17494

A (6) = -.00000 17494

A (7) = -.00000 17494

A (8) = -.00000 17494

A (8) = -.0000 17494

B (1) = -.0000 17494

B (2) = -.0000 17494

B (2) = -.0000 17494

B (3) = -.0000 17494

B (1) = -.0000 17494

B (2) = -.0000 17494

B (3) = -.0000 17494

B (4) = -.0000 17494

A (1) = -.0000 17494

B (1) = -.0000 174

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FUNCTION HSL(T)

HSL COMPUTES ENTHALPY (BTU/LBW) OF SATURATED

MATER GIVEN TEMPERATURE

DIWENSI CN A (6)

HSL COMPUTES ENTHALPY (BTU/LBW) OF SATURATED

DIWENSI CN A (6)

HS = 0.0411706E2

A (1) = -9.0411706E2

A (3) = -4.2744E-5

A (4) = 9.41244E-5

A (5) = -1.031537E-7

A (5) = -1.0088084

A (6) = -1.0088084

A (7) = -1.0088084

A (8) = -1.008

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A(5)=.15741642 A(6)=-.031329585 A(7)=.0038658282 A(8)=-.00C24901784 A(9)=.0000068401559 P1=P*10. D3 15 I=1,9 J=1-I T5L=TSL+A(I)*ALGG(PT)**J RETURN

2

HCW COMPUTES ENTHALPY (BTU/LEM) OF COMPRESSED WATER GIVEN PRESSURE AND TEMPERATURE DIMENSION A(5), B(5,5) DO 5 1 = 1, 5 A(1)=0. ENTCW=0. IF(P.LT.250.) GO TO 6 B(1,1)=-3.18831669083E1 B(1,2)=2.985C4393234E-3 B(1,2)=2.985C4393234E-3 B(1,3)=1.33348288125E-7 B(1,4)=9.70260583567E-10 SLBROUTINE HCW(P, 1, ENTCW)

```
B(5,1) = 4.0766436036E-10
B(5,2) = -1.87878835824E-13
B(5,3) = 1.1016365709E-15
B(5,4) = -2.0687586605E-18
B(5,5) = 1.2174855867E-21
C(70 9
F(P-LT-15.) G) TO 8
E(11) = -32.298005582
B(1,2) = 1.27673877487E-2
B(1,2) = 1.27673877487E-2
B(1,2) = 1.24633564596E-4
B(1,4) = 7.14487908312E-7
B(1,5) = -1.36503536452E-9
                                                                               ) =-1,41016204839E-6
3) = 1,11163180527E-8
3) = -3,06157715541E-11
1) = 3,50394655357E-14
5) =-1,43655502814E-17
          0048960506
05314335283E-5
746250309E-8
48793678207E-11
2881336815E-14
                                             .82721817375E-5
3.12450383809E-7
.3331884114E-10
1.04460627415E-12
                                                                                                                                                                                                                              911 02 04 C795 E-4
8 7857 57 295 E-6
091 61 72 5681 E-8
29548 52791 E-10
9 19975 54328 E-13
                                                                                                                                                                                            1376
3 C30 8E-4
5496 E-6
17424 E-8
5407E-11
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= 1.47
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= 2.93
= 2.865
= 1.30
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= 4.087
=-4.09
= 1.829
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3 7661172896 E-9 8 £82 8 64 C67E-11 8 40798 4 32 13E-13 1 882 31 5 96 E-15 2 80 7800 713 6E-18 1)=2.55004247051E-5 1)=-1.92085012998E-5 3)=4.32399525838E-6)=-3.70393732743E-7 3)=1.07027718423E-8 2 3721135296 - 8 5 4789011626 - 8 5 478901026 - 8 1 9899720846 - 9 8 C 2 170097196 - 11 05018E-3 1421E-3 1979E-4 1626E-5 19796E-6 1) =-33.9774136563 2) = 1.42585787825 3) =-329355699335 4) =2.87673452024E-2 5) =-8.42437941683E-4)=1.12118345966 |=-8.72001344198E-2 |=1.99827532858E-2 |=-1.733285E5779E-3 111965391764 19677751792E |=-2,65590705 |=1,960973114 |=-4,45063219 |=3,834672516 |=-1,11243809 * (7] = -1 .37 | = 4 .68 | = -4 .84 | = 2 .11 8 | = -3 .28 6. 923 6. 923 1-1.54 1.319 =1,5 11+8 = DO 10 1= K=J-1 A(I)=A(I 11 11 0 8 11.2 8 11.5 8 11.5 コンラナウ 4,5 ろろろろう ろろろろろ ころろろろ UMMUM UNANA 10 15 34444 00 K=1 O 88838 9 88888 மைமை 8888 88888

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9 ES THE THERMAL CONCUCTIVITY (BTU/HR-FT-F) WATER GIVEN PRESSURE AND TEMPERATURE K= I-1 ENTRCW=ENTRCW+A(I)*T**K RETURN ENC |=-1.286417756E-10 |=-6.66766057E-12 |=1.273196646E-14 TCCW(P,T,TC) |=-. C0170641 C367 |=4.163327E-7 |=-3.73672272E-9 |=3.09441147E-12 DI WENSION A(5), B(5,4) DO 5 I=1,5 A(1)=0. TC=0. IF(P.GT.10.) GO TO 10 A(1)=307.7700899 A(2)=-696656122 A(3)=-00141211951 DO 6 I=1,3 K=I-1 TC=TC+A(I)*T***K 2,1)=.7234487569 [2,2]=-.000112715317 2,3]=6.3925874E-7 2,4]=-5.0782358E-10 10 4,1)=1.008384811E-6 4,2)=1.80385129E-9 4,3)=1.46999925E-12 4,4)=-2.3690054E-1 (1, 1) = 307.0877221 (1, 2) = .007133552 (1, 3) = -.00001984573 (1, 4) = 1.5643034E-8 CCW CO MPUT SLBROUTINE 5,55 8868 8000 2000 9 09

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COMPRESSED WATER GIVEN PRESSURE AND TEMPERATURE

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DC 20 I=1,5 K=I-1 T C=TC+A(I)*T**K RETURN END

8(5,4)=-7.32465883E-1E

DG 15 1=1,5 DC 15 J=1,4 K*J-1 A(I)=A(I)+B(I,J)*P**K

SUEROUT INE CPCW (P,T,CP)

CCC 502

VOLCW COMPUTES SPECIFIC VOLUME (FT3/LBM) OF COMPRESSED WATER GIVEN PRESSURE AND TEMPERATURE SLBROUTINE VOLCW(P, T, VOL) GO TO 10 DIMENSION A (7)
VOL=0.
IF (P.GT.40.) GD TO 5
A (1)=.016055142
A (3)=.00000025908
A (3)=.00000043087
A (4)=-1.2311E-10
A (5)=2.737E-13
A (5)=2.737E-16
DO 4 1=1.6
K=1-1
VCL=VOL+A (1)*T**K
GO TO 40
IF (P.GT.250.) GO TO
A (1)=.01604542
A (3)=-00000024005
A (3)=-00000024005
A (4)=-1.0967E-16
A (5)=2.843E-13
A (6)=-4.747E-16

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0 IMENS ION A (8)
VI S=0.
A(1)=614.4041
A(2)=-10.547513
A(3)=-09648986
A(4)=-000626601
A(5)=-000001748041
A(5)=-3.460226E-9
A(7)=3.74087E-12
A(8)=-1.697431E-15
D(0) S I= 1,8
K= 1-1
VI S=VI S+A(I)*T**K
RETURN

COCO

COMPRESSED WATE

SUBROUTINE VISCM (T, VIS)

OF

VISCOS ITY ((LBF-SEC/FT2)X10E7) R GIVEN TEMPERATURE

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OF VISS COMPUTES VISCOSITY ((LBF-SEC/FT2)X10E7) STEAM GIVEN TEMPERATURE VISS(P, T, VIS)) =-4.2130659E-8 |) =-3.7618844E-10 | =-2.1559946E-13 | =-2.35229651E-15) = 1 • 77924019E-11 2) = 5 • 4324874E-14 1) = 2 • 0441744E-16 1) = 6 • 0458155E-19 E(1,1)=8.7550405 B(1,2)=.096375699 B(1,3)=-.00C054876232 B(1,4)=4.14264051E-7)= .014332668)=-.00042096669)= 2.2221582E-7)=-1.92572826E-9)= .000C43096178 |= 6.4811772E-7 |=-1.5156235E-10 |= 3.25662448E-12 00 DC 20 1=1,5 DO 20 J=1,4 K=J-1 A(I)=A(I)+B(I,J)*F**K A(7)=1,3371E-17 D0 10 1=1,7 K=I-1 TC=TC+4(I)*T***K GC TO 30 DC 25 I=1,5 K=1-1 TC=TC+A(I)*T**K RETURN END SLBROUTINE 4444 4901 B(5,2) B(5,3) B(5,3) 10m3 mmmm 2000 8688 8868 8888

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CPS COMPUTES SPECIFIC HEAT (BTU/LBM-F) OF STEAM GIVEN PRESSURE AND TEMPERATURE

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DIMENSION A(7)
VIS=0.

VIS=0.

A(1)=1.9266.29

A(2)=.00002555

A(3)=.000026555

A(4)=-.0000000049502

A(5)=6.3081E-11

A(5)=6.3081E-11

A(5)=-4.0795E-14

A(7)=1.05411E-17

DO 5 I=1.05411E-17

A(1)=5.75541

A(1)=5.72541

A(2)=-.0332628

A(3)=-.0332628

A(4)=-2.088647E-7

A(5)=1.636259E-10

A(5)=1.636259E-10

A(5)=1.636259E-10

A(5)=1.636259E-10

A(5)=1.636259E-10

A(5)=1.636259E-10

SU BROUT INE CPS (P, T, CP)

D IMENS ION A(7), B(7,5)
D(5 1=1,7
A(1)=0.
CP=0.
IF (P.GE.10.) GO TO 16

(2,1)=.000181043581 (2,2)=-.00C170325517

1= .422296265 1= .030268522 1= .004854928 1= .000005974

A A A COLOR OF SOLUTION OF SOL

```
| =1.9550162513E-12
| =-5.8231567639E-12
| = 4.10144879154E-12
| =-9.18383604222E-13
                                                                                                                                       1)= 7, 02 557694 356E - 19

1)=-1,79132 736742E-18

1)=1,10536956 813E-18

1)=-2,31734765803E-19

1)=1,528936 17959E-20
                                                                                                          1352 5E-15
1341E-15
18501 E-15
18987E-16
                                                                                                                                                                                                                 26
                                                520996 E-10
520512 E-9
156325 37E-9
1864156 E-10
33612442E-11
-.000013866942
1.37436147E-5
-1.38328347E-6
                   |=-1.6226512E-7
|=-1.3626817E-7
|=4.8500908E-7
|=-1.4264727E-7
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                                                                                                                                                                                                                               200
                                                                                                          | =-2.01614243
|=5.387276783
|=-3.47742978
|=7.472605289
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A A CONTRIBUTION OF THE CO

)= 1.40514276E-6)=5.510352E-8)=5.0367755E-10)=-2.13368295E-12 1)=-2,3595704E-9 1)=-3,3266941E-11 1)=-1,54501998E-12 1)=4,3756116E-15)=-.00C30842028 !)=-3.30841469E-5 !)=-2.56142116E-7 !)=4.0736494E-10 =-6.16157702E-16 =7.0953059E-18]=-4.0450706E-19 =1.34272907E-21 |=1,9590| 81 8 E-12 |=-2,753866E-15 |=1,26930|77 E-15 |=-3,966466 8E-18 1 £54 004 0 468 168 0 0157 02 1974 1 £92 83 £ - 7 7 309 7 59 £- 11 DO 20 1=1,6 DO 20 J=1,4 K=J-1 A(I)=A(I)+B(I,J)*P**K 1)= .018 18816 2)=-.00025378215 3)=8.1211789E-7 4)=-1.15184066E-9 .0947953 4(1)*T** = -3.1 = -0504 = -0000 = 2.318 = -9.73 1=1,6 1-=146 (6,1) (6,2) (6,4) CP=CP+A BELL 1 20020 222 กักกัก = 0000 8888 8888 8888 8888 20 25 C 26

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T=TF/1,8+255.38 P=PA/14,6955 B1 =(2641,62/T)*10.**(80870./T**2) B2=82.546 B3=162460./T B4=.21828*T B5=126970./T B0=1,89-B1 FC=1,89-B1 * (372420./T**242) COMPUTES ENTHALPY (BTU/LBM), ENTROPY (BTL/LBM-F) D DENSITY (FT3/LBM) OF STEAM GIVEN PRESSURE D TEMPERATURE SUBROUT IN E SS (PA, TF, HSS, SSS, RSS) DD 30 1=1,5 DC 30 J=1,5 K=J-1 A(I)=A(I)+B(I,J)*P**K DC 35 I=1,5 K=I-1 B(4,1)=2,7766181E-8 B(4,2)=-3,9361743E-10 B(4,3)=1,30491831E-12 B(4,4)=-1,904084E-15 B(4,5)=8,1631412E-19 B(3,1) =-.000033784538 B(3,2)=4.7562105E-7 E(3,3)=-1.55257254E-9 B(3,4)=2.2709037E-12 B(3,5)=-9.6702875E-16 B(5,2)=1,21404264E-13 B(5,3)=-4,0161977E-16 B(5,4)=5,9420773E-19 B(5,4)=-2,5627204E-22 CP=CP+A(1)*T**K RETURN END SS CAND AND

. F.

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CCCCC

B 7=2.*F C*(B 4-B5)-B0*B 5

E=E0*(1.*/f)*(B0*P)/T **2)*(B2-B3+((B0*P)/T **2)*(B4-B5)*BC*P))

X *(B0*F)/T)*(B0-F0)*P+((B0/2.)*(P/T)**2)*(B6+((B0/2.)*(P/T))**2)*B0AUX08190

X *(B0*(B 4-B 5)-2.*B7))

V(L=.0160185*('4.55504*T1/P+B)

N SS=1. /VOL

HSS=F+.043557*(F0*P+((B0/2.)*(P/T))**2)*(-B6+BC*(B2-B3+2.*B7)*(BC/2.AUX08220)

X)*(P/T)**2))

X) *(P/T)**2) / D

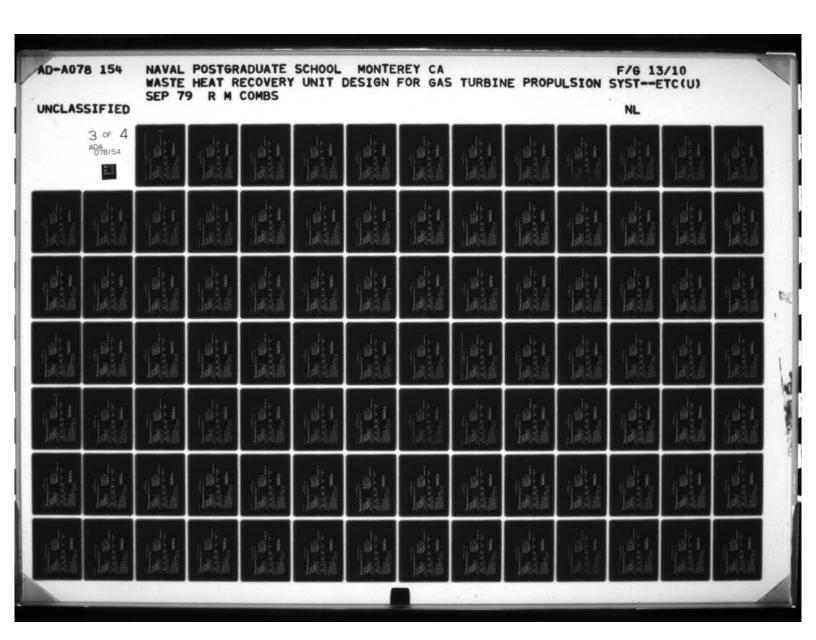
X) *(P/T)**2) / D

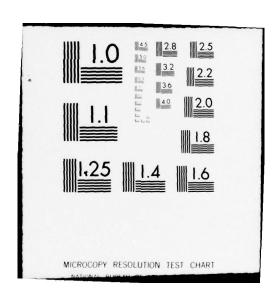
X) *(B0/2.)*(P/T)**2) / D

X) *(B0/2.)*(B0/2.)*(P/T)**2) / D

X) *(B0/2.)*(B0/2.)*(P/T)**2) / D

X) *(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B0/2.)*(B





 $_{\rm roc}$.. 06.54.31 26.41.193

T. T. W. T. L.

MASTE HEAT RECOVERY UNIT DESIGN RUN

RATAK HESEPOWEA: 16421.0. AFPHUNIAMIE CORRESPONDING SHIP SPEED: 20.0 KTS
TEACHTST GAS TEACHTORE 1089.0 F BATAR (113.2 LBM/SEC)
EXHALST GAS FELSA FELS 40.7589.0 LBM/HR (113.2 LBM/SEC) CAS TUREINE

TRABLER SUFFACE ET 2.5 INOUTSIDE TOOK JAMETER: 1.9 INI ISTOF THAT JAMETER: 1.9 INI ISTOF THAT JAMETER: 1.9 INFINITY SECURE SECONDARY
FINITY SECONDARY
FINITY SECONDARY
FINITY SECONDARY 6VEF 31 . 01-14-151 315: 17-16 . 15-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 . 17-16 HEAT EXCHENSES SEGMETHY

(EDILING LENGTH: 3.1 FT.) NUTSI UE AREA/PASS: 3264.9 50.FT. INSIDE AREA /PASS: 187.5 SC. FT. NUMEER OF PASSES: 21 (TOTAL)
HARTING SECTION: 9
BAJLING SECTION: 10
SUPERINEATING SECTION: 2 FROMTAL AREA: 143.5 SG. FT. NUMBER OF TUBES PER ROWS NUMBER OF RCMS PER PASS: TLEE LENGTH 12. FT.

GAS TEMP. IN GAS TEMP. OUT FLUID TEMF. IN FLUID TEMF. OUT REYNOLDS NUMPER (AVG.) 27700.6 213652.1 544.7 MEAT EXCHANGEN PENFERPANCE PCILITIONS SEPERIFATING SECT 174

STEAM PRISSULET BUD O PSIA (SATURATION TEMPERATURE. 518.3 F) STEAM FLOW KATE: 15121.8 LBMAIR.

G45-510E PD ESSIDE TO 1P: 1.8 IN H20 PINCH PCINT: 32.0 F

STEAM TURBLINE HCHSEPCWER: 5205.2 TGTAL SYSTEM HURS EPUMER: 21162.5 CT H'FSEPIMERIPEVISEDIS 15957.2 SYSTEM PEHF CHMANICE

SPECIFIC FULL CANSUMPTION (LBM-FUEL/HP-HR): 6.39C STEAP TURBLUE SHARE OF THE LOAD: 24.6 PERCENT FUEL CONSCHIPTION (LOP-FUEL/HR-): 6984.7

GT AT SYSTEM HP: 8252.2 GT AT SYSTEP hP: 0.355

COLAS: 0.419

FALMEN LEFT IC LENCY:

CONDENSER PRESSURE: 4.08 IN HG STEM TURBINE EFFICIENTY: 0.85. FW HEATER FRESSURE: 15.0 PSIA LIV OF FUEL: 13400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS:

LONGITLEINAL THAL PACING: 3.93 IN.

TARVOVERSE TUME SPICING: 4.50 IN.

WASTE HEAT RECOVERY UNIT DESIGN RUN

FRANK FCFSEFTMER: 8526.0, APPRIXIMATE CURRESPONDING SHIP SPEED: 16.6 KIS EXMALSI 345 TEMPERATURE: 742.0 F EXFAUST GAS FLIM AATE: 328641.3 LBMAHR (91.3 LBM/SEC) GAS TURRINE

CUTSIDE AREA/PASS: 3264.9 SQ.FT. INSIDE AREA/PASS: 187.5 SO. FT. NLWBER OF PASSES: 15 (TCTAL)
ILEATING SECTION: 5
BOIL ING SECTION: 2
SUPERHEATING SECTION: 2 FROWTAL AKEA: 143.5 SC. FT. NUMBER OF TUBES PER ROWS NUMBER OF RCMS PER PASS : TUBE LENGTH 12. FT. PEAT TAYOREA SUPFACE COLORS OF THE COLORS OF LONGITUDITIEL TURE SPECIFIES 3.90 IN. TRANSVERSE TUBE SPACINGS 4.50 IN. CV EP ALL E14E 1517715: E15671: 12-0 FT. MIJATT: 12-0 FT. HEAT EXCHANGER GEUNETRY

FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVS.) 108754. 5 STEAM PRESCURE: BOU.D PSIA (SATURATION TEMPERATURE- 518.3 F) 200.0 508.9 518.3 GAS TEMP. OUT GAS-SICE PAESCURE CROP: 3.7 IN HED GAS TEMP. IN STEAM FLOW RATE: 20105.6 LBHAIR. PINCH PILITE 36.8 F BELLING BELLING SEPTEMENTING SEC TI ON

CONDENSER FRESSURE: 4.08 IN HG STEAT TIRRINE EFFICIENCY: 0.855 FW HELS PRESSURE: 15.0 PSIA LHV OF FLEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 5305.8 GT AF SYSTEM HP: 0.287 SPECIFIC FUEL CONSTMETION (184-FUEL /HP-HR): 0.482 STEAM TURBINE SHARE OF THE LOAD: 24.1 PERCENT FUEL CCASCMFTICN ALE'-FULL/FR-1: COUAS: 0.344 STEAM "INCINE HURSEPCHER: 2656.5 TOTAL SYSTEM HOUSEONERS 11012.6 ST HOF SEPTWERINEVISEDI: 8350.1 THEN BAL EFFICIETES

SYSTEP FEFFCHPANCE

HEAT EXCEPTIBLE PERFORMATICE

(HEATING LENGTH= 3.4 FT.)

2. 14.

MASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TUNBIPE

Carillis 11. 52. 26

HANKE HJRSCPIJAËR: 1684.0; AFPRIXIMATE CORRESPONDING SHIP SPEEC: 9.0 KTS [47415T GAS FEYDERATURE: 689.0 F EJIMIST GAS FLOW HATE: 159731.0 LBV/HR (44.4 LBM/SEC)

HEAT EXCHANGER GEOMETRY

CV ER ALL CITETS LT.S: T. LENGTH: 12.0 FT. HEIGHT: 12.0 FT.

CONSTRUCTION CLAMEER: 20 IN10310 LUS CONFERS: 1.9 IN1031111 AS A GENTY E
11 SET LUS CONFERS
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LONG ITUDITAL TURE SPACINGS 3.90 IN. TRANSVERSE TIIDE SPACITIES 4.50 IN.

(BOILING LENGTH: 4.5 FT.) OLTSIDE AREA/PASS: 3264.9 SC.FT. INSIDE AREA/PASS: 187.5 SQ. FT. FRENTAL AREA: 143.5 SQ. FT. NUMBER OF TUBES PER ROW: NUMBER OF RCHS FER PASS : TUBE LENGTH 12. FT.

NUMBER OF PASSES: 11 (TOTAL)
ILEATING SECTION: 3
BOLLLING SECTION: 5
SUPERFEATING SECTION: 3

HEAT EXCEANGER DEPRINAVICE

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) BELL ING SCPLENETING SECTION

STEAM PRESSURE: 830.0 PS IA ISATURATION TEMPERATURE. 518.3 F. STEAM FLUM AFTE: 7236.4 LBMAHR.

GAS-SICE PRESSURE CRCP: 0.3 IN H20 PINCE PINIS 39.6 F

SYSTEM DERI JAMBILLE

STEAP FINABLYE STARE OF THE LOADS 36.5 PERCENT 955.2 TUTAL SYSTEM HORSEPONER: 2615,7 STE 1" TURBINE HURSEPOWERS GT HCFS EFONEH (REV IS EC):

COMOGNSER PRESSURE: 4.08 IN. HG STEAF TURBINE EFFICIENCY: 0.85 WHEATER PRESSURE: 15.0 PSIA LHV CF FUEL: 18400 RTUZER

A SSUMED SYSTEM CHARACTERISTICS:

SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HR):

0.890

GT AT SYSTEP HP: 0.155 FLEL CONSUMPTION (LBF-FUEL/MR.1: 1766.0 GT AT SYSTEM HP: THEAPL EFFICIENCY: COGAS: 0.205

WASTE HEAT RECOVERY UNIT CESIEN RUN

GAS TURBLINE

ENABLY CREEPINER: 16421.3, APPRIXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS

ENABLY GAS TEMPERATURE: 849.0 F

EARAUST GAS ILIM RATE: 40.1589.0 LBMAIR 1113.2 LBM/SEC)

NUMBER OF TUBES PER ROLI NUMBER OF ROWS PEP PASSE LONGITUDINAL TOOK SPACINGS 2.92 IN. TRAISVERSE TURE SPICINGS 3.39 IN. OVERALL OF MENSIONS: FI-FIGURE 12-0 FIGURE 12-0 MEDIUS 13-0 MEDIU HEAT EXCEEDER CE IMETPY

TUBE LENGTH 12. FT.

OUTSIDE AREA/PASS: 3290.5 SO.FT.

INSIDE AREA/PASS: 189.0 SO. FT.

FRINTAL AREA: 144.8 SO. FT.

NUMBER OF PASSES: 16 (TOTAL)

BOIL HG SECTION:

SUPERHEATING SECTION: 2 (FOIL ING LENGTH= 5.3 FT.)

#EATITY | 551.4 | 551.4 | 551.2 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.3 | 518.

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMF. OUT

REYNGLDS NUMPER (AVG.) 27356.4 213355.1

> STEAP FLCV HATE: 38597.2 LBM/HR. GAS-SIJE PF ESSONE DROP: 6.0 IN H20

SYSIEM PENFORMANCE

PINCH PCINT: 32.3 F

ASSUMED SYSTEM CHARACTERISTICS: SPECIFIC FUEL CENSUFFIION (LM4-FUEL/FP-HR): 67 AT SYSTEM HP: 0.391 STEAM FURBIUE SHERE OF THE LOADS 24.2 PERCENT STEAP TENNINE HUFSEFEWER: 5049.7 TOTAL SYSTEM HAPSEPSIMER: 21116-1 CT HEPSEPHEP (3EVISED): 16016.4

THERET EFFICIENCY: COURS: 0.418 GT AT SYSTEM MP: 0.354

FUEL CUNSCHPTAUS LLBF-FUELVIR-1: 6992. 7

GT AT SYSTEM HP1 8257.0

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HEAT EACHANIER PLAFCRMAICE

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MASTE HEAT RECOVERY UNIT DESIGN RLN

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MAKAF HINGEPIMES. 6526.0, APPROXIMATE CORRESPONDING SHIP SPEED: 16.0 KTS EXHIRITY SPEED: 16.0 KTS EXHILIST JAS TEMPERED SPEED: 16.0 KTS EXHILST JAS TEMPERED SPEED: 16.0 KTS FAHALST JAS TEMPERED: 12.0, APPROXIMATE SPINSECI

htal Exchinces CEONETRY

CVERALL ULVENSLINS: FT. WIDTH: 12.1 FT. helon: 2.9 FT.

AT TAIN FEAT SIFFACE OLISIUE TUNE DI METER 1.4 IN. TUEZI IN ARKA GENEVITE FILE IN THE SEMBNIED FILE STAFF OF THE SEMBNIED FILE THE SEMBNIED FILE THE SEMBNIED

NUPBER OF PASSES: 12 TOTAL)
HEATIN, SECTION:
BUILING SECTION:
SUPERFEATING SECTION: 2 FRONTAL AREA: 144.8 SC. FT.

OUTSI UE AREA/PASS: 3250.5 SQ.FT. INSIDE AKEA PASS: 189.0 SC. FT.

NIMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS :

TURE LENGTH 12. FT.

(HEATING LENGTH 2.1 FT.)

HEAT EXCHANGEN PERFCAPANCE

SECTIM

ICAGITUDINAL TUBE SPACITIE: 2.92 IN.

TRANSVERSE TUBE SFACING: 3.33 IN.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMF. IN FLUID TEMP. DUT PEYNOLDS NUMEER LAVG. 1 109056.4 HEATING ROLLING SUPERHEATING

STEAM PRESSURE: BUD.U PSIA (SATURATION TEMPERATURE 518.3 F) STEAM FLOW RITE: 19998-8 184/HR.

GAS-SIDE PRESSURE DEGP: 3.1 IN H20 FINCE PULL SOLL F

SYSTEP REFF CAPANCE

ASSUMED SYSTEM CHARACTERISTICS: SPECIFIC FUEL CONSUMPTION ALBM-FLEL (MP-HR): STEAM (URBINE SAMRE OF THE LOADS 23.9 PERCENT STEAP THREINE HORSEPFWER: 2629.1 TITAL SYSTEM HIRSFPINER: 10995.6 GT HTF SEP INERINEVISEUDI: 8366.4

CONDENSER PRESSURE: 4.08 IN. HG STEAT TING INE EFFICIENCY: 0.85 FW HEATER PRESSURE: 15.0 PSIA LHV OF FLEL: 18400 0TU/LBM

GT AT SYSTEM HP: FUEL CCNSCHPTION JLEP-FUEL/HR. 1: 4432. \$ THER ST CALVE 16.261

COUAS: 3.343

GT AT SYSTEM HP: 0.287

2 1 1

WASTE HEAT RECOVERY UNIT DESIGN RLN

PARKE HORSEPHER: 1684.0, APPROXIMATE CORRESPONDING SHIP SPEED: 9.0 KTS Stanity of as temperature: 16973.0 Februar (44.4 LEP/SEC) Exials GVS FLOW Rate: 15973.0 LBP/HR (44.4 LEP/SEC) GAS TURBINE

OUTSIDE AREA/PASS: 3290.5 SQ.FT. INSIDE AREA/PASS: 189.0 SQ. FT. NLPBER OF PASSES: 9 (FOTAL)
HEATING SECTION: 2
SUPERHEATING SECTION: 5
SUPERHEATING SECTION: 2 FRONTAL AREA: 144.8 SQ. FT. NUMBER OF TUBES PER ROW! NUMBER OF ROMS PER PASS : TLBE LENGTH 12. FT. MEAT TEAMSEEN SURFACE

OLISEDE INSTITUTE IS IN.

INSTITUTE AREA CELEBRITATION IN THE INSTITUTE IN THE INSTIT TRANSVERSE TUBE SONT ING: 3.36 IN. CVERALL DIMENSIONS: FT. LENSIN: 12.6 FT. HIGH. 12.1 FT. HELAIL: 2.2 FT. HEAT FACETANSER GEOMETRY

(HEATING LENGTH= 5.4 FT.) LONGITUDIAL TUSE SPACING: 2.92 IA.

4874.5 38746.6

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FILLID TEMP. DUT REYNOLDS NUMBER (AVG.) STEAM PRESSURE: 800.0 PS IA (SATURATION TEMPERATURE. 518.3 F) 0.6 IN H20 STEAM FLIM KATE: 7253.1 LBMAIR. GAS-SIDE PRESSURE CPCP: PINCE PINTS 53.0 F BCILING BCILING SUPLANEATING Sect 10n

SYSTEM PERF. 12 MAYICE

CONDENSER PRESSURE: 4.08 IN. HG SIGAP TURINE EFFICIENCY: 0.65 FW HEATER PRESSURE: 15.0 PSIA LHV CF FUEL: 18400 BTU/LR A SSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 2331.6 GT AT SYSTEM PP: 0.156 0.889 SPECIFIC FLEE CHISUMPTION (LBP-FIEL/HP-HR): SYSTEM HP: STEAM TUREINE SHARE OF THE LOAD: 36.7 PERCENT FUEL CONSCHIPTION (LBP-FUEL/HR.): 166.1 CUGAS: 0.205 962.1 1JTAL SYSTEM HOR EPONER: 2623.1 GT HENSEFONERIREVISEEJI 1660.9 STEAM TOWNINE MINSEPONERS LIENPEL LIPTICIENCY:

HEAT EACHANGER PEGFORMANCE

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MASTE HEAT RECOVERY UNIT CESICN RUN

	k 1.5	
	SPEEDI	
	315	EC.
	SPONDING	.2 184/5
	CORRE	===
	PPRIXIMATE	.O LAMAIR
	16421.0. A	EXTAINT CAS TENT HAT UNE: 917.0 [SMAIR (113.2 LBM/SEC)
	CRS EP IMER:	G15 71 74 R
GAS TURBINE	ER AKL P	EXFA IST
CAS		

	EXEALST GAS TEMPRATURE: 849.0 F MAIN III3.2 LBM/SECI	[9MAIR	1113.2	LBM/SEC)	
HEA	HEAT ENCHANGE GEOMETRY				
	OVERALL DITETSITUS:				NUMBER OF ROMS PER
	MJ) 14: 12:0 FT.				NIMBER OF TUBES PE
	PE ICFT: 2.1 FT.				TLAE LENGTH 12.
	HEAT 1441SFL4 SUMPTICE TO	Z			OLISIDE AREA/PASS
	TOBELT AFFIGHENTS	<u>:</u>			INSIDE AREA/PASS:
	FIN SPACING 11.88 FIN	15/1 k.			FPCNTAL ARED: 143
	FIN THICKNESS: 0.024				NUMBER OF PASSES:
	TRANSVEASE THUE SPACING: 2.25 IN.	<u>. x</u>			BOILING SECTION
	LCNG ITUDITIAL TURE SPECIFIC: 1.95 IN.	ž			

	::
	•••
	LENGTH:
	1801 LING
(TOTAL)	10N: 1
FINOT	SECT
NUMBER OF PASSES: 13 (TO	FEAT FIG
HEAT	SUP E
NUMB	

: 3264.9 SC.FT. 187.5 SC. FT.

ER ROWS R PASS 8

FT.

3.8 SO. FT.

IAS TEMP. IN GAS TEMP. QUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMPER (AVG.) STEAM PRESSURE: 800.0 PSIA (SATURATION TEMPERATURE 518.3 F) 5000 540.5 GAS-SILE PRESSUME DRCP: 5.3 IN H20 STEAM FLOW RATE: 39189-5 LIMARA. PINCE PUBLIT: 34.0 F HEAT EXCHANGES PERFORMETCE SUPERFERENCE SECTION

203528.9

CONDENSER PRESSURE: 4,08 IN HG STEAM TURBINE EFFICIENCY: 0,85 FW HEATER PRESSURE: 15,0 PSIA LIN OF FUEL: 18450 BTU/LB4 ASSUMED SYSTEM CHARACTERISTICS: FUEL C 715UMPT1014 (LBP-FUEL/NR.): 6995.9 GT AT SYSTEM HP: 8238.4 0.387 THERM'L EFFICIENCY: COGAS: 0.420 GT AT SYSTEM HP: 0.357 SPECTIFIC FUEL CONSUMPTION IL BM-FUEL /HP-HR : SYSTEM HP: STEAP TERSINE SHARE OF THE LOAD: 24.6 PERCENT STEAM TUREINE HIMSEPTMER: 5226.6 TOTAL SYSTEM HUNSFPUNER: 21267.1 GT HERSEFENEARREVISEDI: 16040.5 SYSTEM FERE IRMATICE

MASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TUREINE BRINE HOWSEPJUER: 9526.0, AFPROXIMATE CORRESPINCING SHIP SPEED! 16.0 KTS EAFILS! CA'S TEMPERATURE 328641.0 TRM/HR (91.3 LUM/SEC)

MEAT EXCHANGE GEOMET PY
OVERALL DIMENSIONS: FT.
LENGTH: 12.0 FT.
HISH: 12.0 FT.

NUMBER OF PASSES: 9 (TOTAL)
HEATING SECTION: 4 (FEATING LENGTH: 1.3 FT.)
SUPERFETING SECTION: 2 (B)ILING LENGTH: 5.6 FT.)

FFC"ITAL AREA: 143.8 SQ. FT.

DUTSIDE AREA/PASS: 3264.9 SQ.FT.
INSIDE AREA/PASS: 187.5 SQ. FT.

NUMBER OF REWS PER PASS: NUMBER OF TUBES PER ROWS

TLBE LENGTH 12. FT.

HEAF EXCHAILER PEPFIRMANCE

LENGITUDINAL TUNE SPACING: 1.95 IN.

TRANSVERSE TILLE SPACINGS 2.25 IN.

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) 14117.1 111551.6 244 449 450 8 ECILING SLPERIEVENS SEC 11 JA

STEAM FRESCHE: BUD.O PS IA ISATURATION TEMPERATURE. 518,3 F1

STEAM FLIM RATE: 15852.0 LOMAIR.

CAS-SIJE PRESSURE CRCP: 2.5 IN H20 PINCH PINT: 34.4 F

SYSTEM PERF JAMANCE

CONDENSER PRESSURE: 4.08 IN. HG STEAP TURBINE EFFICIENCY: 0.85 FW HEATER PRESSURE: 15.0 PSIA LIV CF FIJEL: 18400 BTU/LRM A SSUMED SYSTEM CHARACTERISTICS: STEAP THRETTE SHARE OF THE LIAC: 23.8 PERCENT STEAM TURBL'IE MUR SEPUNER: 2623.0 131AL SYSTEM HUNSEPCHER: 10999.1 GT HENSEROWERINEVISEEN: 8376.2

SPECIFIC FEEL CONSUMPTION (18M-FIELZHP-HR): 05482

FLEL (JASUMPTION (LBP-FUEL/NR-1: 4-13.9

THEN PAL LEFT CLENCY: COJAS: 0.343 GT AT SYSTEP HP: 0.287

GT AT SYSTEM HP:

The state of the

WASTE HEAT RECOVERY UNIT CES IGN RUN

5.0 × 1S

BEET BALLST CL. CL. T. F. Y.

MEST STATE THE LANGE TERT TO THE STATE TO THE STATE TO THE STATE T

(BELLING LENGTH: 4.3 FT.) OLTSIDE AREA/PASS: 3264.9 SO.FT. INSIDE AREA/PASS: 187.5 SQ. FT. FRINTAL AREA: 143.8 SO. FT. NUMBER OF TUBES PER ROLL NUMBER OF ROWS PER PASS: TLBE LENGTH 12. FT.

NLMBER OF PASSES: 7 (TOTAL)
HEATING SECTION: 3
SUPERHEA II:1G SECTION: 2

FINE LA L'OUT AL L'ENVIET

1000

LIVINOTER FOR SPAINS 1.95 IN-

TATTOR .. 114. 50 CHUS 2.25 IN.

LAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS MINPER (AVG.) 482.5 543.6 612.1

STEAM FOR THE BOWN PS IN (SATURATION TEMPERATURE SIB. 3 F) Sff. 4 ft.1. 41.ft. 1253.1 LBM/HR.

UATTO PARTIE OF DE IN HZD

9.956.5 C mit tr . c. e . e' toll le 1061.4 Stell Let or 112 S. PoneR:

SECTION OF THE CONSTRUCTION (LEW-FUEL/HP-HR): GT AT SYSTEM HP: 0.890 STEIN CHALLE HARE OF THE LOADS 36.5 PERCENT

GT AT SYSTEP HP: 0.155 Int. Pic. 11 1. 15 147: COUAS: 0.205

Dille Syfler and Eberth: 2015.9

CONDENSE PRESSURE: 4.08 14. HG STEAL TURBILE EFFICIENCY: 0.85 FW HAFFE PRESSURE: 15.0 PSIA LIV CF FUEL: 18400 BLULLM

A SSUMED SYSTEM CHARACTERISTICS :

08/22/19 12.18.18

RUN #10

The state of the

WASTE HEAT RECOVERY UNIT CESIGN RUN

GAS TUPRINE

FRAKE PERSENGEN 16421.00 APPRIXIMATE CORRESPONDING SHIP SPEED: 2C.0 K1S EXHALST DAS TEMPERATURE: 849.0 F
EXPANST GIS FLIM GATE: 407589.0 LBM/HR (113.2 LBP/SEC)

HEAT EXCEANCES CENSETFY

OVERALL DIMENSIONS: F. LEASTH: 12:0 FT. HELDER: 12:0 FT. HELDER: 6:2 FT.

HAF T PARTE A SUPERIOR THE ZO IN. CONTROL OF FIRE LAS IN. ITS LOCKED THE FORE LAS IN. TO SUPERIOR THE SUPERIOR THE FIRE LAS IN. TO THE FIRE LAST IN. CONTROL OF THE LAST IN.

TRANSVERSI TURE SOLCINGS 4.5C IN.

NLYBER OF TLBES PER ROW: 32.

TLBE LENGTH 12. FT.

OUTSIDE AREA/PASS: 3264.9 SQ.FT.

INSIDE AREA/PASS: 187.5 SQ. FT.

FHONTAL AREA: 143.5 SC. FT.

NUMBER OF ROWS PER PASS:

NUPPER CF PAS SES: 19 (TOTAL)
HEATING SECTION:
8 HEATING LENGTH: 0.3 FT.)
SUPERIEATING SECTION: 2 (BCILLING LENGTH: 2.5 FT.)

HEAT EXCHANGER PEPFORMANCE

SECTION

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLLID TEMP. DUT REYNOLDS NIMPER (AVS.) 26712.4

224266.2

FF. [Mg 223.5 404.5 200.0 646.3 486.3 486.3 516.4 0.0 0.0 PSIA (SATURATION TEMPERATURE 486.3 F)

STEAM FLUE KATE: 39494.7 18#/HR.

GAS-SIDE PRESSURE 9479: 6.7 IN H20 PINCH PCINT: 37.2 F

SYSTEM PEH CHMANCE

UNDENSER PRESSURE: 4.09 14. HG TEAM TURBINE EFFICIENCY: 0.85 WHEATEP PRESSURE: 15.0 PSTA THY OF FIRE: 18400 HTU/LRM ASSUMED SYSTEM CHARACTERISTICS: STEAP TURNINE HCKSEPCWER: 5072.3 TOTAL SYSTEM HORS EPONER: 21065.6 CT HEFSEP INCREMISERIS 15993.3

STEAM FLAGILE SHARE OF THE LOADS 24.1 PERCENT SPECIFIC FLEE CLASSMETTEN ILUM-FLEEVEP-HRIS GT OLLY: 0.437 COUAS: 0.332 GT AT SYSTEM HP: 0.392

FUEL CCRSUMFILCY (LF"-FUEL/F".): 6969.5 GT AT SYSTEM HP: 8261.2

THEPPAL EFFICIETY: CGLAS: 0.417 GT AT SYSTEM HP: 0.352

MASTE HEAT RECOVERY UNIT DESIGN RLN

CAS	GAS TIKEINE	
	RATAK HINSEPTURES ESSO.O. APPROXIMATE CURRESPONDING SHIP SPEED: 16.0 KTS EXHAUST GAS FEUM RATE: 32 do41.3 LBW/HR (91.3 LPW/SEC)	P SPEED: 16.0 KTS
HEA	HEAT EACHDWIER WEINETRY	
	CVERALL OLNEWSIONS:	NUMBER OF ROMS PER PASS: 1.
	E E E E E E E E E E E E E E E E E E E	NLMBER CF TLBES PER ROW: 32.
	9 507 mg 65 65 65 65 65 65 65 65 65 65 65 65 65	TUBE LENGTH 12. FT.
	GUISTON TIME JIAMETER: 2.3 IN.	MUTSIDE AREA/PASS: 3264. 5 50.FT.
	TABLE TO THE TEXT OF THE TEXT	INSIDE AZEA/PASS: 187.5 SO. FT.
	FILS STOCKS 5.54 FINS/IN.	FFCNTAL BREEF 143.5 SC. FT.
	111 Tali Ka 55: 0.046 IN.	NUMEER OF PASSES: 17. (TOTAL)
	TRAMSVLASE TUBE SPACING: 4.50 IN.	SOLLING SECTION: 6 (HEA
	LONG HILL INAL THAT SPACHICE 3.93 IN.	

04.5 ICMP. IN GAS TEMP. DUT FLUID TEMF. IN FLUID TEMP. DUT REVINEDS NUMBER (AVG.) 513.4 430.5 15018.2	129121.1					
FLUID TEMP. 011T	486.3					
FLUID TEMF. IN 200.0	486.3	E= 486.3 F)				
IN GAS TEMP. DUT	513.4	STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE= 486.3 F)	R.	N H20		
	1,001	JU.U PSIA (5	17 "FL 6.00222	JH CP: 4.1 1		
SECTI NA	SUPERFER PIG	STEAM PRESSURE: 6	STEAM FLOA FITE: 22200.9 LIWAIR.	SA 5-51 JE PAESSURE JECP: 4.1 IN HZD	PINCE STUTE 47419	

CONDENSER PRESSURE: 4.00 IN. HG STEAM TURBINE EFFICIENTY: 0.85 FW HE TER PRESSURE: 15.0 PSIA LHV OF FUEL: 1840C BTU/LR ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HD: 5371.5 SPECIFIC FUEL CENSUPETION (LEW-FJELZPP-HR): 61 AT SYSTEM HP: 0.479 CT AT SYSTEM HP: 0.289 STEAM FUSGINE SMAKE OF THE LOVUE 25.5 PERCENT FUEL CENSTAFFION (LET-FULL/FG.): THERPAL LEFT CLENCY: COGAS: 0.350 STEAM THREINE NCHS EPCWER: 2862.3 TOTAL SYSTET hitsenames: 11211.4 GT HOP SEP IMPOUNT VISEUS: 8349.2 SYSTEP FEFF CAPANCE

HEAT EXCHANGIE PERFUNNAVCE

(HEATING LENGTH= 0.3 FT.)

WASTE HEAT RECOVERY UNIT DESIGN RLN

HARKE HARSEPHER: 1684.0, APPRAKIMATE CARRESPANDING SHIP SPEED: 9.0 KTS EXHANT GAS TEMPERATURE: 083.3 F EXHAIST GAS FLOW RITE: 159731.0 LBM/HR (44.4 LBM/SEC) GAS TURBINE

NUMPER OF ROMS PER PASS: HEAT TABYSTER SULFACE TER: 2.0 IN.
10.1511/2 (1045) 11.00 FEF: 1.9 IN.
10.167/1 (1045) 10.00 FEF: 1.9 IN.
10.167/1 (1045) 10.00 FEF: 1.9 IN.
10.167/1 (1045) 10.00 FEF: 1.00 IN. TRANSVERSE TUBE SPACINGS 4.50 IN. DVERALL DIMENSIONS: FT. | 12.0 FT. | 12.0 FT. | 12.0 FT. | 13.0 FT HEAF EXCHANGER LENNETRY

(BEILING LENGTH 2.9 FT.) OUTSIDE AREA/PASS: 3264.9 50.FT. INS IDE AREA/PASS: 187.5 50. FT. FRANTAL AREA: 143.5 50. FT. NLYBER OF TUBES PER ROWS TLBE LENGTH 12. FT.

NLWRER OF PASSES: 12 (TOTAL)
HEATING SECTION: 3
4021 10 SECTION: 6
SUPERHEATING SECTION: 3

HEAT EACHANGER PERFORMANCE SECT 10N

LONGITUTION TUBE SPACING: 3.90 IN.

SAS TEYP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMF. DUT REYNJLDS NUMPER (AVG.) 5426.1 47057.9 STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE: 486.3 FI 200.0 466.3 486.3 STEAP FLEE FATE: 8286.4 18M/HR. 5.43. 5.883. SLPERNEAFING

0.8 IN H20 GAS-SIJE PRESSURE UPOP: PINCH PEINT: 41.3 F

SYSTEM PLAFORMYRCE

GONDENSER PPESSURE: 4.08 IN HG STEAM TURNINE EFFICIENCY: 0.85 FW HERSPURE: 15.0 PSIA LHV OF FIEL: 1840G STUVLH ASSUMED SYSTEM CHARACTERISTICS: SPECIFIC FULL CLASSIMFTICN (LBM-FJEL/PP-HR): 6.873 STEAM TOWALTE SHARE OF THE LOAD: 39.3 PERCENT STEAM TERMINE HERSEPEMER: 1372.3 TETAL SYSTEM HORS EPONER: 2733.3 CT HERSEPHARPIREVISEDI: 1660.4

GT AT SYSTEM HP: 0.158 THEPPAL EFFICIENTY: COGAS: 0.214

FILE CENSUMETER IL BY-HIH / FR - 1: 166.0

GT AT SYSTEM HPE 2385.9

200

CB/22/75 .12.46.51

WASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURBINE

PRAKE HIRIEPINER: 16421.0, APPROXIMATE CORRESPONDING SHIP SPEEC: 20.0 KTS EXFANST 645 TERPERATURE: 849.0 F EXHALST GAS FLCH RATE: 4.7549.0 LBP/HR (113.2 LBM/SEC)

HEAT EXCHENSER SECMETER

CVERAL CIMEISTRIS: FT. ALDAR H. 12-0 FT. ALDAR H. 12-1 FT. FT. FT. FT. FT.

FAT TAYISTE SUFFACE DATE THE TAY IN TASE TO SELECT TO SELECT THE TAY IN THE TAY IN TAY IN TAY IN TAY IN TAY IN THE TAY IN

NUMBER OF PASSES: 15 (TOTAL)
HEATING SECTION: 6
ROLLING SECTION: 7
SUPERHEATING SECTION: 2

FPCATAL AREA: 144.8 SC. FT.

ALTSIDE AREA/PASS: 3290.5 SC.FT. INSIDE AREA/PASS: 189.0 SC. FT.

NUMBER OF TUBES PER ROW: NUMBER OF ROWS PER PASS :

TUBE LENGTH 12. FT.

(HEATING LENGTH: 9.3 FT.)

MEAT EXCHANGE PEHFORMFICE

LUNGITUDINAL THAT SPACING: 2.52 IN.

THANSVLASE THEL 'Put ING: 3.18 1%.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. NUT REYNNLDS MUMPER (AVG.) ATILITIES ING SEFFIN

223123.4

STEAM PRESSULE: CUC.C PSIA (SATURATION TEMPERATURE 446.3 F)

5.6 IN H20 STEAM FLOW PATE: 39239.4 LAM/HR. GAS-SIJE PRESSUNE DRCP:

PINCE PARTY: 40.1 F

SYSTEM FERFCHMANCE

STEAP THEGINE HORSEPCHEP: 5080.8 UT HTRSEPUMERIREVISEDI: 16031.2

CONDENSER FRESSLRF: 4.08 IN HG STEAM TURNINE FFFICIENCY: 0.85 FW HEATER PRESSURE: 15.0 PSIA LINU DF FOEL: 16400 BTL/LBM

ASSUMED SYSTEM CHARACTEPISTICS:

STEAM TURNING SHARE OF THE LOAD: 24-1 PERCENT TOTAL SYSTEM HIRSEPINER: 21112.0

GT AT SYSTEM HP ! SPECIFIC FIEL CERSIMPTION (LIN'-FIEL/FP-HR): J. DALY: 0.436 CGAS: 0.331 GT AT SYSTEM HP1 FALL C PTS 1907 1794 (LR4-FIELZIP. 1)

8257.6

0.391

GT AT SYSTEM PP: 0.354 THEWALL EFFICIENCY: COGAS: 0.417

MASTE HEAT RECOVERY UNIT DESIGN RUN

CAS TURBINE

(BALLING LENGTH: 3.5 FT.) OLTSIDE AREA/PASS: 3250.5 SC.FT. INSIDE AREA/PASS: 189.0 SC. FT. NUMBER OF PASSES: 13 · (TOTAL)
HEATING SECTION:
60111NG SECTION:
7 FFONTAL AREA: 144.8 SO. FT. NUMBER OF TUBES PER ROW: NUMBER OF ROWS PER PASS : TUBE LENGTH 12. FT. APANCE HONSEPOWER: 6526.0, AFPROXIMATE CONNESPONDING SHIP SPEEC: 16.0 KTS EXFANST 645 TEMPER 1742.0 F EXHALST 645 FLOW FATE: 324641,0 18M/HR (91.3 LBM/SEC.) FIT FELLY: 0.8 10. FINSTIN. FIT FELLY: 0.8 10. LONGITUDINAL TURE SPACING: 2.92 IN. TRANSVERSE THEE CHACINGS 3.38 IN. FENT TRANSPER SHAFTCE GUTSILE THRE SIA INSINE TURE DIAM TUBELLE IN AREA TOE HEAT EXCHANSER GEUMETRY

FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMPER (AVS.) 14511.6 122571.C STEAM PHESTURES DUD DE 14 (SATURATION TEMPERATURE= 486.3 F) LAS TEMP. IN GAS TEMP. DUT GAS-SILE PAESSURE CREP: 3.3 IN HZD SIERM FLOW RITE: 21557.0 LBMAIR. PINCH PANAT: 37.1 F HEAT EXCESSIVER PERFORMATCE PEAT PIG SCALLING SUPERHEATERS SEC 11 OIL

CONDENSER PRESSURE: 4.08 19. HC STEAN TURBINE FFFICIENCY: 0.85 HW HEATER PRESSURE: 15.0 PFIA LHV CF FUEL: 18400 BTU/LHM A SSLMED SYSTEM CHARACTERISTICS: FLEE CONSUMPTION (LEFT-FUEL/HR.): OF TH PE 4412.0 FOSSE 4432.6 GT AT SYSTEM HPE 5308.1 0.475 GT AT SYSTEM HP: 0.289 SPECIFIC FUEL COMEDIATION (LAP-FUEL/HP-HR): ET PILY: 0.553 CUGAS: 0.396 GT AT SYSTEM HP: STEAM THEEINE SHARE OF THE LUAC: 25.3 PERCENT CO34S: 0.349 STEAM TURNINE HINSEPOWER: 2837.8 131AL SYSTEM HJRSEPOWER: 11201.1 GT HCFSEFOWERIREV IS ECH: 8363.3 THERPAL EFFICIENCY: SYSTEM PERFORMANCE

CE/22/15 13.C1.14

WASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TUREINE

BSTACE HORSEPORES 1684.0. APPROXIMATE CORRESPONCING SHIP SPEED: 9.0 KTS EXPANSI (A) FEM-ENTHRE: 089.0 F EDAMEN (44.4 LBM/SEC)

HEAT EXCHANGER GECMETHY

CVERAL CITE SIDIS: FT. 61.01 FT. 61.

HEAT 19 A 4 SEE & S.D. FACE TO THE SEE TO SE

FILE FELCEFT: 0.8 IN.
FIN TALKWESS: 0.036 IN.
TRANSVERSE TIEE : PACING: 0.38 IN.
LOYGITJOJIAL TOSE SPACING: 2.92 IN.

NUMBER OF RCMS PER FASS: 1.
NUMBER OF TUBES PER ROW: 43.
TUBE LENGTH 12. FT.

OUTSIDE AREA/FASS: 3290.5 SO.FT.
INSIDE AREA/PASS: 189.0 SC. FT.
FRONTAL AREA: 144.8 SQ. FT.

NLMAFA OF PASSES: 9 (TOTAL)
2 HEATING SECTION: 5 (HEATING LENGTH* 4.7 FT.)
80PERPEATING SECTION: 2 (BOILING LENGTH* 6.5 FT.)

HEAT EXCEPTIBLE PERFIRMANCE

SEC 11 3N

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) 5146.9 44092.8

STEAM FLOW RATE: BC43.7 LBPAHR.
CAS-SLOE PRESSURE CFFP: U.6 IN H20

PINCH POINTS 54.5 F

SYSTEM PEPI IR 44'ICE

CONCENSER PRESSURE: 4.08 17, HC STEAM TURRINE FFFFCIENCY: 0.85 FW HEATER PRESSURE: 15,0 P.SIA LHV OF FUEL: 18400 BTU/LRM A SSUMED SYSTEM CHARACTERISTICS: STEEN FURBLINE HORSEPCHER: 1039.6 TUTAL SYSTEM HORSEPONER: 2700.5 1661.0 CT PERSEFENCE HIREVISEED:

STEAP TUPOINE SHIFTE OF THE LIAC: 38.5 PERCENT SPECIFIC FUEL CUNSUMPTION (LAM-FUEL/HP-HR): 61 THEY: 1.03 COAS: 0.654 GT AF SYSTEM HP: 0.878

FULL CONSUMETION (LUM-FUEL/HR.): 61 AT SYSTEM HP: 2370.0

THERMAL EFFICIENCY: COJAS: U.ZII GT AT SYSTEM HP: 0.158

08 /22/79 13.16.58

RUN #16

MASTE HEAT RECOVERY UNIT DESIGN RUN

BHAKE HCAREPOWER: 16421.0. APPRIXIMATE CIRRESPINDING SHIP SPEED: 20.0 KIS FAMAUST GAS TEMPERATURE: 849.0 FUMIN ILLS.2 LUPVISECI EXFAUST (AS FLIM RITE: 4.37549.0 LUMIN ILLS.2 LUPVISECI EAS TURBINE

DVERALL DI PENSIONS: 1 175111: 12-0 FT. 11711: 12-0 FT. HELS-11: 2-0 FT. HEAT EXCHANGES GENTETRY

(BEATING LENGTHE 5.1 FT.) OUTSIDE AREA/PASS: 3264.9 SQ.FT. INSIDE AREA/PASSI 167.5 SO. FT. NUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION: 6
801110 SECTION: 6
SUPERHEATING SECTION: 2 FPUNTAL AREA: 143.6 SC. FT. NUMBER OF TUBES PER ROWS NUMBER OF ROWS PER PASS: TLBE LENGTH 12. FT.

HEAT EACHANJER PERF JAMANCE

LUMBITUDITAL TUBE SPACING: 1.95 IN.

TRANSVERSE TUSE SPACINGS 2.25 IN.

FLUID TEMP. IN FLUID TEMP. DUT REYN'LDS NUMBER (AVG.) 230765.6 STEAM ARESSILLE: 6JU.D PSIA (SATURATION TEMPERATURE= 486.3 F) GAS TENP. DUT \$10.9 645-5166 PRESSURE DRUPE 4.9 IN H20 GAS TEMP. IN STEAM FLCh RATE: 39 159.0 LBM/HR. HENTING HOLL 116 SEPERHEATING SECTION

PINCH PUBLIT: 48.4 F

SYSTEM PERFURPANCE

ASSUMED SYSTEM CHAPACTERISTICS: STEAM THRAINE SHAKE OF THE LOAD: 24.6 PERCENT STEAM ILRHINE HORSEPCWER: 5232.3 TETAL SYSTEM HIRS ENGLER: 21285.7 GT HCF SEPT4ER (# EV ISED 1: 16053.3

CONDENSER PRESSURE: 4.CE IN. HG STEAM TIPPINE EFFICIENCY: 0.885 FW HER SPRESSURE: 15.0 DSIA LHY OF FUEL: 18400 RTU/LHW

SPECIFIC FUEL CONSUMPTION (LAM-FIEL/MP-HR): 6.387 GT AT SYSTEM HP: 0.387 GT AT SYSTEM HP: FIRE CONSUMPTION (LET-FIEL / HR.): 6997.7

0.357 GT AT SYSTEM PP: CCGAS: 0.421 TREADER CHETS HENCY:

206

2

1

1

WASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURBINE

CA/22/75 14.12.23

HEAT EXCHANSER GECNETRY

OVERALL CIVENSITYS: LENGTH: 12.0 FT. HITH: 12.0 FT.

1 .08 FINS/IN. HE TT 1:15FE SUF CE 10 51DE TIBE DIAMETER 10 51DE TUBE DIAMETER 10 8E/FI - A21 CREVEN FIN TYPE: EGMEN E FIN SPACING: 0.5 I

LONGITUE II AL TUBE SP CINGS 1.95 IN. 2.25 IM. TRANSVERSE TIBE PACITIG

NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS :

TUBE LENGTH 12. FT.

DUTSIDE AREA/PASS: 3264.9 SO.FT. 187.5 SO. FT. FRCNTAL AREA: 143.8 SO. FT. INSIDE AREA/PASS #

(HEATING LENGTH- 2.5 FT.) NUMBER OF PASSES: 10 (TOTAL)
HEATING SECTION:
BOILING SECTION:
SUPERFEATING SECTION: 2

HEAT EXCHANGER PE FIRMWICE

FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVS.) 126 956 .9 GAS TEMP. IN GAS TEMP. DIST 512.0 BOLLING SUPE SHEATING SEC TI CN

STEAM PRESSURE: 630.0 P. LA (SATURATION TEMPERATURE 486.3 F)

GAS-SIDE PRESSURE CRCP: 2.8 IN H20 STEIN FLOW RITE: 21564.0 LRHAM.

PINCE PRINT: 36.7 F

SYSTEM PERF RMA CE

ASSUMED SYSTEM CHARACTERISTICS: STEAT TURBINE HIS SEPTINFRE 2828.4 TOTAL SYSTEM HORSEPONER: 11200.7 GT HORSE POWERINEVI EDI: 8372.4

CONDENSEP PRESSURE: 4,00 IN HG STEAM TURBLINE EFFICIENCY: 0,05.85 FINE PRESSURE: 15,0 PSIA LHV OF FILEI: 18400 BTULLEN

SPECIFIC FUEL CHISCHPTION (LEM-FUEL/HP-HR): STEAM TLABINE SHARE CF 'HE LOAD: 25.3 PERCEIT

GT AT SYSTEM HP: 5368.0 FUEL CONSUMPTION (LBM-FUEL /HR.):

C36451 0.349

THE MYLEFF! IEN'Y:

GT AT SYSTEM HP1 0.289

08 /22 /79 14.21.08

WASTE HEAT RECOVERY UNIT DESIGN RIIN RUN #18

G S TURAINE

PRINK HORSEPINGER: 1684.0. AFPROXIMATE CHRRESPINGING SHIP SPEEDS EXFANCT GAS (EMPIRATIONE: 689.0 F Extanct GAS FIN OFFE: 159731.0 [BM/HR (44.4 LBM/SEC)

EXCHANGER GEOMET RY HEA NEGALL DIMENSIONS:

FIN TYPE SENENTED FINS IN. FIN HEIGHT 0.5 IN. FIN HEIGHT 0.5 IN. FIN THE NIESS: 0.024 IN. HEAT TRANSFER SUBFACE UTSIDE TUNE DI M IN IDE UBE CIAME TUNE/FIN AMENNEM

LONGITUDINAL TUBE SPACING: 1.95 IN. TATHSVERSE TUBE STOINGS 2.25 IN.

NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS :

OLTSIDE AREA/PASS: 3264.9 SO.FT. TLBE LENGTH 12. FT.

INSIDE AREA/PASS: . 187.5 SO. FT.

FRONTAL AREA: 143.8 SO. FT.

NUMBER OF PASSES: 7 (TOTAL)
HEATING SECTION: 3
SUPERHEATING SECTION: 2

(HEAT ING LENG "HE 4.4 FT.)

HEVT EX'T NUER PERFORMANCE

SEC TON

GAS TEM". IN G'S TEMP. DUT FLUID TEMP, IN FLUID TEMP. DUT REYNOLDS NUMFER (AVG.) B) IL 1.6 SLPERHEATING

STEAM PRESSU E: 600.0 PSI: (SATURATION TEMPERATURE. 486.3 F)

0.5 IN # 20 STEAP FLCW RATE: 1992.5 LBM/HR. GAS-SIGE PF ESSUIE DK 191

PINCH POINTE 33.1 F

SYSTEM PERF CREAMCE

STEAM TLABINE HOR EPCWER: 1028.3 TO AL .YS'EY HOR EPINERS 2689.7 GT HIRS ED IMERINEN ISED 1: 1661.4

CONDENSER PRESSURE: 44CB IN HG STEAT TITRETTE EFFICIENCY: 0485 FW HEATER PRESSURE: 150 PSTA LHV OF FUEL: 18400 ATUZEM

ASSUMED SYSTEM CHARACTERISTICS

SPECIFIC FUEL CONSIMP ION (LBM-FJEL/HP-HR): UT ONLY: 1.063 COSAS: 0.657 GT AT SYSTEM MP: 0.879 STEAT TURBLIE SH E JF THE LOUDS 38.2 PERCENT

GT AT SY: FEM HP1 2364 .6 FILEL COASUMP 104 (184-FIEL/H: 1: 165.2

HERPAL EFFICIENCY: COGAS: 0.211 . G' AF SYSTEM HP: 0.157

08/22/19 14.35.21

MASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURBINE

RRIME HIPSEM WET 14421.0. APPROXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS Familis GA Ferpealing 10.0 DBW/HR 1113.2 LBM/SEC) Familis GIS CLOM Rates +0.7589.0 LBM/HR 1113.2 LBM/SEC)

HEAT EX HINGER GEOMETRY

OUTSIDE THE DIAMETER: 2.3 IN.
OUTSIDE THE DIAMETER: 1.9 IN.
118 LIN THE UNITER: 1.9 IN.
118 LIN THE UNITER: 2.9 IN.
FIN HE UNITER: 1.0 10.048 IN. CVERALL DIMENSIONS: LENGTH: 12.0 FT. HIDTH: 12.0 FT.

PEAT

OUTSIDE APEA/PASS: 3264.9 SO.FT. INSIDE AREA /PASS : 187.5 SO. FT. FRONTAL AREA: 143.5 SC. FT. NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS : TUBE LENGTH 12. FT.

(BOILING LENGTH 1:3 FT.) NUMBER OF PASSES: 15 (TOTAL)
HEATING SECTION: 5
SUPERHEATING SECTION: 2

HEAT EXCHANGER PERFORMAICE

LONG! HOINAL TUBE : PACTIG: 3.93 IN.

TRANSVERSE TUBE FACING: 4.50 IN.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NIMPER (AVG.) POLLING SUPERHEAT 146 SETTION

STEAM PRESSURE: 400.0 PSIA ISATURA ION EMPERATURE. 444.6 F.)

STEAM FLOW 4'TE: 38942.0 LAM/HR.

GA 5- SI DE PRESSURE DRCP: 5.3 IN H20 PINCH PARTY 11.9 F

SYSTEM PERFIRMA CE

ASSUMED SYSTEM CHARACTERISTICS: STEAM TURBINE SHARE OF THE LOAD: 23.1 PERCENI STEAM URBINE HIS SEPTMER: 4821.6 TOT'L SYSTEM HORSEPONER: 20861.1 GT HORSEPOWERIREVISEDI: 16039.5

CONDENSER PRESSURE: 4,00 IN. 85 STEP TURBINE EFFICIENCY 0.085 FW HEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 8TU/LBM

"PECIFIC FUEL CONSTANTION (LBN-FUEL/M-HR.):
GT OALY: 0.435 COGAS: 0.335 GT AT SYSTEM HP: 0.396

GT AT SYSTEM HP: 0.345 GT AT SYSTEM HP: FUEL CHISUMPT ING JLBM-FUEL (HR.) 1895.8 ChGAS: 0.412 THE G CALY: 0.317

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CB/22/79 14.56.50

VASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURBINE

PRINCE HINGSEO MEUT. 8526.0. SPPROXIMATE CORRESPONDING SMIP SPEEDT 16.0 KTS EXNALST GS ENDERFACION TO TO TO THE TOTAL TO T

HELT EX P NOTR DEDMETRY

CVERALL CIMENS JONS: FT. LENGTH: 12.0 FT. HEIGHT: 5.2 FT.

RAN FER THR FACE
OUTSIGE TUBE DIAMETER: 2.0 IN.
115 IDE TUBE OF SETEN: 1.9 IN.
1 6E FF II ARRADGERS: 2C THRISTED
LIN TYPE I CE THRISTED 7F11 ARREDGETER 1
IN TYPE SESMINED
FIN HELLOH 1 LO IN.
FIN HELLOH 1 LO IN.
FIN HELLOH 2 LO IN. HEAT

LONGI ILLINAL TUBE PACTIG: 3.93 IN. TRANSVERS TUBE SPACINGS 4.50 IN.

OUTS10E AREA/PASS: 3264.9 50.FT. NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS 1 TUBE LENGTH 12. FT.

F PONTAL AREA: 143.5 SO. FT.

INSIDE AREA PASS: 187.5 SQ. FT.

(HEATING LENGTH 3.3 FT.) NIPBER OF PASSES: 16 (TOTAL)
HEATING SECTION:
BOLL ING SETTION:
SUPERHEATING SECTION:
3

HEAT EXCHANGER PERFORMANCE

FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) SAS TEMP. IN GAS TEMP. DUT SOLL THE TING SETTIN

143729.1

STE'N PRESSURE 1 400.0 PSIA ISA URATION TEMPERATURE 444.6 F)

GAS-SIDE PRESSURE JROP: 3.8 IN 120 TEAP FLC4 RATE: 23 807.4 LB4/HR.

PINCH PCIN: 42.4 F

SYSTEM PEPFCRPANCE

STEAP HEBINE HORSEPHERE 2942.6 LT HUP SEPUMERIRE VISEUDI 8354.6

STE M TLRBINE SHARE OF THE LOAD: 26.0 PERCENT TOTAL SYSTEM HOF SETTMER: 11297.3

STEAM TURS IN E EFFICIENCY 0 18 5 5 1 H HEAT TURS IN E EFFICIENCY 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM

ASSUMED SYSTEM CHARACTERISTICS:

GT AT SYSTEM HP : 5399.8 PECIFIC FIEL CONSUMPTION IL BY-FJEL/HP-HR JE SYSTEM MPE FUEL C 175 140 174 1LR4- FJEL J.R . 1431.7

GT AT SYSTEM HP: 0.285

C164: 0.353

THERMAL EFF IC IET VE

Ud /22/79 15.19.43

RUN #21

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Cr. T. S. la ...

WASTE HEAT RECOVERY UNIT DESIGN RUN

G'S TURH INF

BRAKE HOR EPUMER: 1684.0. APPRIXIMATE CIRRESPONDING SHIP SPEED: 9.0 KTS EXHAUST GAS TEMPERATURE: 669.0 FENTAN (44.4 LBF/SEC)

DVERALL DI MENSI DNS: FT. 12.0 FT. WID-N: 12.0 FT. HEIGHT: 4.2 FT. EXCHAIGER GEIMETTY HEA

HEAT TRANSFER SURFACE (UTSIDE TO IN. UN DE UNE DIATER! 1.9 IN. UN DE LATER! 1.9 IN. UN DE LATER I SECURITER! 1.9 IN. UN DE LATER I SECURITED FIN PACI IG: \$5.94 FINS IN. FIN FILT THE KIESS! 0.048 IN.

LUNGITLDINAL TUBE PACING: 3.93 IN.

(HEATING LENGTH- 0.7 FT.) DITSIDE AREA/PASS: 3264.9 SO.FT. INSIDE AREA/PASS: 187.5 SQ. FT. NUMBER OF TUBES PER ROWS 32. FRONTAL AREA: 143.5 SQ. FT. TUBE LENGTH 12. FT.

NUMBER OF ROWS PER PASS:

NUMBER OF PASSES: 13 (TOTAL)
HEATING SECTION:
BOIL ING SECTION:
SUPERHEA'ING SECTION:
3

HEAT EXCHANSER PERFORMANCE

G'S TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMPER LAVG.) 5951.7 56273.6 STE M PRESSURE: 400.0 PSIA (SATURATION TEMPERATURE- 444.6 F) HEATING BOILING UPERHEATING SECT1 ::1

TEAM FLOW RATE: 9494.3 LBM/HR.

GAS-SIJE PRESSURE OROP: 0.8 IN 120

PINCH FCIN : 30.1 F

SYS 'EN PEPFCRPANCE

CONDENSER PRESSURE: 4,08 1% HG STEAM TURNE FFFICIENCY: 0,855 FW HEATER PRESSURE: 15,0 PSIA LIVO F VEL: 18400 BTU/189 ASSIMED SYSTEM CHARACTERISTICS: STE M TURRINE SHARE OF THE LOADS 41.4 PERCENT STEAP TURBINE HUR EPCWER: 1171.5 TO AL SYSTEM HIS EVINERS 2831.8 GT HOR SE POWER (REVISED) : 1660.3

PECIFIC FUEL CONSIMP TON ILAM-FIEL/HP-HRIS GT A SYSTEM HP! FUEL CONSUMPTION TEBM-FIEL /HP. 1: 706.0

THEN A EFFI IE! Y: COGA : 0.222

GT AT SYSTEM IP:

2

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MASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURRINE

PARKE PORTEPUNER: 16421.0. APPRIXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS MATE) GAS TEMPERATURE: 649.0 F STF. UST GAS FLIM ATE: 407569.0 LBM/HR 1113.2 LBM/SECI

HEAT EXCRANGER CE METHY

OVERALL OLMENSION: F. LEVETH: 12.0 FT. HEIGHT: 2.9 FT.

HEAT TAANSFER SURFACE OLTSIDE TUBE DIA FEERS TOBE FEED ARE GLANFEERS

LONGITLDINAL TUBE PACING: 2.92 IN. TRANSVERSE TUBE SPACINGS 3.38 IN.

HEATING LENGTH 3.5 FT. OUTSIDE AREA/ PASS: 3290.5 SO.FT. INSIDE AREA/PASS: 189.0 SO. FT. NUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION:
BOILING SECTION:
SUPERHEATING SECTICN: 2 FRONTAL AREA: 144.8 .50. FT. NUMBER OF TUBES PER ROWS NUMBER OF ROWS PER PASS: TLBE LENGTH 12. FT.

HEAT EXCHANSER PERFORMANCE

FLUID TEMP. IN FLUID TEMP. DIT REYNOLDS NUMPER (AVG.) 231167.1 STE'M PRESSURE: 400.0 PSIA (SATURATION TEMPERATURE +44.6 F) GAS TEMP. IN GAS TEMP. DUT 931, 113 SUPERHEATING S ECT 1 ''

STEAP FLCW PATE: 38942.0 184/18.

GAS-SIJE PRESSURE DROP: 4.4 IN H20 PINCH PCINT: 71.5 F

SYSTEP FEEF CHMANCE

STEAM THREINE NORS EPONER! 4804.9 TOTAL SYSTEM HIS SPUNER: 20873.6 GT HJF SEPTHERIREVISEDI: 16068.7

CONDEMSER PRESSURE: 4.08 IN HG STEAM TURRINE EFFICIENCY: 0.855 FW HEATER PRESSURE: 15.0 PSTA LHY OF FUEL: 18400 BTULEN

ASSUMED SYSTEM CHARACTERISTICS:

PECIFIC FIEL CONSUMPTION (LBM-FUEL / PP-HR): SYSTEM HP: 0.396

STEAM TURNINE SHARE OF THE LOAD: 23.0 PERCENT

FULL CHSUMPTION (LBM-FUEL/HR.): GT ONLY: 6949.8 CUGAS: 6999.8 GT AT SYSTEN HP: GT AT SYSTEM HPE CD GAS: 0.412 THE SULL EFF ! IEN Y:

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MASTE HEAT RECOVERY UNIT DESIGN RITH

BRIKE HORSEPOWER: 8526.0, APPROXIMATE CORRESPONDING SHIP SPEED: 16.0 KTS EXTRUST (45 TEMPERTURE: 742.0 F EMAIN (91.3 LBM/SE); GAS -URBINE

N'ED FINS/IN. FIX 17PE: EGNEN EU FINS/1P FIN SPACING: 7.92 FINS/1P FIN HEIGH: 0.8 IN. FIN THICKNES:: 0.036 IN. TRAN VEHSE THUE : PAC ING: 3.38 IN. OVERAL FIVENSINS: FT. BLOOM FT. BLOOM FT. BLOOM FT. BLOOM FT. BLOOM FT. HEAT EXCHANGER GECHETRY 1.3

(BOILTING LENGTH: 3.2 FT.) OUTSIDE AREA /PASS: 3290.5 SO.FT. INSIDE AREA/PASS: 189.0 SO. FT. NUMBER OF PASSES: 13 (TOTAL)
HEATING SECTION: 7
SUPERIERIING SECTION: 7
SUPERIERIING SECTION: 2 FFONTAL AREA: 144.8 SO. FT. NUMBER OF TUBES PER ROWS TUBE LENGTH 12. FT.

NUMBER OF RCMS PER PASSE

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REWIGLDS NUMBER (AVG.) 139551.1 STEAP PRE SURE: 430.0 PS IA ISATURATION TEMPERATURE. 444.6 F) 3.2 N H20 STEIN FLOW RATE: 23545.2 LBMAIR. GA- 1DE PRESSURE CRIP: HEAT EXCHANGEN PERFIRMANCE BOILING SUPERIFEATING SEC TI ON

A SSUMED SYSTEM CHARACTERISTICS: SP E' JE LE GONSUMPTION (LBM-FUEL /HP-HR): G GALY: 0.530 CAGAS: 0.392 GT AT SYSTEM HP: STEAP TLEBINE SHARE CF 'HE LOAD: 26.0 PERCENT 2931.5 TOTAL SYSTEM HIR SEPONER: 11276.5 GT HORSEPONERIREVI EDJ: 8365.0 STEAM TURNINE HIS SEPTIMEN: SYSTEM DERF IRMATICE

PIN'T POINTS 41.5 F

CONDENSER PRESSURE: 4.08 IN. HG STEAM TURBINE EFFICIENT'S 0.85 FW HEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM

FUEL DISCUMPTION (LBM-FUEL AIR.): GT AT SYSTEM HP: 5399.5 THEP HEL EFF! LENCY:

GT AT SYSTEM HP: 0.289

C364S: 0.352

213

LONGITUETIAL TUBE SP.CING: 2.92 IN.

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MASTE HEAT RECOVERY UNIT DESIGN RUN

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PRAKE HORSEPONER: 1684.0. APPROXIMATE CORRESPONDING SHIP SPEED: 9.0 Eariust Gas Temperiture: 689.0 F Earainst Gas Flow Rate: 159731.0 Lam/HP (44.4 LBW/SEC)

HEAT EXCHANGER GECHETRY

MER'LL DIMENSIONS:
LENGTH: 12-0 FT.
HE IGHT: 2-4 FT.
HEAT TRANSES SILESE

HEAT TRANSFER SUFFACE IN INS IN. 118 IN. 118 IN. 118 EN IN.

INSIDE AREA/PASS: 189.0 SO. FT.
FRINTAL AREA: 144.8 SQ. FT.
NUMBER OF PASSES: 10 (TOTAL)
HAT ING SECTION:
SUPERHEATING SECTION: 2 (BOILING LENGTH= 0.2 FT.)

DLTSIDE AREA/PASS: 3290.5 SQ.FT.

NUMBER OF ROWS PER PASS: NUMBER OF TUBES PER ROWS

TLBE LENGTH 12. FT.

HELT EXTENSER PERFORMANCE

LONGITUDING TUBE SPACING: 2.92 IN.

TR: HSVERSE TUBE SO CINGS 3.38 IN.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FILLID TEMP. DUT REYNOLDS NUMPER (ANG.) 53585.1 STEA" PRESSU E: 400.0 PSIA (SATURATION TEMPERATURE. 444.6 F) 412.6 STEAM FLCh RATE: 9425.4 LBM/HR. HEATING HOLL TIG SUPERHEATING SEC. 10N

PINCH POINT: 33.6 F

0.7 IN 420

GAS-SICE PRESSUPE DROPE

SYSTEM PERF CRPANCE

CONDENSER PRESSURE: 4.08 IN HG STEAM TURBINE FFICIENCY: 0.85 FERENCE FOR 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: SPECIFIC FUEL CONSIMPTION ILBM-FIEL/HP-HRI: GT ONLY: 1.063 COGAS: 0.626 GT AT SYSTEM HP: 0.860 STEAM TURBLUE SHIVE OF THE LOADS 41.1 PERCENT STEAM TLABINE HURSEPCWER: 1161.0 TO'AL SYSTEM HOR EPOMER: 2821.9 GT HIRS EPINE (19 EV ISED II 1660.9

GT AT SYSTEM HP: 2428-1

FUEL CONSTRPTION (LBM-FILEL/HR.): GT ONLY: 1766.1 COGAS: 1766.1 GF A' SYSTEM HP: 0.161

CUGAS: 0.221

HERPAL EFF ICIENCY:

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WASTE HEAT RECOVERY UNIT DESIGN RUN

	KTS	
	20.0 KTS	
	SPEEDS	
	G SHIP	/S EC.)
	E SPONDI N	3.2 1.84
	MTE CORR	/HR (11)
	APPROXIM	0.6
	HALKE HIRSEPHERE 16421.00 APPROXIMATE CORRESPONDING SHIP SPEED	E 1 40758
	WE'S	LOL RAT
Ę	H JRSEP	ST GAS
AS TLABIN	HRAKE	EXHAL
A S		

OUTSIDE AREA/PASS: 3264.9 SQ.FT. INSIDE AREA /PASS: 187.5 SQ. FT. NUMBER OF PASSES: 9 (TOTAL)
HEATING SECTION: 5
SUPERHEATING SECTION: 1 FRONTAL AREA: 143.8. SQ. FT. NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS : TUBE LENGT 12. FT. LONGITUDINAL TUBE SPACING: 1.95 IN. FIN TPE: SECHENTED FINS/IN. FILE THICK-LESS: 0.024 IN. TRANSVERSE TUBE PACING: 2.25 IN. CVERALL CIMENSIONS: LENGTH: 12.0 WIDTH: 12.0 HEIGHT: 1.5 HEAT EXTENDER GEOMETRY HEAT

GAS TEMP. IN GA" TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) 23810.6 213343.7 STEAM PRESSURE: 400.0 PSIA (SA'URA'ION EMPERATURE 444.6 F) STEAM FLOW RATE: 38643.0 LBM/HR. SUPERFERENCE SUPERFERENCE SETTION

(BOILING LENGTH- 8.3 FT.)

STEAM FLOW RATE: 38643.0 LBM/HR. GAS-SIDE PRESSURE DRCP: 3.5 IN H2O PINCE POLIT: 71.9 F

SYSTEM PEFFCRMANCE

ASSUMED SYSTEM CHARACTERISTICS: 0.346 GT AT SYSTEM HPE GT AT SYSTEM HP : SPECIFIC FIEL CONSUMPTION ILBY-FUEL/IP-HR 1: GT AT SYSTEM HP: GT ONLY: 0.435 COGAS: 0.336 GT AT SYSTEM HP: STEAM TURBINE SHARE OF THE LOAD: 22.7 PERCENT FUEL CONSUMP TON (LBM-FJELVIR.): 7033.9 CO GAS : 0.411 STEAP URBINE HORSEPHWER: 4732.7 TOTAL SYSTEM HORSENDMEN: 20831.3 GT HOR SEPOWER (REVISED) : 16098.5 THER AL EFF IC IENCY:

EXCHANGER PERFORMENCE

HEA

MASTE HEAT RECOVERY UNIT DESIGN RUN

RRESPONDING SHIP SPEED: 16.0 KTS 91.3 LBW/SECI	NLWBER OF ROWS PER PASS: 1. NLWBER OF TUBES PER ROW: 64. TUPE LENGTH 12. FT. OUTSIDE AREA/PASS: 3264.9 SO.FT. INSIDE AREA/PASS: 187.5 SO.FT. FRONTAL AREA: 143.8 SQ.FT. NUMBER OF PASSES: 10 (TOTAL) HEATING SECTION: 5 (HEATING LENGTH- 2.4 FT.) SUPERHEA'ING SECTION: 2 (BOILING LENGTH- 3.8 FT.)
645 TURBINE 83 TERNISEPONER: 8526.0. APPROXIMA E CORRESPONDING SHIP SPEED: 16.0 KTS EXHAUST 645 TEMPERTURE: 742.0 F EXHAUST 645 FLUB RATE: 328641.0 LBP/HR (91.3 LBM/SEC)	CVERALL CIMENSIONS: ELENGINE 12.0 FT. HEATTHE 12.0 FT. HEATTHE 12.0 FT. HEATTHE STYRACE OUTSIDE TOUS UITHERS: 0.9 IN. 11 STORE TOUS UITHERS: 0.9 IN. 11 STORE TOUS UITHERS: 0.9 IN. 12 STYLES STORE SEGNETTE FIN SON LIGHT 0.5 IN. 18 NEWSKERS TOUS SPACING: 2.25 IN. LONGI UCINAL TOUS PACING: 2.25 IN.

	(AVS.)								
	REYNOLDS NUMBER	1,789.1						171051	PACOS IN HG
	GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.)	434.0 444.6 635.0						ASSUMED SYSTEM CHARACTERISTICS:	CONDENSER PRESSURE: 4.08 IN. HG
	FLUID TEMP. IN	444.0	E. 444.6 FI		•			ASSUMED	No.
	GAS TEMP. DUT	401.5	ITI ON TEMPERATUR		•				
	GAS TEMP. IN	475.1	D PSIA (SATURA	15.2 LBM/HR.	Pt 2.7 IN 1120			11 6373.6	HER: 2954.5
HEAT EXCHANGER PERFORMANCE	SEC TON	HENTING BOT 116 SUPERIERTING	STEA" PRESSU E: 400.0 PSIA (SATURATION TEMPERATURE. 444.6 F)	STEAM FLCh RATE: 23945.2 LBM/HR.	GAS-SIDE PRESSURE DROPE 2.7 IN H20	PLYCH POINT: 41.1 F	SYSTEM PERFCRPANCE	GT HJAS EPTHET IR EV ISED IS 8373.8	STEAM TURBINE HORSEPCHER: 2954.5
Ŧ							2		

STEAM TURBINE EFFICIENCY: 0.85 FW HEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM GT AT SYSTEM HP: 5410.0 SPECIFIC FUEL CONSIMPTION (LBM-FIEL/HP-HR): Of ONLY: 0,529 CJGAS: 0,39! GT AT SYSTEM MP: 0,478 G' AT SYSTEM HP: 0.290 STEAM TURBINE SHIPE OF THE LOAD: 26.1 PERCENT FUEL CCNSUPTION (LBP-FUEL/HR.): 6 GOAS: 4433.6 CUGAS: 0.353 TOTAL SYSTEM HOR: EPOWER: 11328.3 HERPAL EFFICIENCY:

WASTE HEAT RECOVERY UNIT DESIGN RUN

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MAKE HIRSEP HEST 1684.0, APPROXIMATE CORRESPONDING SHIP SPEED: 9.0 KTS EXMANST DAS EMPRATURES EXMANST DAS ELDER RATES 159181.0 LBW/HR I 44.4 LBM/SEC)

HEAT EXCHA! GER GETHETPY

OVERALL DI PENSIONS: 1 FUST-11 12.0 FT. MIDTH: 12.0 FT. HEISAT: 1.3 FT.

COUTS OF STREAGE 1.3 IN.
INSTITUTE OF TUBE 1.4 THE STREAM OF THE STREAM HEAT

(HEATING LENGTH- 3.0 FT.) NLMBER OF PASSES: B (TOTAL)
NEATHNG SECTION: 2
BUILING SECTION: 4
SUPERHEATING SECTION: 2

FRONTAL AREA: 143.8 SQ. FT.

OUTSIDE AREA/PASS: 3264.9 SO.FT. INSIDE AREA/PASS: 187.5 SQ. FT.

NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS :

TLBE LENGTH 12. FT.

HEAT EXCHANGER PERFORMANCE

LUNGITUDINAL TUBE PACING: 1.95 IN-

TRANSVERSE TUTE SPACINGS 2.25 IN.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) 55609.7 HEATING 301LING UPERHEATING SECTIN

STEAM PRESSURE: 400.0 PSIA (SAIURA'ION EMPERATURE* 444.6 F)

GAS-SIDE PRESSURE DROP: U.6 IN H20 JEAM FLCW RATE: 9526.0 LBM/HR.

PINCE PCIN: 39.9 F

SYSTEP PERFCREANCE

CONDEN SER PRESSURE: 4.08 IN HG STEM TURBINE EFFCIENCY: 0.85. FW HEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: STEIN TURISME SHARE OF THE LOADS 41.5 PERCENT TEAP TURBINE HORSEPINER: 1177.4 TOTAL CYSTEM HINGED WER: 2838.5 GT HIPSEPHWERIREVISEDI: 1661.2

GF AT SYSTEM HP: 2436.0 PECIFIC FUEL CONSUMPTION (LBM-FJEL/HP-HR): GT O'LLY: 1.063 COSAS: 0.522 GT AT SYSTEM HP: 0.858 FUEL CONSUMP 10N 118"-FUEL /HR. 1: 166.2 ThEP ALL EFF IC IEV (Y: GT CALY: 0.13)

COGAS: 0.222

GT AT SYSTEM HP: 0.161

68/15/79 15.09.46

RUN #28

MASTE HEAT RECOVERY UNIT DESIGN RUN

CAS TUBBINE

PRAKE HORSEPOWER: 16421.0. AFPROXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS
EARAUST GAS TEMPERATURE: 449.0 F
EXPANST CAS FLOW AATE: 407589.0 LBM/HR (113.2 LBM/SEC)

HEAT EXCHANGER GEOMETRY

DVERALL DIMEYSIONS: FILE | 12.0 FT. | 13.0 F

FIN FELCHTS 1.0 IN.
FIN THICKNESS: 0.048 IN.
TAANSVERSE TURE SPACING: 4.5C IN.
LONGITUDI'AL TURE SP'CING: 3.90 IN.

NUMBER OF TUBES PER ROW: 40.

TUBE LENGTH 12. FT.

OLTSIDE AREA/PASS: 4081.2 SQ.FT.

INSIDE AREA/PASS: 234.4 SG. FT.

FRONTAL AREA: 179.5 SQ. FT.

NUMBER OF PASSES: 18 ITOTAL)

HEATING SECTION: 8 (HEATING LENGTH= 1.4 FT.)

SUPERFERING SECTION: 2 (BOILIPG LENGTH= 3.4 FT.)

NUMBER OF ROWS PER PASS:

HEAT EXCEMBER PERFURANCE

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER LANG.) STEAM PRESSURE: 800.0 PS IA ISATURATION TEMPERATURE. 518.3 F) 549.0 764.6 4.3 IN H20 STEAM FLUE RATE: 38770.5 LBP/HR. CAS-SIJE PRESSURE CROP: PINCH POINT: 32.5 f BELLING BELLING SUPERIEATING SEC TION

SYSTEM PERF JR44NCE

CONDENSER PRESSURE: 4.08 IN HG STEAM TURBINE EFFICIENCY: 0.85 HHATER PRESSURE: 15.0 PSTA LHV OF FUEL: 18400 BFUZLEM ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 8246.9 SPECIFIC FUEL CUNSUMPTION (LBM-FUEL/HP-HR): 0.385 GT AT SYSTEM HP: 0.356 STEAP TURBINE SHARE OF THE LUAC: 24.2 PENCENT FUEL CT CALLY 11 TOLO.3 COGAS: 1000.3 COGAS: 0.419 STEAM TURBINE HURSEPCHERS 5132.8 TOTAL SYSTEP HORSEPCHER: 21235.0 CT PERSEICAERIREVISEED: 16072.2 THER WAL EFFICIENCY:

66.24.21 21.45.59

RUN #29

MASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TUREINE

BHAKE HORSEPOWER: 0526.0. APPROXIPATE CORRESPONCING SHIP SPEED: 16.0 KTS EXPAUST GAS TEMPERITIVE: 742.0 F EXPAUST GAS FLUE RATE: 328641.0 LBW/HR (91.3 LBM/SEC)

HEAT EXCHANGE GECMETRY

OVERALL CIVE 1517 15: FT. HINTH: 12:0 FT. FELCHT: 4:6 FT.

HEAT TAINSFER SURFACE LAFEER: 2.5 INCITY LUCK CLAREFER: 1.9 ININSTEAL THE FAIL SERVICE
FIN SPACE CONTROL
FIN TYPE: ECCHEVED
FIN TYPE: ECCHEVED
FIN THE FILE FILE
FIN THE F

NUMBER OF PASSES: 14 (TOTAL)

BEATING SECTION: 7 (HEATING LENGTH* 1.6 FT.)

SUPERFEATING SECTION: 2 (BOILING LENGTH* 1.5 FT.)

OUTSIDE AREA/PASS: 4081.2 SO.FT.
INSIDE AREA/PASS: 234.4 SQ. FT.

NUMBER OF RCWS FER PASS:

TUBE LENGTH 12. FT.

FRONTAL AREA: 179.5 SO. FT.

HEAT EXCENDER PEFFORMANCE

LONGITUCITAL TUTE SPACING: 3.90 IN.

THANSVEHSE TIBE SPACING: 4.50 IN.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMPER LAVG.) 87717.6 \$46.9 546.3 706.9 BELLING BELLING SLOFTHEATING SECTION

STEAP PRESSURE: 800.0 PSIA (SATURATION TEMPERATURE= 518.3 F) Steam Flor Rate: 20212.2 18P/HR.

CAS-510E FRESSURE CROP: 2.4 IN H20

PINCH POINTS 31.2 F

STSTEM PERF TRYANCE

ASSUMED SYSTEM CHARACTERISTICS: STEAP FUFBINE SHARE OF THE LOADS 24.2 PERCENT STEAM TURBINE HOR SEPEMER: 2670.5 TUTAL SYSTEM HORSEPCHER: 11049.4 GT PERSEECHERIREVISEED: 8378.9

SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HR): SYSTEM HP: 0.481
FUEL CONSUMPTION (LBF-FUEL/HR-1: 4.34.2 GT AT SYSTEM HP: 5318.0

HERPEL EFFICIENCY: COGAS: 0.345 GT AT SYSTEM HP: 0.287

ř.

CA 115/75 15.54.15

MASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURBINE

BRANE HIRSEPINER: 1684.0, APPROXIMATE CORRESPONCING SHIP SPEEL: 9.0 KTS EXHAUST GAS TE40ERATURE: 689.0 F EXHAUST GAS FLCM BATE: 159731.0 LBW/HR 144.4 LBW/SECI

HEAT EXCHANGER GEUNETRY

CVERAL CINE 12.0 FT. HIJOHI 15.0 FT. HELCHEL 15.0 FT.

TRINSIER SUPERCE CUSSICE TUDE DIAMETER: 2,0 IN. INSIDE TUDE TUDE DIAMETER: 1,9 IN. TUDELFILI ACTA LEGANTE: FIN SPACING: 1,6 LANGE FINS SIN. FIN BELCHT: 1,0 IN.

LCAGIFUCINAL TURE SPICINGS 3.90 IN. TRANSVERSE TUBE SPACINGS 4.50 IN.

NUMBER OF TUBES PER ROWS NLYBER OF RCMS PER PASS:

TUBE LENGTH 12. FT.

DITSIDE AREA/PASS: 4081.2 SC.FT. INSICE AREA/PASS: 234.4 SC. FT. FPCNTAL AREA: 179.5 SO. FT.

INFATING LENGTH= 2.4 FT.) NUPRER OF PASSES: 10 (TOTAL)
HEATING SECTION: 3
BOJLING SECTION: 4
SUPERFEATING SECTION: 3

HEAT EXCEANGES PERFORMANCE

FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMPER (AVS.) 4033.4 CAS TEMP. IN GAS TEMP. OUT BCILING SUPERIEATING SECTION

31670.3

STEAP FRESSURE: 433.0 PS IA (SAFURATION TEMPERATURE 518.3 F)

STEAM FLOW RATE: 7149.0 LBM/HR.

GAS-SICE PRESSURE DRCP: 0.5 IN H20 PINCE POINTS 35.0 F

SYSTE" FE FF JRY MICE

CONCENSER PRESSURE: 4.08 IN HG STEATURE EFFICIENCY: 0.85 FW HATER PIRESSURE: 15.0 PSIA LIV OF FUEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: 949.3 LT HCH SEFONERIREVI:EDJ: 1061.6 STEAM TURBLUE HUNSEPONERS

SPECIFIC FUEL CUISUMPTION ILAM-FUEL /HP-HR):
GT CALY: 1.063 COGAS: 0.677 GT SYSTEM HP: STEAP TLABINE SHAPE OF THE LOAD: 36.4 PERCENT TOTAL SYSTEM HORSEPONERS 2610.3

GT AT SYSTEM HP: 2325.5 FULL C 175UMPTION (LAM-FUEL /HR.): 1766.3

GT AT SYSTEM HPE COG15: 0.204 THER PAL EFFICIENCY:

08/15/75 20.50.10

RUN #31

WASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TUREINE

WARANE HORSEPOWER: 16421-0, AFPROXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS EXFLUST GAS TEMPERATURE: 849.0 F EXHALST GAS FLOW RATE: 407549.0 LHH/HR (113.2 LBM/SEC)

HEAT EXCHANGES GECHET RY

WERALL DIMENSIONS:

IN TYPE: EGGETTED
1 SPACING.
1 FELGETT: 0.030 IN. PEAT TRANSFER SUFFICE DUTSIDE TUBE DIA INSIDE TUBE DIAP TUBEZITI AS. CISE

LONGITUDINAL TUBE SPACING: 2.92 IN. TRANTVESSE TUBE SPACING: 3.38 IN.

NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS :

OLTSIDE AREA/PASS: 4132.2 SQ.FT. INSIDE AREA/PASS: 237.3 SQ. FT. FR7WTAL AREA: 181.9 50. FT. TUBE LENGTH 12. FT.

NLYBER OF PASSES: 15 (TOTAL)
HEATING SECTION:
SOLLING SECTION:
SUPERFEATING SECTION: 7

HEATING LENGTH 5.1 FT.)

HEAT EXCHANGES PERFORMENCE

FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) 172417.9 GAS TEMP. IN GAS TEMP. OUT 730.9 S DEFENEATING SEC TION

STEAM PRESSURE: 830.0 PSIA (SATURATION TEMPERATURE 518.3 F)

STEAM FLIM ALTE: 39123. 8 LBM AIR.

SYSTEM PERF JAMAICE

STEAT TURBLINE HJF SEPCHER: 5154.9 GT HORSE PUNERIRE VISEDI: 16092.0

SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HR): 0.387

FULL C JYSUAPTIUM (LBM-FUEL/MR.): 67 DALY: 7003.0 CGGAS: 7003.0 GT AT SYSTEM HP: 8235.5

GT AT SYSTEM HP: 0.357 COGAS: 0.420 THERMAL EFFICIENCY:

221

GAS-SICE PRESSURE UKCP: 3.7 IN H20 PINCH PAINT: JE.4 F

STEAP TLABINE SHARE OF THE LOAD: 24.4 PERCENT TOTAL SYSTEM HUNSEPOWER: 21287.0

CONCENSER PRESSURE: 4.08 IN HG SPEAM TURBINE EFFICIENCY: 0.85 WHICH PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 RIU/LBM

ASSUMED SYSTEM CHARACTERISTICS:

MASTE HEAT RECOVERY UNIT DESIGN RUN

BRAKE HOBSEPONER: 8526.0. AFPROXIMATE CIRRESPONDING SHIP SPEED: 16.0 KTS EXFAUST 345 TEMPERATURE: 3742.0 F EXHALST GAS FLOW RATE: 328641.0 LBM/HR (91.3 LBM/SEC) GAS TURBINE

HEAT TRANSFER SURFACE
CUTSIDE TUAL DIGHTER: List IN.
INSTITUTE OF CLAMETER: List IN.
TUAL FLIN ACADEMINE: SE-MENTED
FIN SPACIAL: SE-MENTED
FIN HELUIT: 0.0 FINS/IN.
FIN HELUIT: 0.0 FINS/IN.
FIN THICKNESS: 0.036 IN. HEAT EXCHANGER GECHET RY

(BELLING LENGTH 3.4 FT.) OLISIDE AREA/PASS: 4132.2 SQ.FT. INSIDE AREA/PASS: 237.3 SO. FT. FRONTAL AREA: 181.5 SO. FT. NUMBER OF TUBES PER ROWS TURE LENGTH 12. FT.

NUMBER OF ROMS PER PASS:

NLWBEK OF PASSES: 11 (TOTAL)
HEATING SECTION: 5
SUPERHEATING SECTION: 5

HEAT ENCHANGER PEAFORMANCE

LONGITUDINAL TUSE SPACING: 2.92 IN.

TRANSVERSE TUBE SPICINGS 3.38 IV.

GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNDLDS NUPBER (AVG.) 87322.8 STEAM PRESSU'E: EUG.C PSIA (SATURATION TEMPERATURE. 518.3 F) 548.B 675.4 GAS TEMP. IN HEATING HOLL ING SUPERHEATING SECTION

STEAM FLUE RATE: 20352.2 LBM/HR.

GAS-SIDE PP ESSURE DROPE 1.9 IN H20 PINCH POINT: 30.5 F

SYSTEM PERFURMANCE

ASSUMED SYSTEM CHARACTERISTICS: 0.482 SPECIFIC FUEL CONSUMPTION (LBM-FUEL ZHP-HR) : STEAM TURBINE SHARE (F THE LOAD: 23.9 PERCENT STEAM JURHINE HURSEPOWER: 2041.5 1) IAL SYSTEM HORSEPOWER: 11029.2 GT MCAS EFOWERINEV IS ECH: 8387.7

CONDENSER PRESSURE: 4.08 IN. HC STEAP TURBINE EFFICIENCY: 0.65 HW HEATER PRESSURE: 15.0 P SIA LHV CF FUEL: 18400 BTU/LRM

GT AT SYSTEM HP: 5311.3 FUEL CONSUMPTION (LBM-FUEL /HR.): CL . 1415.1 THER PAL EFFICIENCY:

COGAS: 0.344

GT AT SYSTEM HP: 0.287

MASTE HEAT RECOVERY UNIT DES IGN RUN

9.0 KTS BRAKE FCRS EPOMER: 1684.0, APPATXIMATE CURRESPONDING SHIP SPEED: EXHALSI GAS TEMPERATURE: 159731.0 LBM/HR (44.4 LBW/SEC) GAS TURBINE

OUTS10E AREA/PASS: 4132.2 SQ.FT. INSIDE AREA/PASS: 237.3 SO. FT. FRUNTAL AREA: 181.9 SC. FT. NUMBER OF TLBES PER ROWS NUMBER OF ROWS PER PASS: TUBE LENGTH 12. FT. AT FAMILE SUBFACE

OUTSIDE THE DIAFFER: 1.5 IN.

INSIDE THE DIAFFER: 1.5 IN.

TUSE/EIN ARHANGEPENT:

FIN TYPE: SEGMENTED

FIN HEIGHT: 0.8 IN.

FIN HEIGHT: 0.8 IN. LONGITUDINAL TUBE : PACING: 2.92 IN. TRANSVERSE TUBE SPICINGS 3.38 IN. OVER ALL DIMENSIONS: FT. LEVITH: 15.0 FT. WIGHT: 15.2 FT. HEISHT: 2.0 FT. HEAT EXCEMICER GEINETRY HEAT

(POIL ING LENGTH- 4.4 FT.) NUPBER OF PASSES: 8 (TOTAL)
HEATING SECTION: 8
SUPERHEATING SECTION: 4

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HEAT EXCHANGER PERFORPANCE

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) STEAM PRESSURE: 800.0 PSIA (SAFURATION FEMPERATURE 518.3 F) GAS-SIDE PRESSURL JROP: 0.4 IN H20 STEAP FLC4 FATE: 7201-1 LB4/HR. PINCE PCINT: 47.7 F HEATING BOILTYG SUPERHEATING S ECT 1 IN

30667.8

SYSTEP FE FF CFPANCE

CONDENSER PRESSURE: 4.08 IN. HG SEAN TURANNE EFFICIENCY: 0.85 FM HEATER PRESSURE: 18.00 BTU/LBM THY OF FLEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM NP: 2329.1 0.155 GT AT SYSTEM HP: SPECIFIC FUEL CURSUMPTION (LBM-FJEL/HP-HP): COLASTEM HP: STEAM TURBINE SHARE OF THE LOADS 36.5 PERCENT FUB. C7/15/14PT 104 (LBM-FUEL /HR.): 66.3 COUAS: 0.205 956.2 TOTAL SYSTEM HORSEPHWER: 2618.1 GT HOP SEPOMERIRE VISE DIS 1661.9 STEAM FIRBINE HURS EPCHER: THER OF CALY: 3.135

MASTE MEAT RECOVERY UNIT DESIGN RUN

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BRIKE HIRSEPONER: 16421.0. APPLOXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS EXFAUST 64S TEMPERITURE: 849.0 F EXHALST 64S FLOW RATE: 437589.0 LBW/HR 1113.2 LBW/SEC)

HEAT EXCHANSER GECHETRY

OVER ALL CIVE'S IDES LENGTH: 12-0 WIDTH: 15-C F

FIL SR AGENEVI: FIN TYPE: CECHENED IN SPACING 0 1.88 FINS/IN. FIN HELLON: 0.5 IN. FIN THE UNESS: 0.024 IN. PEAT.

(HEATING LENGTH- 1.9 FT.) NUMMER OF PASSES: 12 (TOTAL)
HEATING SEFTION: 5
BOILING SECTION: 4
SUPERHEATING SECTION: 1

F FCNT AL AREA: 179.8 SQ. FT.

OUTSIDE AREA /PASS: 4081.2 SO.FT. INSIDE AREA/PASS: 234.4 SQ. FT.

NIMBER OF TUBES PER ROW! NLMBER OF ROWS PER PASS :

TUBE LENGTH 12. FT.

HEAT EXCHANGER PERFURPANCE

LONG ITUE LIAL THE SPICING: 1.95 IN.

TRANSVERSE TUBE SPACINGS 2.25 IN.

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMPER LANG. I 22250.0 SUPERHEAT ING SEC (11.3N

163175.6

STEAP PRESSURE: 800.0 PSIA (SATURATION TEMPERATURE 518.3 F)

GAS-SIDE PRESSURE DRCP: 3.3 IN H20 STEAM FLOW RATE: 39189.5 LBM/HR.

PINCE POINT: 30.7 F

SYSTEM PERFURPANCE

STEAM TURBINE HORSEPCHER: 5211.1 TOTAL SYSTEM HORSEPINER: 21318.2 GT HURSEPUNEAIREVISEDI: 16107.1

ASSUMED SYSTEM CHARACTERISTICS:

ONDENSER PRESSURE: 4.08
FIEAM THABINE EFFICIENCY:
H HEATER PRESSURE: 15.0

SPECIFIC FUEL CONSUMPTION ILBY-FUEL / HP-HR 1: SYSTEM HP: GT OLAS: 0.329 GT AF SYSTEM HP: STEAM TURNINE SHARE OF THE LOAD! 24.4 PERCENT

0.386

8230.2 0.356 GT AT SYSTEM HP: GT AT SYSTEM HPS # FUEL CLISSIMPTING (LBM-FUEL/HR.): 7005.1 COUAS: 0.421 THER CALY: O.ST.

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MASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURBINE

		5.5 FT. J
P SPEED: 16.0 KTS	NUMBER OF RCMS PER PASS: 1. NUMBER OF TUBES PER ROW: 80. TUBE LENGTH 12. FT. OUTSIDE AREA/PASS: 4081.2 SQ.FT. INSIDE AREA/PASS: 234.4 SO. FT.	FRUNTAL AREA: 179.8 SC. FT. NUMBER OF PASSES: 9 (TOTAL) HEATING SETTION: 4 (HEATING LENGTH= 1.6 FT.) SUPERHEATING SECTION: 2 (EDILING LENGTH= 5.5 FT.)
ORRESPONCING SHI		
BATAKE HORSFPONER: MS20.0, APPROXIMATE CORRESPONCING SHIP SPEED: 16.0 KTS EXHAUST GAS TEMPERATURE: 742.0 F EXHAUST GAS FLOW RATE: 328641.0 LBW/HR (91.3 LBW/SEC) HEAT EXCHAUSER GEOMETRY	OVERALL CLACASIONS: FT. L. C.	TRANSVLASE TUBE SPACING: 11.88 FINS/IN.

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMPER (AVG.)	11569.7					
FLUID TEMP. OUT A	513.3			•		
FLUID TEMP. IN	513.3	E. 518.3 F1				
GAS TEMP. DUT	5439.9 643.9	ATI CN TEMPERATUR		•		
GAS TEMP. IN	543.7	D.O PSIA ISATUR	1426.0 LB4/IR.	3 1.7 IN H2		
S ECT 1114	HEAT ING BOIL ING SUPERHEAT ING	STEAM PRESSURE: 800.0 PSIA ISATURATION TEMPERATURE. 518.3 F)	STEAP FLCW FATE: 20426.0 LB4/HR.	GAS-SIDE PRESSURE URUP: 1.7 IN H20	PINCE PCINT: 10.4 F	

	ASSIMED SYSTEM CHARACTERISTICS:	CONDENSER PRESSURE: 4.08 IN. HG	FW HEATER PRESSURE: 15.0 PSIA	LHV UF FLEL: 18400 BTU/LBM	401	FUEL CHRUMPTING ILAM-FUEL/HR.1: 6735.4 GT AT SYSTEM HP: 5334.1	286
					SPECIFIC FIEL CONSUMPTION IL BY-FUEL / HP-HRJ: SYSTEM HP: 0.481	2	THER ALL EFFICIENCY: COLAS: 0.346 GT AT SYSTEM HP: 0.286
					Ī	1	Ì
					YSTE	YSTE	YSTE
				ENT	5	2 1	- 5
				STEAM TURBINE SHARE OF THE LOAD: 24.4 PERCENT	£ 5	5	5
				24.4	-du / 1	5.4	46
	-:	9.90	9.0	0:	-FUE	1,5	6.3
	1656	27	11 09	LOA	AS :-	S.E.	15:
	GT HOMSEPOWERIRE VISEDI: 8391.1	STEAP TUREINE HORSEPCHERS 2706.8	TOTAL SYSTEM HIASEPOWER: 11098.0	THE	200 200	FUEL	000
	SE DI	EP CH	3MC	. OF	H T	E 4	
	IE VI	HORS	14SE	MARI	00 S	135	757
CE	ER	N.E.	7	AE.	1.	17.	3.
FPA	EP.3M	1961	STE	1881	E.	NE.Y	. NEF
PF C	0 P S	-	15 1	-	11:3	3.5	676
+ FE	GT H	STEA	TOTA	STEA	SPEC	FUEL	THER
SYSTEP FEFF CAPANCE							

HEAT EXCHANGER PEAF CHPANCE

The Market War

WASTE HEAT RECOVERY UNIT DESIGN RUN

BRAKE HIPSEPONER: 1684.0. APPROXIMATE CORRESPONCING SHIP SPEED: EXPANST 645 TEMPERATURE: 689.0 F EXMALST GAS FLOW RATE: 159731.0 LBM/HR (44.4 LBM/SEC) GAS TURBINE

NUMBER OF TUBES PER ROWS NUMBER OF RCMS FER PASS TUBE LENGTH 12. FT. CV 6R ALL CINE 12.0 FT. MINTH: 12.0 FT. MINTH: 12.0 FT. HEAT EXCHANGER GECHETRY

HEAT TAIN SEEN SUNFICE CHANGE EN 1.3 INCAST TOUR CHANGE EN 0.9 INTOBETT TOUR CHANGE TO 1.3
FOR THE TOUR CHANGE TO 1.3
FOR THE TOUR CHANGE TO 0.024 IN-

(BOILING LENGTH: 5.7 FT.) NUMMER OF PASSES: 6 (TOTAL)
HEATING SECTION: 2
SUPERHEATING SECTION: 2

OLTSIDE AREA/FASS: 4081.2 SO.FT. INSIDE AREA/PASS: 234.4 SQ. FT.

FPENTAL AREA: 179.8 SO. FT.

HEAT EXCHANGER PERFIAMA ICE

LONGITUDINAL TUBE SPICING: 1.95 IN.

4.25 IN.

TRANSVEASE THRE SPACING:

GAS TEMP. IN GAS TEMP. GUT FLUID TEMP. IN FLUID TEMP. DUT REYNJLDS NUMBER (AVJ.) 31476.1 BELLING BELLING SUPERHEATING SEC TION

STEAM FRESSURE: 8JO.O PSIA (SATURATION TEMPERATURE= 518.3 F) STEAM FLOW RATE: 7149.0 LHMMR.

GAS-SIJE PRESSURE CROP: 0.3 IN H20 PINCH POINT: 84.2 F

SYSTEM PERF JRMANCE

CONCENSER PRESSURE: 4.08 IN. MC STEAM TURBLINE EFFICIENCY: 0.85 FW HEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM A SSUMED SYSTEM CHARACTERISTICS: STEAP TUPBINE SHARE OF THE LOAD: 36.3 PERCENT STEAM TURNINE HORSEPOWER: 948.3 TOTAL SYSTEM HORSEPONER: 2610.5 GT hChiefGwenineviseth: 1662.2

GT AT SYSTEM HP: 2325.3 0.891 SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HRI: 61 AT SYSTEM HP: 61 Outy: 1.064 FUEL CONSUPFILION LLB"-FUEL /HR. 1: 706.4

GT AT SYSTEM HP: 0.155 THERMAL EFFICIENCY: COJAS: 0.204

80.04.61 87/21/80

MASTE HEAT RECOVERY UNIT DESIGN RUN RUN #37

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The Market Land

GAS TURBINE

PRAKE HOFSEPONER: 16421.0. AFPROXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS
FARILST 015 TEMPERATURE: 449.0 F
EXFALST GAS FLOW RITE: 407589.0 ENFAHR (113.2 LBW/SE)

HEAT EXCHANGES LECHETRY

DVERALL DIMENSIONS: FT. IENGTH: 12.0 FT. HELDIN: 15.0 FT. HELDIN: 5.5 FT.

MEAT THANSER SUPERCE 12.) INCULTINE TEACH DIAMETER: 1.9 INTHANSEPHINE:
THANSEPHINE:
THANSEPHINE:
FIN TYPE: SCHENED
FIN TYPE: SCHENED
FIN TYPE: SALIGES:
FIN THE WITHER FINSTIN-

LONGITUDINAL TUBE : PACING: 3.90 IN-TRANSVERSE TUBE SPACING: 4.50 IN.

00 NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS! TLBE LENGTH 12. FT.

OUTSIDE AREA/PASS: 4081.2 SO.FT. INSIDE AREA/PASS: 234.4 SO. FT. F PCNTAL AREA: 179.5 SC. FT.

I POIL ING LENGTH- 2.6 FT.) NUMBER OF PASSES: 17 (TOTAL)
HEATING SECTION: 7
HOLLING SECTION: 8
SUPERHEATING SECTION: 2

HEAT EXCHANGER PERFCREANCE

SECT IN

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEPF. DUT REYNOLDS NUMFER (AVG.)

178832.9

STEAM PRESSUAE: 630.0 PS IA (SATURATION TEMPERATURE- 486.3 F) HEATING ECILING SCPERMEATING

STEAM FLOW RATE: 39455.5 LBMAHR.

4.0 IN H20 GAS-SILE PRESSURE CREP. PINCH POLATE 38.7 F

SYSTEM PEPFORMANCE

GT HCFS LFOWERIREV IS EC 1: 16081.9

STEAM TURBINE HOR SEPOWER: 5099.4 TOTAL SYSTEM HORS EPONER: 21181.4

CONDENSER PRESSURE: 4.08 IN. HG STEAM TURBINE EFFICIENCY: 0.85 FM HEATER PRESSURE: 15.0 PSTA LHV CF FUEL: 18430 HTU/LBM

A SSLMED SYSTEM CHARACTERISTICS:

SPECIFIC FUEL CONSUMPTION ILBM-FUEL/HP-HR): 61 7:117: 0.435 COGAS: 0.331 GT AT SYSTEM HP: STEAP THE INE SHARE OF THE LOADS 24.1 PERCENT FLEL CONSLIPTION (LEP-FUEL/HR.) 1001.6

0.355 GT AF SYSTEP HP: CO3AS: 0.418 THERPAL LEFT CLENCY:

GT AT SYSTEP HP: 8249.9

0.385

MASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURBINE

NUMBER OF ROMS PER PASS: BRANE FORSEPHWER: 6526.0, APPROXIMATE CURRESPONDING SHIP SPEED: 16.0 KTS EXHALST GAS TEMPERATURE: 324641.0 LBP/HR (91.3 LBM/SEC) HEAT THANSFER SUFFACE
TO SUFFER 1.3 IN.
IN SUFFER 1.9 IN.
IN SUFFER 1.9 IN.
IN SUFFER 1.9 IN.
IN SUFFER 1.9 IN.
FIN PRESS 5.996 FINS IN.
FIN FILLERS: 0.068 IN. DVERALL DIMENSIONS: HEAT EXCLINGER GEOMET RY

(Briling Length: 3.3 FT.) OLTSIDE AREA/PASS: 4081.2 SQ.FT. INSIGE AREA/PASS: 234.4 SQ. FT. FROMTAL AREA: 179.5 SQ. FT. NUMBER OF TUBES PER ROW! TLBE LENGTH 12. FT.

NUMBER OF PASSES: 15 (TOTAL)
HEATING SECTION:
501.1 NG SECTION:
60.2 SCHERATING SECTION: 2

HEAT EXCLANGER PERFIRMANCE

LUNGITUDIYAL TUBL SPACING: 3.90 IN.

TRANSVERSE TUBE SPICINGS 4.50 IN.

FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMPER LANG. 11871.6 98751.3 STEAM PRESSURE: 600.0 PS IA (SATURATION TEMPERATURE + 486.3 F) GAS TEMP. DUT 2.4 IN H20 GAS TEMP. IN STEAM FLJB RATE: 22173.9 LBP/HR. CAS-SIJE PHESSURE CROP: PINCH POINT: 32.7 F BELLING SCHERNEATING SCHERNEATING SECTION

SYSTEM PERFURMANCE

CCNDENSER PPESSURE: 4.08 IN. HG STEAM TURBINE EFFICIENTY: 0.85 FW HEATER PRESSURE: 15.0 P.SIA LHV OF FUEL: 18400 BTULEM ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 5380.7 GT AT SYSTEM HP: 0.285 SPECIFIC FUEL CUNSUMPTION (LBM-FUEL/HP-HR):
67 CALY: 0.529 COGAS: 0.395 GT AT SYSTEM HP: 0.475 STEAP TLEBINE SHARE OF THE LOAD: 25.5 PERCENT FUSE COTSCHPTION SLBH-FUEL/HR. 1: 44 34.1 COGAS: 0.351 STEAM TURBINE HTH SEPONER: 2860.6 TOTAL SYSTEM HORSEPONER: 11239.3 GT HCASEFCHERIREVISECUS 8378.6 THER WELL EFFICIENCY:

IN STE HEAT RECOVERY UNIT DESIGN RUN

GAS TURBINE

;

BRAKE HOHSEPOMER: 1684-0. APPROXIMENTE CORRESPINDING SHIP SPEED: 9.0 KTS EXFALST GAS TEMPERATURE: 0689.0 F EXFAUST GAS FLOM RATE: 159731.0 LBM/HR (44.4 LBM/SEC)

HEAT EXCHANGER GECPETRY

OVER ALL DIMENSIONS:
LENGTH: 12.0 FT.
NIDTH: 15.C FT.
FELCHT: 3.6 FT.

HEAT TAGNSFER SUFFACE STANFER: 2.3 IN.
TOTAL TOTAL STANFER: 1.9 IN.
TOTAL TOTAL STANFOLD
TOTAL TOTAL
TOTAL TOTAL
TOTAL TOTAL
FIN SOFT TOTAL
FIN HELDE: 2.0 124
FIN HELDE: 2.0 124
FIN HELDE: 2.0 124
FIN HELDE: 3.0 124

THANSVERSE TUBE SPACING: 4.50 JH.

LONGITUE IN TUBE SPYCING: 3.90 IN.

OLTSIDE AREA/PASS: 4081.2 SQ.FT. INSIDE AREA/PASS: 234.4 SQ. FT. F FCNTAL AREA: 179.5 SO. FT. NUMBER OF TUBES PER ROWS TLSE LENGTH 12. FT.

NUMBER OF ROWS PER PASS:

(HEATING LENGTH= 3.4 FT.) NUMBER OF PASSES: 11 (TOTAL)
HEATING SECTION: 3
301LING SECTION: 5
SUPERFERING SECTION: 3

HEAT EXCHANGER PERFCREANCE

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS MUMPER (AVG.) HEATING BOILING SUPERFEATING S ECT I IN

STEAM PRESSURE: 630.0 PSIA (SATURATION CEMPERATURE 486.3 F)

STEAP FLEW FATE: 8234-7 LBM/HR.

GAS-SIDE PRESSURE URCP: 0.5 IN H20 PINCE PCINT: 37.3 F

SISTEP FEFFCREANCE

STEAM TLABINE HORSEPCHER: 1062.4 ICTAL SYSTEM HORS EPOWER: 2725.9 GT HORSEPOWEGIREVISEDI: 1661.5

CONCENSER PRESSURE: 4°CE IN HG STEAM TURBINE EFFICIENCY: 0.85 FA HEATER PRESSURE: 15.0 PSTA LHV OF FUEL: 18400 BTU/LBM

ASSUMED SYSTEM CHARACTERISTICS:

FUEL CONSUMPTION LIBY FUEL HAS 11 166.2 GT AT SYSTEM HP: 2381.3 SPECIFIC FUEL CUNSIMPTION (LBM-FIEL/HP-HR): 67 AT SYSTEM HP: 0.874

STEAM TURBINE SHARE OF THE LOADS 39.0 PERCENT

GT AT SYSTEM HP: 0.158 COGAS: 0.213 THERPAL EFFICIENCY:

MASTE HEAT RECOVERY UNIT DESIGN RUN

ERAKE HURS EPOWER: 16421-0. APPROXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS
EXAKLSI GAS TEMPERATURE: 849.0 F
EXFAUST (AS FLOW RATE: 407589.0 LBM/HR (113.2 LBM/SEC)

DLISIDE AREA/PASS: 4132.2 SQ.FT. INSICE AREA/PASS: 237.3 SQ. FT. NUMBER OF PASSES: 14 (TOTAL)
HEATING SECTION:
50 NOTE ING SECTION:
7 SUPERFEATING SECTION: 7 FRONTAL AREA: 181.9 SO. FT. NUAPER OF TUBES PER ROW! NUMBER OF ROMS PER PASS: TLBE LENGTH 12. FT. HEAT TRANSFER SURFACE
OUT SIDE TOBE DIABLEER: 1.5 IN.
ILISIDE TUBE CAPEER: 1.5 IN.
ILISIDE TUBE FRANCEERIENTE
FIN TYPE: SECHENTE
FIN TYPE: SECHENT IDAGITUDINAL TUBE SPECING: 2.92 IN. 3.38 IN. TRANSVERSE TUBE SFACING: OVERALL DIPENSIONS: FT. NIDIA: 15.2 FT. HELGHT: 3.4 FT. HEAT EXCHANGER GETMETTY

GAS TEMP. IN GAS TEMP. QUT FLUID TEMF. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) 179758.6 MEAT EXCHANGER PERFORMANCE HEATING BOIL 11G SUPERFEAT ING SECTION

(HEATING LENGTH= 5.7 FT.)

STEAM PRESSURE: COU.O PSIA (SATURATION TEMPERATURE* 486.3 F.)

STEAP FLUW FATE: 39693.2 LBW/MR. GAS-SIDE PRESSURE DRCP: 3.5 IN H20

PINCH PEINT: 45.8 F

CONDENSER PRESSURE: 4.08 IN. HG STEAM TURBINE EFFICIENCY: 0.85. FW HEATER PRESSURE: 5.0 PSIA LHV OF FUEL: 18400 BTULLS ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 0.357 SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HR): CT AT SYSTEM HP! 0.387 GT AT SYSTEM HP : STEAM TURBINE SMARE OF THE LOAD: 24.3 PERCENT FUEL CONSUMPTION (LBM-FUEL/HR.): CO 6 451 0.420 STEAM FURBINE HORSEPCHERE 5167.7 TOTAL SYSTEM MASEPOWER: 21265.2 GT HJRSEP INEKIREVISEDI: 161 01.5 THER WAL EFF IC IE TOY: SYSTEP FEFF CAPANCE

MASTE HEAT RECOVERY UNIT DESIGN RUN

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BRAKE HORSEPOWER: 4526.0. APPROXIMATE CURRESPONDING SHIP SPEED: 16.0 KTS EXFAUST (45 TEMPERATURE: 742.0 F EXHAIST GAS FLOW RATE: 328641.0 LBM/HR (91.3 LBM/SEC)

HEAT EXCHANGER SECRETRY

FIN TYPE: SECHENTED FINS/IN. P. SPACING. P. 92 FINS/IN. FIN THICKNESS: 3.036 IN. OVERALL CIMEIS DAS: LENGTH: 12.0 FT. NOTH: 15.2 FT. FEICH: 2.9 FT. HEAT TRANSFER SUPERIOR TUBE CLANING DIABLE TUBE CLANING DIABLE TUBE FIN TYPE STEEL SEE

(BOILING LENGTH 2.3 FT.) OLTSIDE AREA/PASS: 4132.2 SO.FT. INSIDE AREA/PASS: 237.3 SQ. FT. NUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION: 4
BUILING SECTION: 2
SUPEFFEATING SECTION: 2 F HCNT AL ARE # 181.9 SQ. FT. NUMBER OF TUBES PER ROWS NUMBER OF REWS FER FASS: TUBE LENGTh 12. FT.

HEAT EXCHANGER PERFURHALCE

LONGITUDINAL TUSE SPACINGS 2.92 IN.

TRANSVERSE TUBE SPACING: 3.38 IN.

GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) 97271.8 STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE 486.3 F) EAS-SIDE FRESSURE CROP: 2.0 IN HZO GAS TEMP. IN STEAM FLUB RATE: 21894.0 LBP/HR. PINCH POINTS 31.6 F BELLING SLPFRHEATING SECTION

SYSTEM PERFURMANCE

ET PERSESCHENINEVISECUS 8385.5

CONCENSER PRESSURE: 4.08 IN. HG STEAM TURBINE EFFICIENCY: 0.85 FW HERR PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM A SSUMED SYSTEM CHARACTERISTICS: FLEL CONSLIPTION (LBP-FUEL/HR.): 61 AT SYSTEM HP: 5373.6 SPECIFIC FUEL CUNSUMPTION (LBM-FUEL/HP-HR): 0.475 STEAP TUPBINE SHARE OF THE LOAD: 25.2 PERCENT STEAM TURBINE HUR SEPCHER: 2832.3 TOTAL SYSTEM HOASEPCHERE 11217.8

GT AT SYSTEM HP: 0.289 COUAS: 0.350 THERPAL EFF ICIENCY:

MASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURBINE

NUMBER OF ROMS PER PASS : PRAKE HCSSEPOWER: 1684.0. APPROXIMATE CORRESPONDING SHIP SPEED: Explaist das temperature: 1689.0 f Explaist gas flow rate: 159731.0 [BM/HR (44.4 LBF/SEC) OVERALL DIMENSIONS: FT. HENCH: 12.0 FT. HEIGHT: 12.2 FT. HEIGHT: 2.2 FT. HEAT EXCESS GENETRY

OUTSIDE AREA/PASS: 4132.2 SO.FT. INSIDE AREA/PASS: 237.3 SO. FT. FRONTAL AREA: 181.9 SC. FT. NLMBER OF TLBES PER ROW! TLBE LENGTH 12. FT.

(HEATING LENGTH- 5.2 FT.) NLMBER OF PASSES: 9 (TOTAL)
HEATING SECTION: 2
BOLL ING SECTION: 5
SUPERHEATING SECTION: 2

HEAT EXCHANGER PERFORPANCE

LONGITLE INAL TUBE SPACING: 2.92 IN.

TRANSVERSE TUBE SPACINGS 3.38 IN.

REYNOLDS NUMBER LAVG. 1 4212.0 GAS TEMP. IN GAS TEMP. DUT FLUID TEMP, IN FLUID TEMP. DUT STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE= 486.3 F) HEATING HOILING SUPERHEATING SECTION

STEAP FLEW PATE: 8285.8 LBM/HR.

GAS-SIDE PRESSURE UROP: 0.4 IN H20 FINCE FCINT: 50.6 F

SYSTEP FEFFCHPANCE

CONDENSER PRESSURE: 4.08 II STEAM TUABINE EFFICIENTY: 0. STATER PRESSURE: 15.0 LHV OF FUEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: SPECIFIC FUEL CONSUMPTION (LBM-FJEL/HP-HR): 0.873 STEAM ILRBINE SHARE OF THE LOAD! 39.2 PERCENT FUEL CONSUMPTION (LBM-FIEL/HR.): 1766.3 STEAP FUFBINE HURSEPCWER: 1071.9 TUTAL SYSTEM HJRSEPUNER: 2733.6 GT HUF SEPONERIREVISEOI : 1661.7

GT AT SYSTEM HP: 0.158 GT AT SYSTEM HP! CO3AS: 0.214 THERMAL EFF IC LEMEY:

MASTE HEAT RECOVERY UNIT DESIGN RUN

CAS	GAS TURBINE			
	STATE WOODER O ICEAST SECOND STATES	1113 2410 4003 5000		6
	SYLAINT CAC TEMP COATINGS OAAD OF CO	URKE SPUNDING SHI	ש אננני	₹
	ENALS SAS FLOW PATE: 407589.0 LBM/HR 1113.2 LBM/SEC	(113.2 LBM/SEC)		

SPONDING SHIP SPEECE 20.0 KTS .2 LBM/SEC!	NUMBER OF RCMS PER PASS: 1. NUMBER OF TUBES PER ROW: 80. TUBE LENGTH 12. FT. OLTSIDE AREA/PASS: 234.4 SC. FT. FROTAL AREA: 179.8 SQ. FT. NUMBER OF PASSES: 11 (TOTAL) HEATING SECTION: 6 (HEATING LENGTH= 3.6 FT.) SUPERFERING SECTION: 1 (BOILING LENGTH= 6.6 FT.)
BARAKE HUNASPOWER 1 6421.0. APPROXIMATE CORRESPONDING SHIP SPEEC: 20.0 KTS EXHAUST GAS TEMPEGALURE: 407589.0 LBM/HR (113.2 LBM/SEC)	CVERAL CITENSITYS: CVERAL CITENSITYS: LAGTH: 15.0 FT. LEAT TAYSER SUCKECE TOUSING FILL CITERER: TOUSING FILL CITERER TOUSING FILL CITERER TRANSVERSE TUBE SPACING: 2.25 IN. LONGITUDITAL TUBE SPACING: 1.95 IN.

	FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.)	21083.2				
	FLUID TEMP. UUT	412.5				
	FLUID TEMP. IN	4470.90 486.39	E= 486.3 F1			
	GAS TEMP. IN GAS TEMP. DUT	314.5 742.6	STEAM PRESSURE: 600.0 PS IA (SATURATION TEMPERATURE.	R.	N H20	
ICE ICE	GAS TEMP.	192.6	30.0 PS 14 (S	35E18.5 LBM/H	CRCP: 3.0 1	
MEST EXCEANGER PERFIRMANCE	SECTION	PEATING BELLING SLPFRHEATIN	STEAP PRESSURE: 6	STEAM FLJM RATE: 35618.5 LBM/HR.	GAS-SICE PRESSURE DRCP: 3.0 IN H20	PINCH PJINT: 42.0 F
HEAT						

CONDENSER PRESSURE: 4.08 IN HG STEAP TURBLAE EFFICIENCY: 0.85 HH HEATER PAESSURE: 15.0 PSIA LHV CF FUEL: 18400 BTU/LBM A SSLMED SYSTEM CHARACTERISTICS: FLEL CONSUMPTION (1887-FUEL/HR.): 6T AT SYSTEM MP: 8237.5 SPECIFIS FLEL CONSUMPTION (LBM-FUEL/MP-HR): 0.387 GT AT SYSTEP HP: 0.357 STEAP TURBINE SHARE OF THE LOAD! 24.2 PERCENT THERPAL EFFICIENCY: COSAS: 0.420 STEAM TURATINE HOR SEPONER: 5154.2 TOTAL SYSTEM HORSEPOWER: 21271.7 GT HEFS EFOWERIREV IS EC 1: 16117.5 SYSTEM PERFURMANCE

1. 4.

WASTE HEAT PECOVERY UNIT CESIGN RUN

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EAAKE FORSEPOMER: 8526.0. APPRIZIMATE CORRESPONDING SHIP SPEED: 16.0 KTS EXHALS] 345 TEMPERATERE: 742.0 FEMANT 1 91.3 LBM/SEC)

HEAT EXCENSER GETMETRY

OVERALL DIMENSIONS: FT. | 12.0 FT. | 13.0 FT

NUMBER OF ROMS PER PASS:

TRANSFER SUFFACE
OLISIO TONE CLAFFER: 1.3 IN.
TOSE FOR ANALYMENTED
FIN SPECIFICATION FINAL
FIN HEIGHT 0.5 IN.
FIN HEIGHT 0.5 IN. HE A T

LONGITUDINAL TUBE SPACING: 1.95 IN. TRANSVERSE ILBE SPACING: 2.25 IN.

(PEATING LENGTH= 9.2 FT.) OUTSIDE AREA/PASS: 4081.2 SQ.FT. INSIDE AREA/PASS: 234.4 SQ. FT. NUMBER CF PASSES: 9 (TOTAL)
HEATING SECTION: 4
BJ1L 1NG SECTION: 4
SUPERHEATING SECTION: 2 FRONTAL AREA: 179.8 SO. FT. NUMBER OF TUBES PER ROWS TLEE LENGTH 12. FT.

HEAT EXCHANGER PERFCREANCE

SAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMF. DUT REYNOLDS NUMBER (AVG.) 100947.2 HEATING BOILING SUPERFEAT ING S ECT LIN

STEAP FLC# FATE: 21789.0 184/19.

STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE- 486.3 F)

GAS-SIDE PRESSURE DRCP: 1.6 IN HZD

PINCE PCINT 11.5 F

SYSTEP HE FF CAPANCE

ASSUMED SYSTEM CHARACTERISTICS : STEAP TLABINE HORSEPCHERS 2813.6 TOTAL SYSTEM NINSEPOWER: 11205.3 GT HORSEPJAERIREVISEDI 8391.7

CONDENSER PRESSURE: 4.08 1W. HG STEAM TURBINE FFECTENNY: 0.85 FW HEATER PRESSURE: 15.0 PSTA LHV OF FUEL: 18400 BTULLBW

SPECIFIC FUEL CONSIDETICE ILBM-FUEL FP-HR II SYSTEM HP : STEAM TURBINE SHARE OF THE LOAD! 25.1 PERCENT FUEL CCESUPETION ILEM-FUEL CHR 1: 4435.5

0.289 GT AT SYSTEM HP1 COLAS: 0.349 THERPAL EFFICIETY:

GT AF SYSTEM HP:

WASTE HEAT RECOVERY UNIT DESIGN RUN

BRIKE HOASEPOWER: 1684.0. APPROXIMATE CORRESPONCING SHIP SPEEC: EXFAUST 665 TEMPERATURE: 0689.0 F ENALSI GAS FLOW RATE: 159731.0 LBW/HH 144.4 LBW/SEC) GAS TURBINE

OLISIDE AREA/PASS: 4081.2 SQ.FT. INSIDE AREA/PASS: 234.4 SQ. FT. FFCNTAL AREA: 179.8 SQ. FT. NUMBER OF TUBES PER ROW: NLMBER OF RCMS FER PASS: TUBE LENGTH 12. FT. 9.0 KTS HEAT TAINSFEE SOFFICE IN IN-COPSIDE THEEFER IN IN-INSIDE THEEFER 0.9 IN-TUBEZEIN ARAAIGEMENTER FIN TYPE: SECRET E FINS/IN-FIN SPACE 11.88 FINS/IN-FIN HELDE: 0.024 IN-FIN THICKNESS: 0.024 IN-TRANSVERSE THRE SPACING: 2.25 IN. OVERALL CINEVSTINS: HEAT EXCHANGER GECHETRY

(HEATING LENGTH 4.4 FT.) NUMBER OF PASSES: 7 (TOTAL)
HEATING SECTION: 2
801LING SECTION: 2
SUPERFEATING SECTION: 2

HEAT EXCHANGER PERFORMANCE

LONG ITUE TIAL TUSE SPACING: 1.95 IN.

FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) 37418.6 STEAP PRESSURE: 600.0 PSIA ISATURATION TEMPERATURE 486.3 FI GAS TEMP. IN GAS TEMP. DUT \$52.4 \$14.9 \$01.8 GA !- SIJE PRESSURE CRCP: 0.3 IN M20 STEAM FLOW RATE: 8183.6 LBM MIL. PINCE POINTE 29.8 F BELLING SUPERHEATING SECTION

SYSTEM PERF JAMA'ICE

CONDENSER PRESSURE: 4.00 1% HG STEM TURBINE EFFICIENCY: 0.655 FW HAM TR PRESSURE: 15.0 PSIA HW CF FUEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: 0.158 GT AT SYSTEM HP: GT AT SYSTEM HP: SPECIFIC FUEL CHASMPTION (LAM-FUEL MP-HR); SYSTEM HP; STEAP THREINE SHARE OF THE LCAD: 38.8 PERCENT FUEL CT ZALYT 1164.3 COCAST 1766.3 COGAS: 0.213 STEAM TURBINE HJP SEPOWER: 1054. 8 TOTAL SYSTEM HORSEPOVER: 2716.8 GT HORSEPONERIREVISEDI: 1662.0 THER MAL EFFICIENCY:

es/11/19 10.20.19

MASTE HEAT RECOVERY UNIT DESIGN RUN

CAS THRRIVE

BHANE HURSLPINER: 16421-0, AFPROXIMATE CIRRESPONDING SHIP SPEED: 20.0 KTS FXFILST GIS FEMPERATURE: 849.0 F EXEMIST GIS FLIM MATE: 407589.0 LBM/HR (113.2 LBM/SC)

HEAT EXCHENSES SECYETRY

9V69 11 0146 45131451 FT. | 15.0 FT. | 15.0

HEAT 1910/FER SUBFIGURE 2.) INOUTSIDE THATER: 1.9 INTHAT IN A PROPERTY 1.9 INTHAT IN A PROPERTY 1.9 INFINE PARTY 2.9 FINS INFINE PARTY 2.9 FINS INFINE PARTY 2.9 FINS IN-

NUPBER OF PASSES: 14 (TOTAL)
HEATING SECTION: 7
SUPEKHEATING SECTION: 2

FRENTAL AREA: 179.5 SQ. FT.

OUTSIDE AREA/PASS: 4081.2 SO.FT. INSIDE AREA /PASS: 234.4 SO. FT.

NUMBER OF TUBES PER ROWS NUMBER OF RCMS PER PASS:

TUBE LENGTH 12. FT.

HEATING LENGTH 2:8 FT:

MEAT EXCHANGE PERF 14421CE

LCNGITUGAAL TUBE SPACING: 3.93 IN.

TRANSVERSE TURE SPACINGS 4.50 IN.

GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVS.) 19452.2 SAS TEMP. IN STORY OF STEAM SECTION

STEAM PRESSURE: 400.0 PSIA (SATURATION TEMPERATURE: 444.6 F)

3.5 IN H 20 STEAP FLEE RATE: 3930d.9 LBM/HR. CAS-SICE PPESSARE OF DP:

PINCH PUINT: 04.4 F

SYSTEM PEPF CREAMCE

ASSUMED SYSTEM CHARACTERISTICS: STEAM TURBLUE SHARE OF THE LOAD: 23.1 PERCENT SIEAM TLABINE MUNSEPCHER: 4849.2 TCTAL SYSTEM HINS EPOWER: 20955.9 GT HEPSERIAERIK EV 15ED1: 161 06.7

CONCENSER PRESSURE: 4°C8 IN HG STEAN TURBINE EFFICIENCY: 0.85 FW HEATER STORE: 15.0 PSIA IN OF FUEL: 18400 RTU/LRM

SPECIFIC FLEE CONSIMPTION (LBM-FIEL/MP-HAI): 67 AT SYSTEM HP: 0.395

GT AT SYSTEM HP: FIREL CCN SCHPTION JL B"-FUEL/H9. 3: 1005.0 THEN PAL EFF I CLENCY:

COGAS: 0.414

GT AT SYSTEM HP: 0.350

MASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURBINE

RRAKE HITTEPINET: 8526.U, APPLIXIMATE CORNESPONDING SHIP SPEED: 16.0 KTS EXMAIST GAS TEMPLRATURE: 742.0 F EXMALST GAS FLIM RATE: 328641.0 LUP/HR (91.3 LBM/SEC)

FEAT EXCHAPTER GENETRY

DVENALL DIPENSIONS: 12.0 FT. VIOTE: 15.0 FT. HEIGHT: 4.5 FT.

TRANSFER STREAM IN THE STREAM HE AT

LUNGITLJINKL TUSE SPACINGE 3.90 IN. THANSVEYSE TUBE SPACINGS 4.50 IN.

NUMBER OF TUBES PER PORT NUMBER OF ROMS PER PASS:

TUBE LENGTH 12. FT.

OUTSIDE AREA/PASS: 4081.2 SO.FT. INSIGE AREA/PASS: 234.4 SO. FT. FRINTAL AREA: 179.5 SQ. FT.

(BOILING LENGTHE 1.6 FT.) NLWBER OF PASSES: 15 (TOTAL)
HEATING SECTION:
BOLLING SECTICN:
SUPERHEATING SECTICN: 3

HEAT EXCHANGER PERFCREANCE

AND THAP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMF. OUT REYNOLDS NUMBER (AVG.) 11 965.1 471.4 HEATING 971LTIS SUPERREAL ING S ECT LIM

116558.0

STEAM PRESSURE: 400.0 PSIA ISATURATION TEMPERATURE. 444.6 F.)

GAS-51.0E P7.E SSURF URCP: 2.4 IN H20 STEAP FLEW PATE: 21945.2 LBW/HR.

FINCE PCINT: 30.3 F

SYSTEM FEFF 1844:CE

STEAM TURNING HIP SEPONER: 2957.1 TOTAL SYSTEM ADR SEPONER: 11336. GT HONSEPONERIREVISEDI: 8379.3

JONCENSER PRESSURE: 4,08 IN HG FEAN TURB NE EFFICIENCY: 0.85 NA FEAFESSURE: 15,0 PSIA THV OF FUEL: 18400 BTU/LBM

ASSUMED SYSTEM CHARACTERISTICS:

SPECIFIC FUEL CONSUMPTION ILBM-FUEL/HP-HR1: 67 AT SYSTEM HP: 67 A4 Y: 0.527 C.3645: 0.391 67 AT SYSTEM HP: STEAM THESTHE SHARE OF THE LOADS 26.1 PERCENT

GT AT SYSTEM HP1 5412.6 0.477 FULL CUNSCAPTION CLUP-FULL/118-1: 4434-2

GT AT SYSTEM HP: 0.290

COUAS: 0.354

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WASTE HEAT RECOVERY UNIT DESIGN RUN

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PRAKE PORSEPIMER: 1044.0, APPROXIMATE CORRESPONDING SHIP SPEED: 9.0 KTS EXHALST JAS TEMPERATURE: 689.0 F EXHAUST GAS FLOW RATE: 159731.0 LBMMR (44.4 LBM/SEC)

HEAT EXCESSIBER CE STETRY

OVER ALL ULMENSIONS: FILE STATES IN 12.0 FT. NIUTH: 15.0 FT. HEAT THANKER SIFFACE FIRE JAMETER: 2.1.

FILE (PS) 1 SESHINES FINSTING 1 PER STANSING 1 PER

NUMBER OF ROMS PER PASS: 1.

NLMBER OF TLBES PER ROM: 40.

TLEE LENGTH 12. FT.

OUTSIDE AREA/PASS: 4081.2 SO.FT.

INSIDE AREA/PASS: 234.4 SO. FT.

FHONTAL APER: 179.5 SO.FT.

NUMBER OF PASSES: 12 (1074.1)

NUMBER OF PERITING SECTION: 3 (BAILING LENGTH: 6.5 FT.)

SUBERMETTING SECTION: 3 (BAILING LENGTH: 6.5 FT.)

HEAT EXCHANGER PERFIRMANCE

LUNGITUDITAL TURE SPACING: 3.90 IN.

TAMSVERSE FIRE SOLCINGS 4.50 IN.

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (ANG.) 463C. 8 44609.7 \$ 5.17.5 6.889.5 HEATING HALING SEPERHEATING SECT 1 JA

STEAM PRESSURE: 400.0 PSIA (SATURATION TEMPERATURE: 444.6 F)

STEAM FLCK RATE: 9524.5 LBM/HR. GAS-SIJE PYESSUAE URTP: G.5 IN H20

PINCH FEINT: 42.5 F

SYSTEM PENECRASHICE

CONDENSEP PRESSURE: 4.08 IN HG STEAM TURNING EFFICIENCY: 0.85 FW HEATEN PRESSURE: 15.0 PSIA LHV CF FUEL: 18400 RTUYL BM A SSUMED SYSTEM CHARACTERISTICS: STEAM TURBLIE HIP SEPONER: 1184.4 TUTAL SYSTEM HIRSEPOWERS 2845.7 GT HURSEPONERIREVISEDI: 1661.4

SPECIFIC FUEL CHARE OF THE LOAD: 41.6 PERCENT SPECIFIC FUEL CHASHIPTION (LBM-FJEL/HP-HR): 37 JULY: 1.063 CO.AS: 0.621 GT AT SYSTEM HP: 0.857 FUEL CONSUMPTION (LBV-FILEL/H9.1: of Jil Y: 1766.2 COGAS: 1766.2 GT AT SYSTEM HP: 2439.3

THER DALY: 3.13) COSA": 0.223 GT AF SYSTEM PP: 0.161

08/16/79 15.46.35

RUN #49 HASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURPINE

PMANE FEFFEMERATURE: 16421.0. APPRIXIMATE CORRESPONDING SHIP SPEED: 26.0 K1S Emals 345 Temperature: 949.0 F Extiust Gas Flow Rite: 407589.0 LB MAR (113.2 LB M/SEC)

MEAT EXCEMEER CENTETRY

GVCRALL DIMENSIONS: FT. WIGHT: 15.2 FT. HE IGHT: 2.7 FT.

HEAT TRANSFER SURFACE
LUUSSINE TUTE UTANETER: 1.5 IN.
INSIDE TUBE LIANETER: 1.4 IN.
TLOKET ARRANGERINE
FOR SPECIAL SECHNIED
FOR SPECIAL OF 192
FOR HELOMIS OF 192
FOR HELOMIS OF 193
FOR HELOMIS OF 193
FOR THICKIESS: 0.036 IN.

TRINSVERSE TUBE SPACING: 3,36 IN.

NUMBER OF ROMS PER PASS: 1.
NUMBER OF TUBES PER ROW: 54.

TLBE LENGTH 12. FT.

OUTSIDE AREA/PASS: 4132.2 SQ.FT.

INSIDE AREA/PASS: 237.3 SQ. FT.

FPONTAL AREA: 181.9 SQ. FT.

NLMBER OF PASSES: 11 (TOTAL)
HEATING SECTION: 5
SUPERHEATING SECTION: 5

(HEATING LENGTH 1.0 FT.)

HEAT EACH ANGER PERFURMANCE

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMPER LAVG. I 19154.8 3 ECT 10N

184657.6

PRESSURE: 400.0 PSIA (SATURATION TEMPERATURE: 444.6 F)

STEAM FLOW RATE: 38942.0 LBM/HR.

GAS-SIDE PRESSURE DROP: 2.7 IN H20 PINCE PCIAT: 64.8 F

SISTEM PEPF DRMANCE

ASSUMED SYSTEM CHARACTERISTICS: STEAP TLABINE HURSEPCHER: 4821.6 GT HAFSEPOAERIREVISEDI: 15127.1

CONDENSER PRESSURE: 4.08 IN HG STEAN TURBINE EFFICIENCY: 0.85-HW HGATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM

> TOTAL SYSTEM HORSEPOWER: 20948.7 STEAM TURBLIE SHARE OF THE LOAD: 23.0 PERCENT

SPECIFIC FUEL CONSIDERTION (LBM-FIEL/hP-HR):
CLOSAS: 0.435 GT AT SYSTEM HP: 0.395
FUEL CCASIMFILDY (LBM-HIEL/HR-1:
CLOSIMFILDY (LBM-HIEL/HR-1:

THEMPAL EFFICIENCY:
GT GALY: 0.313 COGAS: 0.413 GT AT SYSTEM HP: 0.

MASTE HEAT RECOVERY UNIT DESIGN RLN

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HRAKE HORSEPIWER: ESSO.O, APPROXIMATE CORRESPONDING SHIP SPEED: 16.0 KTS EXHAUST GAS TEMPERATURE: 742.0 F EXHAUST GAS FLOW ATTE: 328641.0 LBP/HR (91.3 LBP/SEC)

NUMBER OF ROWS PER PASS : LUTSING THE DIAMEER: 1.5 IN.
LUTSING THE DIAMEER: 1.4 IN.
LUTSING THE SCAMPING IN.
LUTSING SCAMPING FIRST IN.
FIN SPACING OB FIRST IN.
FIN HELDER: 0.036 IN. TRANSVERSE TUBE SPACING: 3.38 IN. CVERALL QIMENSISMS: FT. ENGINE 12.6 FT. MIDTH: 15.2 FT. HELVHI: 25.9 FT. HEAT EXCEANGER GEOMETRY HEAT

I POIL ING LENGTH: 1:3 FT: OUTSIDE AREA/PASS: 4132.2 SO.FT. INSIDE AREA/PASS: 237.3 SQ. FT. NUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION:
BOLLING SECTION:
SUPERINGTING SECTION:
2 FRONTAL AREA: 181.9 SO. FT. NLMBER OF TUBES PER ROWS TUBE LENGTH 12. FT.

HEAT EXCHANGES PENFONMANCE

LONGITUDINAL TUSE SPACING: 2.92 IN.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMPER (AVG.) 11817.9 10974.9 STEAM PRESCURE: 400.0 PSIA (SATURATION TEMPERATURE- 444.6 F) GAS-510E PAESSUAL DRCP: 1.9 IN H20 STEAP FLEA RATE: 23945.2 LB4/IR. PINCH PCINT: 36.4 F HEATING BTIL 146 SUPERFEATING SECT IN

SYSTEM PE HE CHMANCE

CONDENSER PRESSURE: 4.00 IN. HC STEAM TURBINE EFFICIENCY: 0.05 FW HEATER PRESSLET: 15.0 PSIA LHV OF FUEL: 18400 BTU/LRM ASSUMED SYSTEM CHARACTERISTICS: 5417.5 0.477 SPECIFIC FULL CONSUMPTION ILBM-FJEL/ PP-HRJ: COSSEM HPS GT AT SYSTEM HPS STEAM TURBLUE SHARE OF THE LOADS 26.1 PERCENT FUEL CCASLMFTIGN ILEY-FUELTH . 1: 14.34.9 CDUAS: 0.354 STEAP TURBLAE HORSEPCHER: 2964.8 TOTAL SYSTEM MONSEPOWER: 11351.5 ET HEFSEPTAETREVISEDIE 8386.5 THERPAL EFF IC SENCY:

0.530

GT AT SYSTEM HP:

MASTE HEAT RECOVERY UNIT DESIGN RLN

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BHAKE HT9SEPTAER: 1644.0, APPROXIMATE CORRESPONDING SHIP SPEED: 9.0 KTS EXHANST GAS TEMPERATURE: 0689.0 F EXHALST GAS FLUM RATE: 159731.0 LBM/HR 144.4 LBM/SEC)

HEAT EXCHANGER GEINETRY

CVERALL DIMENSIONS: LF15TH: 12.6 FT-WIDTH: 22.6 FT-Helbil: 2.4 FT-

THEASTER STREACE
OUTSIDE TONE CLAREFER: 1.4 IN.
115 DE TONE CLAREFER: 1.4 IN.
115 DE TONE CLAREFER: 1.5 IN. HEAT

ICNGITLDINAL TOUR SPACING: 2.92 IN. TRANSVERSE TUSE SPACING: 3.38 IN.

NUMBER OF TUBES PER RON: NUMBER OF ROMS PER PASS:

TUBE LENGTH 12. FT.

OUTSIDE AREA/PASS: 4132.2 SQ.FT. INSIDE AREA /PASS: 237.3 SQ. FT. FRONTAL AREA: 181.9 SC. FT.

(FOIL ING LENGTH= 0.7 FT.) NUMBER OF PASSES: 10 (TOTAL)
HEATING SECTION: 3
BOLL 10G SECTION;
SUPERHEATING SECTION: 4

HEAT EACHANGER PERFIRMANCE

FLUID TEMP. IN FLUID TEMF. DUT REYNOLDS AUPPER LAVG.) 4712.4 GAS TEMP. DUT GAS TEMP. IN HEATI 16 PTI 116 SEPERFEATING SECT ION

45957.4

STEAM PRESSURE: 400.0 PSIA (SATURATION TEMPERATURE= 444.6 F)

0.4 IN H20 STEAP FLEE FATE: 9524.5 LBM/HR.

GAS-SIDE PRESSURE JROP: PINCE PCINT: 29.3 F

SYSTEM PERFORMANCE

CONDENSER PRESSURE: 4,08 1N° HG STEAM TURBINE EFFICIENCY: 0,85 FW EAR PRESSURE: 15,0 PSIA LHV OF FUEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: STEAP TLABINE MCNSEPCWER: 1181.3 4843.0 1.1931 GT HEFSEPHAERIREVISEDI: TOTAL SYSTEM HJASEPOWER:

SPECIFIC FUEL CONSUMFITON ILBM-FJEL/ PP-HR3: STEAM TURBINE SHARE OF THE LOAD: 41.6 PERCENT

GT AT SYSTEM HP: GT AT SYSTEM HP! FUEL CCASUPFTICN ALT FILLY 1: 166.3 COUAS: 0.223 THERPOL EFFICIE 117:

RUN #52 RECOVERY UNIT DESIGN RUN

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	NOI NG	181
	CURRE SPU	1113.2
	PATINE HOUSE POWER 16421. U. APPRINT MATE CURRESPONDING SHIP SPEED: 20.0	89.0 LB#/HR
	16421.0.	ATE: 4075
	TASE PIWER B	GAS FLJH R
מים ורשפיאר	FY 1KF H	E AMA LS
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CALCA TO SEE THE SECOND A LABOR OF THE CODE COUNTY	GINS SAID	CDEEDS	0 00	× 16		
EXHALS TASS TENERALISES AND TASS TO THE CONTRACT OF STREET	LBP/S EC.1			:		
HEAT EACHANGER GE IMETRY						
CVERELL CLITCHS INS:		NLMBER	OF RO	NUMBER OF ROWS PER PASS:	.1	
12.00		NUMBER	OF TU	NUMBER OF TUBES PER ROWS	.08 tH	
11.16h': 1.3 FT.		TLBE LE	NGTH	TLBE LENGTH 12. FT.		
MEAT TANGER SOFTE IS IN.		01151DE	AREA	OLTSIDE AREA/PASS: 4081.2 SQ.FT.	81.2 SQ.F	1.
TUIE/FILL TO A VIGENIATE		INSIDE	AREA/	INSIDE AREA/PASS: 234.4 SO. FT.	.4 SO. FI	
FIN SPACE OF TILES FINS IN.		FOUNTAL	AREA	FOUNTAL AREA: 179.8 SU. FT.	0. FT.	
FIN THICKNESS: 1.024 M.		NUMBER	OF PA	S SEST B	ITOTAL	
TRANSVEASE TUBE SPACING: 2.25 IN.		500	200	MEALING SECTION:	,4c	7.0
ALL SECTIONS THE SPACEMENT IN SECTION OF			LENIE	1100		

LID TEMP. DUT REYNDLDS NUPRER IAVG.) 394-6 444-6 651-5 190071.5		
FLUID TENP. IN F. 200.0 394.6 444.6	• 444.6 FI	
CAS TEMP. IN GAS TEMP. GUT FLUID TEMP. IN FLLID TEMP. DUT 458.5 681.7 488.5 488.5 681.7 681.7 681.6	STEAM PRESSULE: 400.0 PSTA (SATURATION TEMPERATURE.) STEAM FLCK KATE: 18544.2 LBM/HR.	
	0.0 PSIA (SA 8544.2 LBM/HR P 70: 2.2 IV	u.
SECTION HEATING #314, 116 \$2,000 MAREATING	STEAM PRESSU E: 400.0 PSTA (SATURA STEAM FLCW HATE: 18544.2 LUM/HR. GAS-SICE PEESSURE UP 19: 2.2 IV HZD	PINCH PAINT: 93.3 F

ASSUMED SYSTEM CHARACTERISTICS:	CONDENSER PRESSURE: 4.CE 14. BS STEWN THE REFEICHNY: 0.85 FW HEATER PRESSURE: 15.0 PSIA	LHV OF FIJEL: 18400 BTU/LBM			
A 55.51			0.394	FUEL CENSIPETION LEVY-FUEL/HA-1: 010.1 GT AF SYSTEM HP: 8207.0	THENER EFFICIENTS COURSE 0.414 GT AT SYSTEM HPE 0.351
			HP:	HP:	Ho:
		_	SPECIFIC FUEL CLASSIMFTION (184-FJEL/ PP-HR): 61 AT SYSTEM HP: 0.394	SYSTEM	SYSTEM
		CEN	4	¥	7
		PE	E.	19	5
		23.0	34 16	1.0	4
5	30.4	ë	-F.1E	701	4.0
6143	44	VC1	A S :	A S.	A5 :
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×	HOK Des	SILAF	300	25	E43
ANCE	SEN TEN	41.1E	LY:	14.5	11.
FCR	3 %	2	5.1	TER	T CA
SYSTEM PERFCHANGE OT INPSENDATE IN EVISENDE 16143.9	STEAM TLAGINE MURSEPCHERE 4830.4 TCTAL SYSTEM MONSEPONERE 20974.3	STEAM TURNINE SHAKE OF THE LOADS 23.0 PERCENT	SPEC	FUEL	THEAD

HEAT EACHANGES PERFORMANCE

(BOILING LENGTH 5.5 FT.)

WASTE HEAT RECOVERY UNIT DESIGN RLN

GAS TURBINE

MAAKE HINSEPINER : 8520.00 APPROXIPATE CURRESPONCING SHIP SPEECE 16.0 KTS Expanse 6.5 Temberitale: 328641.0 1847HR (91.3 LBM/SEC)

HEAT EXCHANGES GEOMETRY

9VER N. 014C1511745: LNG'N: 12.0 FT. NIO N: 15.6 FT. FLICE: 1.5 FT.

HLAT TRAINER SUFFACE DATE IN THE FIRST OF THE TANK OF THE REST. THE TANK OF TA

LONGITUDINAL THE SPACINGS 1.95 IN. 2.25 IN. TRATISVE 4SE TUBE S TO FUGE

DLTSIDE AREA/PASS: 4081.2 SO.FT. INSIDE AREA/PASS: 234.4 SQ. FT. MUMBER OF PASSES: 9 JIDTALI HEATING SECTION: 3 BOLLING SECTION: 2 SUPERHEATING SECTION: 2 FP3NTAL AREA: 179.8 SO. FT. NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS : TLAE LENGTH 12. FT.

(HEAT ING LENGTH: 0.3 FT.)

HEAT EXCHANGE PERFORMANCE

GAS TEMP. DUT FLUID TEMP. IN FLLID TEMP. DUT REYNOLDS NUMBER LAVG.) STEAM PRISSULE: 400.C PSIA (SATURATION TEMPERATURE= 444.6 F) 481.5 LAS TEMP. IN HEATING BILL ING SUPERIEATING SECTION

115150.3

STEAM FLUE KATE: 23098.0 LBM/HR.

CAS-SIDE DAESSURE DRUPE 1.6 IN H20 PINCH PCINT: 36.3 F

SYSTEM FEEF CAMATICE

ASSUMED SYSTEM CHARACTERISTICS: STEAM TURAINE HIR SEPONER: 2913.9 THAL SYSTEM HIR SEPONER: 11306,5 UT HORSEPONEMIREVISEDI: 8392.6

CONCENSER PRESSURE: 4.08 IN BHG STEAN IURBINE EFFICIENCY: 0.85 H EM HANTER PRESSURE: 15.0 PSIA LIV OF FUEL: 18400 87U/LAM

SPECIFIC FUEL CONSUMPTION ILBY-FUEL /HP-HR): COLX: 0.529 COLX: 0.392 GT AT SYSTEM HP: STEAM TURBINE SHARE OF THE LOAD: 25.8 PERCENT

GT AT SYSTEM HP: 0.285 GT AT SYSTEM PP: FUEL CTISTMOT TTW (LBM-FUEL/HR.): G1 BALY: 4435.6 CUGAS: 4:35.6 COUAS: 0.352 THEN YEL CALY: 1515Y:

WASTE HEAT RECOVERY UNIT DESIGN RUN

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BRAKE HIJASEPIWEN: 1684.0, APPRUXIMATE CORRESPONDING SHIP SPEED: 9.0 KTS EXFAUST (4) TEMPLENTUME: 0689.0 F EXHALST GAS FLOW RATE: 159731.0 LBM/HR 144.4 LBM/SEC)

HEAT EXCEPTEER CETHETRY

DVER ALL DI MENSIONS: 12.0 FT. MICHAEL 15.0 FT. HEISATI: 15.0 FT. HEISATI: 1.1 FT.

LONGITUDITAL TORE SPACING: 1.95 IN. TRATISVERSE TUBE SPIC 196: 2.25 IN.

NUMBER OF TUBES PER ROWS NUMBER OF ROWS PER PASS:

OUTSIDE AREA/PASS: 4081.2 SO.FT. INSIDE AREA/PASS: 234.4 SQ. FT. FRONTAL AREA: 179.8 50. FT. TLBE LENGTh 12. FT.

NLWBER OF PASSES: 7 (TOTAL)
HEATING SECTION: 2
BOILING SECTION: 2
SUPERHEATING SECTION: 2

(BETTING LENGTH 3.6 FT.)

HEAT EXCHANGES DESENTANCE

FLUID TEMP. IN FLLID TEMP. OUT REYNOLDS NUMPER (AVG.) GAS TEMP. IN GAS TEMP. DUT ECTLING SCPCAMEATING SECTION

STEAM PRESSURE: 400.0 PSIA (SATURATION TEMPERATURE. 444.6 F)

0.4 IN H20 STEAM FLOW RATE: 9175.6 LBM/HR. GAS-SIDE PRESSINE UKOP:

PINCH PCINT: 36.2 F

SYSTEM PERFOR TINCE

CONCENSER PRESSURE: 4.08 IN. HG SFEAT TURBLINE EFFICIENCY: 0.85 THE FEATE PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 07U/LBM A SSUMED SYSTEM CHARACTERISTICS STEAP TLRSINE SHARE OF THE LOAD: 40.6 PERCENT STEAM TURBLIE HIN SEPCHER: 1134. 1 DITAL STEELY MARSEPOWER: 2796.2 GT HEFSEFUNERIAEVISECH: 1662.0

SPECIFIC FUEL CINSTANTION (LRY-FUEL /HP-HR):
CALY: 1.053 CAGAS: 0.632 GT AT SYSTEM HP: 0.864 FUEL CTTSUPPTING (LBM-FUEL/HR.): 1766.4

GT AT SYSTEM HP: 0.16C THE WALL SEPTCIFICY: COGAS: 0, 219

GT AT SYSTEM HP: 2416.0

RUN #4(0)

WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

GAS TURBINE

ктѕ		NLMBER OF ROMS PER PASS:	NEMBER OF TUBES PER ROWS	TUBE LENGTH 12. FT.
9.0		0F RC	0F T;	EN GT F
SPEEDI		NUMBER	NIMBER	TUBE L
RESPONDING SHIP				
BRAKE HORSEPONER: 1684.0. APPROXIMATE CORRESPONDING SHIP SPEED: 9.0 KTS Extaust GAS TEMPERATORE: 689.0 F Extaust GAS Flüh Rate: 159731.0 LBP/HR (44.4 LEP/SEC)	HEAT EXCEMBER GEONETRY	CVERALL CIMENSIONS:	1000 P. 1000 P	HEAT TRANSFER SUFFACE
	I			

(HEATING LENGTH 3.7 FT.) DUTSIDE AREA/PASS: 3250.5 SQ.FT. INSIDE AREA /PASS: 189.0 SO. FT. NUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION:
3 BOLLING SECTION:
5 SUPERHEATING SECTION:
3 FRENTAL AREA: 144.8 SQ. FT.

NTED FINS/IN.

FIN TYPE: SEGME FIN SPACING: 0.8 FIN PETCHT: 0.8

43.

5281.1 40471.1

HEAT EXCHANGER FERFORMENCE

LONGITUDINAL TUBE SPACING: 2.92 IN.

TRANSVERSE TUBE SPACING: 3.38 IN.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMPER LAVG.) STEAM PRESSURE: 800.0 PSIA (SATURATION TEMPERATURE 518.3 F) GA S- SIDE PRESSURE UKCP: 0.9 IN H20 STEAM FLOM RATE: 7577.0 LRM/HR. PINCE POINT: 25.5 F BCILING BCILING SUPEX FEAT 1'16 SECTION

SYSTEP FERFCREANCE

GT HOR SEPONER (KEVISED) : 1660.2

ASSUMED SYSTEM CHARACTERISTICS:

ONDERSER PRESSURE: 4.08 INTERNATION OF THE PRESSURE: 15.0 INTERNATION OF THE PRESSURE: 18400 2361.4 0.157 0.880 GT AT SYSTEM HP: GT AT SYSTEM HP1 SPECIFIC FIFE CONSUMPTION (1, RM-FJEL/HP-HR); GT ONLY: 1. C64 COGAS: 0.658 GT AT SYSTEM HP; STEAM TURNINE SHARE OF THE LOAD: 38.1 PERCENT FULL CONSIDERTION (LBM- FJEL /HR.): 05.9 THERMAL EFF ICHEY: 0.13 COGAS: 0.210 10 22.8 TCTAL SYSTEM HIRSEPONER: 2683.0 STEAP TURBINE HORSEPOWER:

RUN #5

WASTE HEAT RECOVERY UNIT DESIGN RLN

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IDING LEP/S
HRACE HISSEPINES: ESSO. O. APPROXIMATE CURRESPONDING SHIP SPEED: EXHALIC GAS TEMPERATURE: 32.8641.0 LBP/HR (91.3 LEP/SEC)
DXI HATE LBP/HR
742.0 H641.0
6526. C
TENPER
SAS SAS
HRANGE HE EXHAUST
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CVERALL DIVENSIONS: CVERALL DIVENSIONS: LEVISION 12.0 FT. TOBE LENGTH 12.0 FT. OUTSIDE AREA/PASS: 3250.5 SO.FT. INSIDE AREA/PASS: 189.0 SC. FT. FIN HICKLED 3.3 IN. INMANSAERSE TUBE SEACTION: 3.3 IN. LEDALITORING SECTION: 2.92 IN.	HRAKE HYSEPINES: ESSO.O, APPROXIMATE CURRESPUNDING SHIP SPEED: 16.0 KTS Exhauct oas teuperature: 742.0 F Exhaust 345 Flya Rate: 324641.0 EBP/HR (91.3 LEW/SEC)	JRRE SPON	DING SHIP LEM/SECI	SPEEDI	16.0	X TX		
NUMBER OF ROWS PER PASS: 1. NUMBER OF TUBES PER ROW: 43 TUPE LENGTH 12. FT. TUPE LENGTH 12. FT. OUTSIDE AREA/PASS: 3250.5 SC NSIDE AREA/PASS: 189.0 SC. FRONTAL AREA: 144.8 SC. FT. O. U.3 C. IN. NUMBER OF PASSES: 12 CTOTAL) S.33 IN. NUMBER OF SC. TOTAL) S.32 IN. S.33 IN. S.33 IN. S.33 IN. S.34 IN. S.35 IN	HEAT EXCENSES UPINETRY							
H.	CVERALL DIVENSI INST			NUMBER	OF RO	AS PER PASS	:	
TUPE LENGTH 12. FT. 1 1.4 IN. 1 1.4 IN. 1 1.5 IN. 1 IN. 1 1.5	F107h: 12-1 F7			NI WBER	OF 10	SES PER ROM	11 43.	
OUTSIDE AREA/PASS: 3250.5 SCINNIDE AREA/PASS: 189.0 SC. FRONTAL AREA: 144.8 SC. FT. NUPHER OF PASSES: 12 (TOTAL) HATING SECTION: 4 SUPEPHEATING SECTION: 4 SUPEPHEATING SECTION: 4	PEAT TABASER STREET			TURE LE	NGTH	12. FT.		
FRONTAL AREA: 144.8 SC. FT. NUPHER OF PASSES: 12 (TOTAL) HEATING SECTION: 6 SUPEPHEATING SECTION: 6	OLISIOE TUNE DIAMETER: 1.5 IN.			OUT STUE	AR EA	PASS: 329	10.5 SQ.F	-
FRONTAL AREA: 144.8 SC. FT. NUMBER OF PASSES: 12 (TOTAL) HEATING SECTION: SUPEPLEATING SECTION: 6	TUBELLIN ARKAIGEMENTS			INSIDE	AREA 19	ASS: 189.	0 SC. F	٠
NUMBER OF PASSES: 12 (TOTAL) HEATING SECTION: 4 BOILING SECTION: 6 SUPERFEATING SECTION: 2	NI/STI 76. 7 . 91 . 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.			FRONTAL	AREA	144.8 50	. FT.	
HEATING SECTION: 4 BOILING SECTION: 6 SUPEPLEATING SECTION: 2	Fla Tile Kat 55: 3.036 14.			NUPBER	OF PAS	SES: 12 (TOTAL !	
SUPEPHEATING SECTION: 2	TRANSVERSE TUBE SEACING: 3.33 IN.			#5	NZ ZZ	SECTION:	40	(HE
	IGNOTABLINAL THE SPECIAGE 2.92 IN.			S	PEPFE	ATING SECTION	N: 2	6

	3.4 FT.1
	LENGTH.
	(HEATING
(TOTAL)	ICN: 2
PASSES: 12	BOTE ING SECTION: SUPEPHEATING SECTION:
NUPBER OF	SUPER

SECTIN GAS TEMP. IN GAS TEMP. DUT FLUID SECTIN GAS TEMP. IN GAS TEMP. DUT FLUID SEATHER THE SECTING 547.5 547.9 500.0 632.5 518 STEAM PRESSURE: 800.0 PSIA ISATURATION TEMPERATURE 518 STEAM FLOW RATE: 19998.4 LBW/HR.		GAS TEMP. IN GAS TEMP. DUT FLUID TEMF. IN FLUID TEMP. DUT PEYNOLDS NUMFER (AVG.)	511.4	•	518.3 F1	
TITY GAS TEMP. IN THE GAS TEMP. IN THE GAS.5 EMEATING 642.5 EMEATING 640.6 SU.AE: 800.0 PSIA (SATI		GAS TEMP. DUT FLUID T	547.5		URATI CN TEMPERATURE - 518.	
	IEAL EACHANGEN PENFORMANCE	SECTION GAS TEMP. IN		בייונים וויים	SCAE: 800.0 PSIA ISATI	STEAM FLOW RATE: 19998.d LBW/HR.

GAS-SIDE PRESSURE DROPE 3.1 IN HZD FINCE PTIN'T JUST F

ASSUMED SYSTEM CHARACTERISTICS: SPECIFIC FILL CONSUMPTION (LR4-FILL/HP-HHI):
51 JILY: J.533 CO.AS: 0.403 GIAT SYSTEM HP: 0.482
FUEL CONSUMPTION (LR*-HJEL/HR.): 4432.5 GT AT SYSTEM HP: 5300.1 GT AT SYSTEM HP: 0.287 STEIN FURNINE SHARE OF THE LUAD: 23.9 PERCENT COUAS: 3.543 STEAM TURELNE HORSEPCHER: 2629.1 TITAL SYSTEM HIRSEPINERS 10995.6 GT HT SEPTERINEVISEDI: 8360.4 THEN GE LALTS 16.261 SYSTEP FEFF CREANCE

RUN #6(0)

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WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

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BY WE WINGSEPTHER 1 6421.0. APPROXIMATE CORRESPONDING SMIP SPEECT 20.0 KTS CARAIST GS TEMPERATURE 1 849.0 FEMALST GS FEDW RATE: 407889.0 LBM/HR 1113.2 LBM/SECT

HEAT EXCHANGER GEOMETRY

CV ERALL ELYETSINGS: ELNGTH: 12.0 FT. HINTH: 12.1 FT. HELGAT: 2.9 FT.

DUTSIDE TOUR DIAMETER: 1.5 IN.
DUTSIDE TOUR DIAMETER: 1.4 IN.
THEFT TORE OF ANGENIER: 1.4 IN.
THEFT TO SALING: CHANTED
FIN PLEINT: C. 7.52 FINS/IN.
FIN PLICKIES: 0.036 IN. HEAT

LENGITUDINAL TUBE SPACITIC: 2.92 IN. TRANSVERSE TLUE SPACINGS 3.34 IN.

NUMBER OF TUBES PER ROWS NLMBER OF ROWS PER PASS:

OLISIDE AREA/PASS: 3250.5 SO.FT. INSIDE AREA/PASS: 189.0 SC. FT.

TUBE LENGTH 12. FT.

FRONTAL AREA: 144.8 SQ. FT.

(HEATING LENGTH= 0.3 FT.) NUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION: 5
SUPERHEATING SECTION: 6

HEAT EXCHANGE FERFORMANCE

SEC TI IN

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) 187516.3 \$72.0 814.7 SUPERFERTING

STEAM PRESSURE: 600.C PSIA (SATURATION TEMPERATURE 518.3 F)

GE 5- SIDE PRESSURE DRCF: 4.5 IN H2D STEAM FLOW 94TER 35912.3 LBM/HR.

PINCE 00111: 55.0 F

SYSTEP PEFFURDANCE

CONDENSER PRESSURE: 4,08 IN SHE STEAT TURBINE EFFICIENCY: 0.85 THEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 1840C BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: STEEM TURELIE HUR SEPCHER: 4703.0 GE HERSE FEWENINE VISEEN: 16066.0

SPECIFIC FIFE CCASUMPTING (LBM-FUEL/PP-HR):
GI ONLY: 0.436 COCAS: 0.337 GT AT SYSTEM HP: 0.398 STEAM TURNINE SHARE OF THE LUADS 22.6 PERCENT

TOTAL SYSTEM HORSEPC NER: 20765.1

GT AT SYSTEM HP: FUEL CONSULPTION (LBM-FJEL/HR. 1: 6999.4

0.347 GT AT SYSTEM HP : CO CAS: 0.410 THER AL EFF IC IENCY;

MASTE HEAT RECOVERY UNIT DESIGN RUN RUN #14

CAS TURBINE

PRIVE HINSIPINER: ESSO.O. APPROXIMATE CORNESPONDING SHIP SPEED: 16.0 KTS
TALOIS EST TEVEZETURE: 324641.3 LBW/HR (91.3 LBW/SEC)

HEAT EXCHANSER GEOMETRY

CVERAL CIVETSINGS: FINAL TIME 12.0 FT. FINAL 12.1 FT. FILEFT: 3.2 FT.

LONGITUDINAL TURE SPECINGS 2.92 IN. TRANSVERSE FIRE CARCINGS 3.38 EN.

(BALLING LENGTH: 3.5 FT.) OLTSIDE AREA/PASS: 3250.5 SG.FT. INSIDE AREA/PASS: 189.0 SC. FT. FPINTAL AREA: 144.8 SO. FT. NUMBER OF TUBES PER ROWS TURE LENGTH 12. FT.

NUMBER OF ROWS PER PASS :

NUMBER OF PASSES: 13 (TOTAL)
HEATING SECTION:
601.18.0. SECTION:
5.19 EP EATING SECTION: 2

HEAT EXCESSION DESENTANGICE

FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMPER (AV). 1 14511.6 GAS TEMP. IN GAS TEMP. BUT PEST FIG PCST INC SUSTRACATION SEC TION

122571.0

STEAM FAES TINE: 000.0 PS 14 (SATURATION TEMPERATURE 486.3 F)

3.3 PH H20 SIECM FLD4 RITE: 21557.0 LBMAIR. GAS-SILE PRESSURE CPCP:

PINCH 931411: 37.1 F

SYSTEM DENT 12 44 4CE

CONDENSER PRESSURE: 4.08 IN. HG STEATURBLAK EFFICIEKCY: 0.885 HW HEATER PRESSURE: 15.0 PELA LHV CF FUEL: 18400 RFUZLR A SSLMED SYSTEM CHARACTERISTICS: STEAM (URALINE HTH SEPOWER: 2837.8 8363.3 GT HCF: LFJWEN (REV IS EC):

STEAM THEEINE SHARE OF THE LAKE: 25.3 PERCENT TOTAL SYSTEM HORSEPOWER: 11201.1

GT AT SYSTEM HP: 5368.1 SPECIFIC FUR COASMMITTIN (LINF-FUEL/HP-HR): 0.475 FLEE CONSUMPTION (LBN-FUEL/HR.): of THIF: 4+32.0 CONS: 4:32.6

GT AT SYSTEP HP! 0.289 COJAS: C.349 THERE ENTINENCY:

RUN #13(0)

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

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BRANE HOASEPUNER: 16421.0, APPROXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS EXPANST GAS TEMPERATURE: 849.0 F EXHALST GAS FLOW RATE: 4.07589.0 LAW/HR (113.2 LAW/SEC)

HEAT EXCHANGER GEOMETRY

CVENAL CINESTRISS FT.

LCNGITUDINAL TUBE SPACING: 2.92 IN. TRANSVERSE TUBE PACING: 3.38 IN.

NUMBER OF TUBES PER ROW: NUMBER OF RCWS PER PASS :

TURE LENGTH 12. FT.

NUTSIDE AREA/PASS: 3290.5 SO.FT. INSIDE AREA /PASS: 189.0 SO. FT. FRENTAL AREA: 144.8 SQ. FT.

NUMBER OF PASSES: 13 (TOTAL)
HEATING SECTION: 5
SUPERHEATING SECTION: 2

HEATING LENGTH= 1.5 FT.1

HEAT EXCHANGES PERFORMENCE

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYIDLDS NIMBER (AVG.) 25259.9 SUPERFERENCES SEC (1) IN

216614.1

STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE= 486.3 F)

GAS-SIDE PRESSURE DRCP: 4.9 IN HZD STEAM FLOW RATE: 37502.9 LAWAMS.

PINCE PAINT 33.5 F

SYSTEM PERFUP SANCE

CONCENSER PRESSURE: 4.08 IN HG STEM TURBINE EFFICIENCY: 0.85 FW FEMFER PRESSURE: 15.0 PSIA LHV OF FUEL: 18430 BTU/LBM ASSUMED SYSTEM CHAPACTERISTICS: STEAM TIREINE HIT SEP IMER: 4902.1 GT HOR SE FCHERINEVISEUI: 16053.9

SPECIFIC FUEL CONSUMPTION (LAM-FUEL/HP-HA):
CALY: 0.446 COGAS: 0.334 GT AT SYSTEM HP: STEAM TURBINE SHARE OF THE LOAD: 23.4 PERCENT TOTAL SYSTEM HORSEPOWER: 20955.9

GT AT SYSTEM HPS FUEL CHASHMPTING (LBM-FUEL/HR.): 6997.8

COGAS: 0.414

GT AT SYSTEM HP 8 0.35C

C8/21/75 15.48.33

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUL RUN #15(0)

GAS TUREINE

BHANE HCASE PCHEK: 1684.0. APPROXIMATE CORRESPONDING SHIP SPEED: 9.0 KTS
EXPINST (15 TE40 EATTURE: 689.0 F BM/HR (44.4 LBM/SEC)

MEAT EXCHANGER GECHETHY

MENT TRANSPERS SUFFICIENT 1.5 IN.
14510E THE CLAMETER: 1.6 IN.
14510E THE CLAMETER: 1.635 IN.

NUMMER OF PASSES: 13 (TOTAL)
HEATING SECTION: 3
BJLLNG SECTION: 6
SUPERFEATING SECTION: 6

FF911TAL AREA: 144.8 SO. FT.

OUTSIDE AREA/FASS: 3290.5 SO.FT. INSIDE AREA/PASS: 189.0 SQ. FT.

NUMBER OF TUBES PER ROWS NUMBER OF RCWS PER PASS:

TUBE LENGTH 12. FT.

(HEATING LENGTH: 4.8 FT.)

HEAT EACHANGER PE-FORMANCE

LOWETTUCKING THRE SP. CING: 2.92 IN.

THAN VERSE TIBE CPACING: 3.38 IN.

FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER LAVS. 1 GAS TEMP. IN GAS TEMP. DUT 498.9 SOFE HEATING SEC TI ON

49203.8

STEAM FRESTURE: 630.0 PS IA (SATUPATION TEMPERATURE= 486.3 F)

STEAM FLOW RATE: BOLZ.9 LBM/HR.

0.9 IN H20 CAS-CIJE FRESSURE CROP: PI'1CH PILIT: 21.6 F

SYSTEM PERF 12447CF

A SSUMED SYSTEM CHARACTERISTICS: 1135.5 IJIAL SYSTEP HOF EPCHER: 2795.6 ET PER EFE JEHIREVISEED: 1640.1 STENY FURCINE HORSE POWERS

CONDENSER FHESSURE: 4.08 IN MC STEAM TURNINE EFFICENCY: 0.85 FHEN TRANSPESSURE: 15.0 PSIA LHV DF FUEL: 18400 RTU/LAM

SPECIFIC FUEL CURSIMPTION (LBM-FIEL/HP-HRI: CYSTEM HP: 0.864 STEAP THEBLAE SHARE OF THE LOAD: 40.6 PERCENT

GT AT SYSTEP HP: 2415.7 FUEL CONSUPERIOR GLBP-FUELVHR. 1: 1265.9

GT AT SYSTEM HP: 0.160 THERMAL EFFICIENCY: COURS: 0.219

RUN #18(0)

HASTE HEAT RECOVERY UNIT OFF-DESION RUN

08/25/79 13-13.56

5.0 K1S BANKE HEFSEPCHER! 1684-0, APPRIXIMATE CORRESPONDING SHIP SPEED: Exhaust 645 Temperature: 159731-0 LBM/HR (44.4 LBP/SEC) GAS TURBINE

HEAT EXCLANGER GEIMETEY

CVERALL DI MENSIJAS: FLEVENIN 12.0 FLEVENIN 12.0 FT. HE IGHI: 2.0 FT.

THANSPER SURFACE I 1.0 INOLISTO TOPE OLIMETER: 0.9 INTHAT CAPANCE PENT
THAT CAPANCE PENT
FOR THAT CAPANCE HEA1

LONGITLDINAL TUBE SPACING: 1.95 IN. 2.25 IN. TRANSVERSE TLUE SPACINGS

HEAT EACHANGER PERFORMANCE

SECT 10N

(HEATING LENGTH- 3.7 FT.) OUTSIDE AREA/ PASS: 3264.9 SQ.FT. INS 10E AREA/PASS: 187.5 SO. FT. NLPBER OF PASSES: 12 (TOTAL)
HEATING SECTION:
BOILING SECTION:
SUPERHEATING SECTION:
3 FRONTAL AREA: 143.8 SQ. FT. NUMBER OF TUBES PER ROLE NUMBER OF ROMS PER PASS: TLBE LENGTH 12. FT.

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMF. OUT REYNOLDS NUPPER (AVG.)

50891.9

STEAM PRESSURE: 400.0 PSIA (SATURATION TEMPERATURE: 486.3 F) HEATING BOIL 146 SLPEREATING

STEAM FLUE RATE: 8931.9 LBM/HR.

GAS-SIJE PRESSUFE JROP: 0.9 IN H20

PINCE POINT: 15.0 F

SISTEM PEPF CRMANCE

STEAP TURNINE HERSEPCHER: 1177.6 TOTAL SYSTEM HORS EPOWER: 2831.7 GT HCRSEP.INER (REVISED): 1660.1

STEAM TUPBLUE SHARE OF THE LOAD: 41.5 PERCENT

GT AT SYSTEM HP: 2435.6 SPECIFIC FUEL CONSUPFIED ILBN-FJEL/PP-HRI: SYSTEM HPS OT DALY: 1.064 COGAS: 0.622 GT AT SYSTEM HPS FULL CCASHHETTICN ILE"-FUEL / PR. 1: 155.9

0.858

GT AT SYSTEM HP: 0.161

COGAS: 0.222

THERPAL EFFICIENCY:

CONDENSER PRESSURE: 4.00 IN HG STEM FURBINE EFFICIENCY: 0.055 FW HMATIER PRESSURE: 15.0 PSTA LHV OF FUEL: 18400 BTU/LBM

A SSUMED SYSTEM CHARACTERISTICS:

MASTE HEAT RECOVERY UNIT OFF-DESIGN RIM RUN #17(0)

645 TuenIN

HATAS HINSTRUM AS SECTION SECTION APPRIATMENTS CORRESPONDING SHIP SPEEDS 16.0 KTS LANGUS USS STEPPERATOR SECTION SHIP SPEEDS 16.0 KTS LANGUS USS SECTION STEELS 220641.0 LANGUS 191.3 LBM/SECT

HEAF EAFHA'ILF Git 16 FAY

HEAT THATSLES SUCFICE 150 IN. 1014. THE SUCFICE SUCFIC UNE ANT THE STATE OF THE STATE

OUTSIDE AREA/PASS: 3264.9 SU.FT. INSIDE ARFAZOASS: 187.5 SO. FT. 64. NUMBER OF PASSES: 12 (TJTAL)
HEATING SETION: 6
SUPEPHEATING SETION: 6
SUPEPHEATING SETION: 2 FRUNTAL APFA: 145.8 50. FT. NUMBER OF PAMS PER PASSE NUMBER OF TURES PER RCM: TUBE LENGTH 12. FT.

(BOILING LENGTH: 3.8 FT.)

HEAT FALHARGEN FEFFURNEICE

LOJGITUDINAL TUBE, SPICING: 1.95 IN.

TARNSVIRSE TOOP SPACINGS 2.25 14.

FLUID TEMP. IN FLUID TEMP. OLT DEYNOLDS NUMBER (AVG.) 15413.7 125586.6 SIFAM PACISHAFI GOD.O PSII (SATHGATION TEMPERATURE: 486.3 F) GAS TEMP. IN GAS TEMP. DUT 645-5106 M 1250RF BENP: 3.3 IN H20 STEAM FLUM FATE: 22656.2 LB4/HR. 142.3 PINCH POLICIE 21.5 F 6 111 Pr6 8 111 Pr6 Supt Fort & 11 30 5. (111:1

SYSTEM PERFUNITION

SIFAM Librattar Snare, if The LOAD: 26.2 PERCENT STEAM THOUSE HOR SCHOOL R. 2467.9 TJIAL SYSH A HOWSEPCALF : 113.11.4 GT MENSEP JEFFHEVISEDIE 8363.5

CONDENSER PRESSUPE: 4.03 IN HG STGAM TYAHINF EFFICTENCY: 0.85 EM HALFE ORESSUPE: 15.0 DSIA LIV OFFICE: 18400 9TULLA

ASSUMED SYSTEM CHAPACTERISTICS:

SPECTFIC FULL COLSTANTICE (LAM-FULL AND -HP):
61 DALY: 0.534 CCCAS: 0.391 61 AT SYSTEM HP: 0.478 GT AT SYSTEM HP: FIRE CONSCIPTING (LATER LEGANS) 4412.6 The set of the late Vi Course 0.354

GT AT SYSTEM HP: 0.250

85.21.19 13.16.58

RUN #16

The same of

WASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TUPRIME

BRAKE HERSEPHERS 16421-0. APPRIXIMATE CORRESPONDING SHIP SPEEDS 20.0 KIS FAMAUS 645 TEMPLEATURE: 849.0 F EXFAUST 645 FLOW STES 4-J7589.0 ERMINE (113.2 LBP/SEC)

HEAT EXCHANGES GENETHY

HEAT TRANSPER SUFFACE TO IN.
COSTS TWIT DIAMETER: 1.0 IN.
COSTS THE CLAMETER: 0.9 IN.
COSTS THE CLAMETER: 0.9 IN.
COSTS THE CLAMETER TO COSTS THE DVAALL DIPENSIONS: FF. WILLSON FT. HELDEN E. 2.6 FT. HELDEN E. 2.6 FT.

LURGITUDITAL TUBE SPACING: 1.35 IN. TRANSVERSE TUBE SPACING: 2.25 IN.

(PEATING LENGTHS 5.1 FT.) OUTSIDE AREA/PASS: 3264.9 SQ.FT. IMSIDE AREA/PASS: 167.5 SO. FT. NUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION: 6
BOLLING SECTION: 6
SUP ERHEATING SECTION: 2 64. FRINTAL AREA: 143.E SC. FT. NUMBER OF TUBES PER ROW! NIMBER OF ROWS PER PASS: TLBE LENGTH 12. FT.

HEAT EACHANGER PERF JANNICE

GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT PEYNTLDS NUMPER (AVG.) 230765.6 STEAM PRESSURES GODEO PSIA ISATURATION TEMPERATURE 486.3 F) \$101.5 \$10.9 707.6 GAS TEMP. IN STEAM FLCh RATE: 39 159.0 LBM/HR. HENTING HOLL 116 SUPERHEATING SECTION

645-5166 PRESSUPE PROP: 4.9 IN H20 PINCH POINT: 48.4 F

SYSTEM PERFUMPANCE

CONDENSER PRESSURE: 4.08 IN. HG STEAM TIPPINE EFFICIENCY: 0.85 STEAM TIPPINE EFFICIENCY: 0.85 LHV OF FUEL: 1840 RIULY ASSLMED SYSTEM CHAPACTERISTICS: SPECTFIC FUEL CHAS IMPTION (LAM-FIEL/HP-HR):
CT 31L(1: 0.410 C.03AS: 0.329 GT AT SYSTEM HP: 0.387 GT AT SYSTEM HP: STEAM THAN HE SHAVE OF THE LOADS 24.6 PERCENT FUEL CENSORM 10N (LEV-FUEL/HR.): 6497.7 CCGAS: 0.421 STEAM TERMINE HONSEPEWER: 5232.3 TUTAL SYSTEM HITE EPOTER: 21285.7 GT HCF SEPTHER IP EV 15E91: 16053.3 This per eff is lengy:

GT AT SYSTEP HP:

RUN #24(0)

WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

GAS TURPINE

SPEED: 9.0 KTS		NUMBER OF ROMS FER PASS: 1.	NUMBER OF TUBES PER ROLE 43.	TUBE LENGTH 12. FT.	OUTSIDE AREA/PASS: 3290.5 SO.FT.	INSIDE AREA/PASS: 189.0 SO. FT.	FRONTAL AREA: 144.8. SO. FT.	NUMBER OF PASSESS 12 (TOTAL)
BRAKE HORSEPUWER: 1644.9, APPROXIMATE CORRESPONDING SHIP SPEED: 9.0 KTS EXPANST GAS TENPERATURE: 089.0 F EXHALST GAS FLOW RATE: 159731.0 LAM/HR (44.4 LBM/SE3)	HEAT EXCHANGEF GECNETRY	DVERALL DIMENSIONS:	MD14: [2.] FT.	HEAT TOANCE ON CHEER F.	OUTSIDE TUBE DIAMETER: 1.5 IN.	TOTAL TANK ACCEPTED.	FIN SPACING 7.92 FINS/IN.	FIN THICKNESS: 0.036 IN.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) 54546.6 STEAM PRESSURE: 400.0 PSIA (SATURATION TEMPERATURE. 444.6 F) 0.8 IN H20 STEAM FLOW RATE: 9377-8 LBM/MR. CAS-SIDE PRESSURE DROP : PINCH POINTS 32.4 F HEAT EACHANGER PERFORMANCE HEATING BOIL 196 SLPERJEATING SECT ION

CONDENSER PRESSURE: 4.08 IN HG STEAM TURBINE EFFICIENCY: 0.85 FW HEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 8UVLR9 ASSUMED SYSTEM CHARACTERISTICS: STEAM TURBINE HORSEPOWER: 1187.4 TOTAL SYSTEM HUMSEPOWER: 2847.8 GT HCFS EFONER IR EV IS EG): 1660.4 SYSTEM PERFORMANCE

GT AT SYSTEM HP: 2440.3 SPECIFIC FLEL CONSUMPTION (1884-FUEL/MP-HR): 0.857 FUEL CUNSUMPTION (LBP-FUEL/HR-): 186.0 THER PAL EFFICIENCY:

STEAM TURBINE SHARE OF THE LOAD: 41.7 PERCENT

GT AT SYSTEP HP: 0.161

COGAS: 0.223

LONGITUDINAL TUBE SPACING: 2.92 IN.

TRANSVERSE TUBE SPACINGS 3.38 IN.

(HEATING LENGTH- 1.9 FT.)

NLMBER OF PASSES: 12 (TOTAL)
HEATING SECTION:
3
BOILING SECTION:
5
SUPERHEATING SECTION:
4

14.75.719 13.57.41

RUN #23(0)

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WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

GAS TLRIBINE

PRAKE HIPSEPOWER: 8526.0, APPROXIMATE CORRESPONDING SHIP SPEED: 16.0 KTS
EXHAUST GAS TEMPERATURE: 742.0 F
EXHALST GAS FLIW RATE: 328641.0 LBM/HR (91.3 LBM/SEC)

HEAT EXCEANGER GEOMETRY

CVERALL CIMENS 13NS: FT. 12.0 FT. H.OTF: 12.1 FT. HELLINT: 2.4 FT.

HEAT TAMSFE'S SUPERICE 1.5 IN.

10.15 12 TOUR DIANTER: 1.4 IN.

10.36 FIN ARANCETNIE: 1.4 IN.

10.36 FIN TYPE: SCHEMIED

FIN TYPE: SCHEMIED

FIN THE LEFT

FIN THICKLESS: 0.033 IN.

LCAGITUCINAL TUBE SPACING: 2.92 IN. TRANSVERSE TUBE SPACING: 3.38 14.

OUTSIDE AREA/PASS: 3250.5 SO.FT. INSIDE AREA /PASS: 189.0 SO. FT. FRUNTAL AREA: 144.8 SQ. FT. NEMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASSE TUBE LENGTH 12. FT.

(HEATING LENGTH 1.5 FT.) NUMBER OF PASSES: 10 (TOTAL)
HEATING SECTION: 3
BULLING SECTION: 2
SUPERHEATING SECTION: 2

HEAT EXCHANGES PERFORMANCE

GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) STEAM PRESSUPE: 400.0 PSIA (SATURATION TEMPERATURE. 444.6 F) GAS-SIDE PRESSURE DRIPE 2.5 IN H.20 GAS TEMP. IN STEAM FLCW RATE: 21974.8 LBM/HR. HEAT ING BCILING SLPEKHEAT ING SECTION

126450.5

SYSTEM PERFCHPANCE

PINCH POINT: 61.6 F

CONDENSER PRESSURE: 4.08 IN. HG STEAM TURBINE EFFICIENCY: 0.85 FW HERSESURE: 15.0 PSIA IHV OF FUEL: 18400 BTULES ASSUMED SYSTEM CHARACTERISTICS: SPECIFIC FUEL CONSUMPTION (LBM-FUEL/MP-HR): 61 July: 0.529 CDGAS: 0.400 GT AT SYSTEM HP: STEAM TURBINE SHARE OF THE LOAD: 24.4 PERCENT STEAM TURGINE HOR SEPCHER: 26%.7 TOTAL SYSTEM HURSEPCWER: 11073.4 GT HORS EPONEN (R EV ISED): 83 76.7

GT AT SYSTEM HPE 5326.0 FUEL CUNSUMPTION (LBP-FUEL/HR.): THERPAL EFFICIENCY! COGAS: 0.345

GT AT SYSTEM HP!

RUN #22(0)

WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

CAS TURBINE

PRAKE FESE POAFR: 16421.0. APPRIXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS Stands 1645 Temperalure: 80450.0 FEBRACS (183.2 LBM/SEC) Extust Gas flow Rate: 401586.0 EMARR (183.2 LBM/SEC)

HEAT EXCHANGER GETMETRY

OVERALL DIMENSIONS: FT. HISTORY IZ-0 FT. HISTORY IZ-1 FT. HEISAT: Z-4 FT.

HEAT TRANSE EN SURFACE DAMETER: 1.5 IN1115 DE TUBE CLARETER: 1.5 IN1115 DE TUBE CHE: 0.0.036 IN-

LONGITLDINAL TUBE SPACING: 2.92 IN-TRANSVERSE TUBE SPACING: 3.34 IN.

NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS:

OUTSIDE AREA/PASS: 3290.5 SQ.FT. INS 10E AREA /PASS: 189.0 SQ. FT. TLBE LENGTH 12. FT.

(POIL ING LENGTH 3.7 FT.) NUPBER CF PASSES: 10 (TOTAL)
HEATING SECTION:
B71L 1NG SECTION:
SUPERHEATING SECTION: 2 FRONTAL AREA: 144.8 .50. FT.

HEAT EXCHANGER PERFORMANCE

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) HEATING BOILING SUPLEMEAT ING SECTION

219577.9

STEAM PRESSUPE: 430.0 PSIA ISATURATION TEMPERATURE. 444.6 F)

STEAP FLEW RATE: 36760.7 LBM/IR.

GAS-SIDE PRESSURE DRCP: 3.8 IN H20 FINCH PCINT: 96.7 F

SYSTEP FEFF CAPANCE

ASSUMED SYSTEM CHARACTERISTICS: STEAP TURBLAE HORSEPCWER: 4524.0 TOTAL SYSTEM HIRSEPOWER: 20614.9 GT HORSEPOWERIREVISED1: 16090.9

CONDENSER PRESSURE: 4.08 1% HG STEM AN TURRINE EFFICIENCY 0.85 FWANTER PRESSURE: 13.0 PSIA LHV OF FUEL: 18400 BTU/LBM

SPECIFIC FUEL CONSUMPTION (LBN-FUEL/M-HR):
61 GALY: 0.435 COGAS: 0.340 GT AT SYSTEM HP: 0.401 STEAM TURNINE SHARE OF THE LOAD: 21.9 PERCENT

GT AT SYSTEM HP: 0.345 COUGAS: 0.407 THERMAL EFFICIPICY:

FILE CTYSUMPT 174 (LBM-FUEL/HR.): 7002.8

GT AT SYSTEM IP:

MASTE HEAT RECOVERY UNIT DESIGN RUN

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PRAKE HORSEPOWER! 1684-0. APPROXIMATE CORRESPONDING SMIP SPEED: 9.0 KTS Springs of Temperstynes: 9680.0 February 144.4 LBM/SEC) Ekrauci ea: Flow Rate: 15973.0 LBM/HR 144.4 LBM/SEC)

HEAT EXCHANGER GECNETRY

THER THE BINENSIONS IN THE STATE IN THE STAT

HEAT TARNSFER SUFFACE THE DISTINGUISE TO THE DISTIN LONGITUDINAL TUBE SPACING: 2.92 IN. TRINSVEGSE TUBE ST. CING: 3.38 IN.

(BEATING LENGTH 1:2 FT.) OLTSIDE AREA/PASS: 3290.5 SQ.FT. INSIDE AREA/PASSI 189.0 SO. FT. NUMBER OF PASSES: 10 (TOTAL)
HARTING SECTION:
3
BD1.1106 SECTION:
2
SUPERHEATING SECTION:
2 FRANTAL AREA: 144.8. 50. FT. NUMBER OF TUBES PER ROWS TLBE LENGTH 12. FT.

NUMBER OF ROWS PER PASS:

HENT EXTENDER PERFORMANCE

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLLID TEMP. DUT REYNOLDS NUMPER (AVG.) STEA" PRESSU E: 400.0 PSIA (SATURATION TEMPERATURE 444.6 F) 412.6 0.1 IN 120 STEAM FLCh RATE: 9425.4 LBM/HR. GAS-SICE DE ESSUPE DE OPPE PINCH POINT: 33.6 F HEATING BOIL 116 SLPERHEATING NC1 .395

5841.8

.

SYSTEM PERFCRIPANCE

CONDENSER PRESSURE: 4,08 IN. HG STEM TURBINE EFFICIENCY: 0,885 FLAM HEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 2428-1 SPECIFIC FUEL CONSIMPLION (LBM-FJEL/HP-HR): GT ONLY: 1.063 COGAS: 0.626 GT AT SYSTEM HP: 0.860 STEAM TURBINE SHORE OF THE LOADS 41.1 PERCENT FUEL CONSUMPTION (LBM-FUEL/HR.): GT ONLY: 1766.1 STEAM TURBINE HURSEPCHER: 1161.0 TOTAL SYSTEM HOR EPOMER: 2821.9 GT HIRS EPINE : (R EV ISED 1: 1660.9

GT A' SYSTEM HPE

COGAS: 0.221

HERPAL EFF ICLENCY:

(8/25/19 13.47.43

RUN #23(o)

MASTE HEAT RECOVERY UNI T OFF-DESIGN RUN

6.45 TURBINE Brake Horsep: JMER: 6526.0, APPROXIMATE CORRESPONDING SHIP SPEED: 16.0 KTS Exhalst Gas Federature: 328641.0 EBW/HR (91.3 LBM/SEC)

NUMBER OF ROWS PER PASS: 1.

NUMBER OF TUBES PER ROW: 43.

TUBE LENGTH 12. FT.

OLTSIDE AREA/PASS: 3290.5 SQ.FT.

INSIDE AREA/PASS: 189.0 SC. FT.

FRONTAL AREA: 144.8 SQ.FT.

NUMBER OF PASSES: 12 (TOTAL)

NUMBER OF PASSES: 12 (TOTAL)

SUPERING SECTION: 2 (BOILING LENGTH: 1.0 FT.)

SUPERING SECTION: 2 (BOILING LENGTH: 1.0 FT.)

GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) 133818.8 STEAP PRESSURE: 400.0 PS IA (SATURATION TEMPERATURE# 444.6 F) GAS-SICE PRESSURE DRCP: 3.0 IN H20 GAS TEMP. IN STEAM FLOW RATE: 23255.8 LBM/MR. HEAT EXCLANGER PERFORMANCE PEATING PCILING SLPFRHEATING SEC TI ON

SYSTEM PERFORMANCE

PINCH POINT: 41.8 F

CONDENSER FRESSURE: 4.08 IN BHG STEAM TURNINE EFFICIENCY: 0.85 FW HESSURE: 15.0 PSIA LIV OF FUEL: 18400 8TU/L8M ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 5382.0 SPECIFIC FIFE CONSUMPTION (LBM-FUEL/HP-HR): 61 ONLY: 0.530 COGAS: 0.394 GT AT SYSTEM HP: 0.479 GT AT SYSTEM HP: 0.289 STEAP TURBINE SHAFE OF THE LOADS 25.6 PERCENT FUEL C VISUAPTION (LB4-FUEL /HR.): 4433.1 COGAS: 0.351 STEAM TURBINE HIRSEPOWER: 2874.4 TOTAL SYSTEM HURSEPONER: 11243.3 GT HCHSEFCHEKIREVISEDIE 8368.8 THE GAL EFF ICIENCY:

258

LONGITUDITAL TUBE SPACING: 2.92 IN.

THANSVERSE THUE SPACING: 3.38 IN.

08/22/79 16.39.47

RUN #22

WASTE HEAT RECOVERY UNIT DESIGN RUN

GAS TURRINE

PRAKE FCRTEPOMER: 16421-0. APPRIXIMATE CORRESPONDING SHIP SPEED: 20.0 KIS EXHALSI GAS TEMPERATURE: 0849.0 F EXFLUST GAS FLIM GATE: 407589.0 LBM/HR (113.2 LBM/SEC)

HEAT EXCEATEER GE WETHY

OVERALL DI MENSION: LENGTH: 12.0 FT. MID'H: 12.1 FT. HEIGHT: 2.9 FT.

FIN TOPE SEGMENTED FINS IN. HEAT TRANSFER SURFACE OLTSIDE TUBE DIA INTIDE UBE DIANTE

LONGITLOIMAL TUBE PACING: 2.92 IN. TRANSVERSE TUBE SPACING: 3.38 IN.

(HEATING LENGTHE 3.4 FT.) DITS TUE AREN PASS: 3290.5 SQ.FT. INSIDE AREA/PASS: 189.0 SQ. FT. FRONTAL AREA: 144.8 SQ. FT. NUMBER OF TUBES PER ROM! NUMBER OF ROWS PER PASS : TLBE LENGTH 12. FT.

MUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION: 6
HOLLING SECTION: 6
SUPERHEATING SECTION: 2

HEAT EXCHANGER PERFORMANCE

GAS TEMP. IN GAS TEMP. OUT FLUID TEMF. IN FLUID TEMP. OUT REYNOLDS NUMPER (AVG.) 23652.1 STE'M PRESSURE: 400.0 PSIA (SATURATION TEMPERATURE 444.6 F) 144.9 144.9 848.4 HEATING 931, 113 SUPERHEAT ING S ECT I 14

STEAP FLCH RATE: 38942.0 LBM/HR.

4.4 IN H20 GAS-SIJE PRESSURE ORCP:

PINCH POINT: 71.5 F

SYSTEP FEFF CPHANCE

SUBJENSER PRESSURE: 4.08 IN HG SERVE TURNINE EFFICIENT 10.85 HH HEATER PRESSURE: 15.0 PSTA LHV OF FUEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: STEAM TURBINE SHARE OF THE LOAD: 23.0 PERCENT STEAM THREINE HORS EPONER: 4804.9 TOTAL SYSTEM HIRSEPONER: 20873.6 GT HJF SEPOWERIREVISEDJ: 16068.7

PECIFIC F'EL CUNSJAPPION IL BM-FUEL / PP-HR.): GI ONLY: 0.436 COGAS: 0.335 GI AT SYSTEM HP: 0.396 FUEL CINSUAPTING (LBM-FUEL/HR.): GT DNLY: 69%9.8 COGAS: 6999.8

GT AT SYSTEM HP: 0.345 Cr 6451 0.412 THE SULL EFF I IEN Y:

GT AT SYSTEM IP: 8270.7

RUN #36(0)

WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

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PRAKE HORSEPOWER: 1684.0, APPROXIMATE CORRESPONDING SHIP SPEED: 9.0 KIS EXHALST GAS TEMPERATURE: 689.0 F EXHALST GAS FLUR RATE: 159731.0 LBP/HR (44.4 LEM/SEC)

HEAT EXCHANGER GENNETRY

CVERFIL CIMENSIONS: EL-NGTH: 12-0 FT. MICTF: 15-0 FT. heiGHT: 15-0 FT.

STATE SURFACE. 1.0 IN.
SLOE TUBE CLAWETER: 0.9 IN.
SECTION CLAWETER: 0.9 IN.
FIN PAPEL CEREBIT SCHENIED
FIN PAPEL SCHENIED
FIN FAILURES: 0.024 IN. **hEAT**

TRANSVERSE TUBE SPACINGS 2.25 IN.

LENGITUGINAL TUBE SPACING: 1.95 IN.

NIMBER OF TUBES FER ROWS NUMBER OF ROWS PER PASS:

OUTSIDE AREA/PASS: 4081.2 SQ.FT. INSIDE AREA/PASS: 234.4 SQ. FT. TUBE LENGTH 12. FT.

FRENTAL AREA: 179.8 . SC. FT.

AUPBER OF PASSES: 9 (TOTAL)
ALATING SECTION:
2
80.1L.ING SECTION:
5.UPERHEATING SECTION:
5

LEGALING LENGTH- 1:7 FT:

HEAT EXCHANGER PERFORPANCE

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP, IN FLUID TEMP. OUT REYNOLDS NUMBER LAVG. 1 4365.1 33219.9 PEATING ROLLING SUPERFEATING SECTION

STEAM PRESSURE: 600.C PSIA (SATURATION FEMPERATURE 518.3 F)

GAS-SIDE PRESSURE DRCP: 0.5 IN H20 STEAM FLOA HATE: 7169.6 LBM/HR.

PINCE POLIT: 28.4 F

SYSTEP PEFFCRPANCE

CONDENSER PRESSURE: 4.08 IN PG FAM TORNINE FFICIENCY: 0.05 F FW HEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 B1L/10 ASSUMED SYSTEM CHARACTERISTICS: STEAM TUABINE SHARE OF THE LOAD! 38.6 PERCENT 1043.8 TOTAL SYSTEM HIRSEPONER: 2705.4 GT HORSEPOWERIREVISEDI: 1661.6 STEAP TUFBINE HORSEPCHER:

GT AT SYSTEM HP: 2372.3 SPECIFIC FUEL CONSUMPTION (LBN-FUEL/HP-HR): 67 AT SYSTEM HP: 0.877 FUEL CCNSLMPTICN ILEM-FUEL/HR. J: 1766.3

GT AT SYSTEP HP: 0.156

COGAS: 0.212

THERPAL EFFICIENCY:

RUN #35

WASTE HEAT RECOVERY UNIT DESIGN RUN

	SPEEDS	
	CORRESPONCING SHIP	1 91 .3 LBM/SEC 1
GAS TURBLAE	BRAKE HORSEPOWER : 8526.0, A PPROXIMATE CORRESPONCING SHIP SPEED:	ENAIST GAS FLOW RATE: 328641.0 LBM/HR
3		

16.0 KTS

	NUMBER OF REMS PER PASS : 1.	NUMBER OF TUBES PER ROW: 80.	TUBE LENGTH 12. FT.	OUTS IDE AREA/PASS: 4081.2 SQ.FT.	INSIDE AREA/PASS: 234.4 SO. FT.	FRONTAL AREA: 179.8 SC. FT.	NIPBER OF PASSES: 9 (TOTAL)	BOLLING SECTION: 4 (HEATING LENGTH 1.6 FT.)	SUPERHEALING SECTION: 4 FULLING LENGTH 5.5 FI.)
HEAT EACHANGER GEOMETRY		15.0 17.	3 5 5 113 13 13 13 14 14 14 14 14 14 14 14 14 14 14 14 14	COLUMN TON THE TANK TEN I . I . IN.	TUBE// NARANCE PENT:	FIN SPACING TIMES FINS IN.	111 THICKNESS: 0.024 IN.	TRANSVERSE TUBE SPACING: 2.25 IN.	IGAGITUDINAL TUBE : PACING: 1.95 IN.

HEAT EXCHANGER PERFCHPANCE	VCE.										
S ECT 11M	GAS TEN	P. 14	GAS T	ENP. (101	FLUID	TEMP.	Z	GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMPER (AVG.)	REYNOLDS NUMPER	I AV G.
HEAT ING BOTLING SUPERNEAT ING		~00	40.0	543.7		25.0	513.3		513. 518.3 645.0	11569.7	
STEAM PRESSURE: 800.0 PSIA (SATURATION TEMPERATURE. 518.3 F)	00.00 PSIA	(SATURA	11 CN	TEMPE	ATURE	. 518	.3 F	_			
STEAP FLCW FATE: 20426.0 LB4/IR.	20426.0 18	4/H.									
GAS-SIDE PRESSURE I'RUP: 1.7 IN H20	1.1 1.1	IN H20									
PINCE PCINT: 10.4 F											

ASSIMED SYSTEM CHARACTERISTICS	CONDENSER PRESSURE : 4.08	FW HEATER PRESSURE: 15.0	LHV OF FLEL: 18400 BTUY			
ASSI				184.0	5334.1	0.286
SYSTEP FEFF CFPANCE GT HOPSEPDWENTREVISED): 8391.1	STEAP TUREINE HORSEPCHER: 2706.8	TOTAL SYSTEM MINSED IMER: 11 098.0	STEAM LURBINE SHARE OF THE LOAD: 24.4 PERCENT	SPECIFIC FILE CONSIMPTION (LBN-FUEL/HP-HR):	FUEL C. 1504 PT 104 (LRM-FUEL/HR.): GT ONLY: 4-35.4 CO.AS: 4435.4 GT AT SYSTEM HP: 5334.1	THER WALE OF CALY: 3.462 COGAS: 0.346 GT AT SYSTEM HP: 0.28E

RUN #34(0)

WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

GAS TURBINE

12.13.115 11.67.21

ERAKE HTRSEPTHER: 16421.0, APPRIXIMATE CURRESPONDING SHIP SPEED: 20.0 KTS EXHALSI GAS TEPPEFATURE: 849.0 F EXHAUST GAS FLOW RATE: 407509.0 LBM/HR (113.2 LBP/SEC)

HEAT EXCHANGER GENETRY

OVERALL OLMENSIONS: LEWITH: 12.0 FT. WIGHT: 15.0 FT. HEIGHT: 15.9 FT.

MEAT TRANSFER SURFACE TOUR DIAMETER: 0.9 IN.
175 DID TOUR DIAMETER: 0.9 IN.
176 FIN ARRANGEERT:
FIN TRANSFER SCHENTED
FIN SPACING: 11.88 FINS/IN.
FIN HEIGHT: 0.5 IN.

LONGITUDINAL TUBE SPACING: 1.95 IN. TRANSVERSE FUBE SPICING: 2.25 IN.

NIMBER OF TLBES FER ROWS NUMBER OF ROMS PER PASS: TLBE LENGTH 12. FT.

OUTSIDE AREA/PASS: 4081.2 SO.FT.

INSIDE AREA/PASS: 234.4 SO. FT. FRONTAL AREA: 179.8 SC. FT.

(HEATING LENGTH- 1:9 FT.) NLPEER OF PASSES: 9 (TOTAL)
HEATING SECTION:
8011 NG SECTION: 5
SUPERHEATING SECTION: 1

HEAT EXCHANGER PERFUNPANCE

GAS TEMP. IN GAS TEMP. DUT FLUID TEMF. IN FLUID TEMP. DUT REYNOLDS MUMER (AVG.) HEATING BOIL ING SLPERHEATING SECTION

154754.6

STEAM PRESSURE: 800.0 PSIA ISATURATION TEMPERATURE. 518.3 F)

STEAP FLC& RATE: 36836.9 LBM/HR.

2.5 IN H20 GAS-SIDE PRESSURE DROP: FINCH PUINT: 64.5 F

SYSTEM FERFCREAMCE

STEAM TURBLINE HURSEPCHERS 4838.2 GT HORSEPOWERIREVISED1: 16132.9

ONDENSER PRESSURE: 4.CE IN. HG SFEW TURBINE EFFICIENCY: 0.85 FW HEATER PRESSURE: 15.0 PSIA LIVO OF FUEL: 18400 BTULES

ASSLMED SYSTEP CHARACTERISTICS:

SPECIFIC FUEL CUASUMFILON (LBM-FUEL/HP-HR):
GT OF SYSTEM HP: 0.394
CUGAS: 0.334
GT AT SYSTEM HP: 0.394 STEP THREINE SHARE OF THE LADS 23,1 PERCENT

TCTAL SYSTEM HORSEPOWER: 20971.1

GT AT SYSTEM HPS FLEL CUNSUPPTION (LBP-FUEL/HR-): 008.6

GT AT SYSTEP HP: 0.351 THERPAL EFFICIENCY: COCAS: 0.414

94.15.51 91.25/80

RUN #42(0)

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MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

GAS TURBINE

FRANK PERSEPOWEN: 1684.0, APPRIXINATE CORRESPONDING SHIP SPEED: 9.0 K1S
ENALS 34S TEMPERATURE: 689.0 F
EXPAUST GAS FLIM PATE: 159731.0 LBMAIR (44.4 LBP/SEC)

HEAT EXCENICES CENTERY

QVERALL ULMENSLUNS: FT. LEATH: 12.0 FT. WICTH: 15.2 FT. HE LG:11: 3.4 FT.

IN SPACE SECRENTED IN SPACE IN

LUNGITLDINAL TUBE SPACING: 2.92 IN. TRANSVERSE TUSE SPACING: 3.38 IN.

NUMBER OF TUBES PER ROWS NUMBER OF ROWS PER PASS:

TLEE LENGTH 12. FT.

DUTSIDE AREA/PASS: 4132.2 SQ.FT. INSIDE AREA/PASS: 237.3 SQ. FT. FRONTAL AREA: 181.9 SC. FT.

NUPBER CF PASSES: 14 (TOTAL)
HEATING SECTION: 4
BOLLING SECTION: 6
SUPERHEATING SECTION: 4

(POIL ING LENGTH 4.5 FT.)

MEAT EXCHANGER PERF CREANCE

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMPER (AVG.) 6.06.8 6.06.8 6.88.6 ROILING SUPERFEATING S ECT 139

STEAM PRESSURE: 600.0 PSIA ISATURATION TEMPERATURE +86.3 F)

STEAP FLEW FATE: 8814.4 1.04/18.

0.6 IN H20 GAS-SIDE PRESSURE UNCPE PINCE PCINT: 14.9 F

SYSTEP FEFF CAPANCE

GT HTF SEPTAERIREVISEDI: 1661.0

STEAP TURBLAE HORSEPCHER: 1164.2 TUTAL SYSTEM MINSEPOWER: 2825.2

0000E45ER PRESSURE: 408 IN HG TEAH TURBINE EFFICIENT: 0.85 WHEATER PRESSURE: 15.0 PSIA HV OF FLEL: 18400 BTU/LRM

ASSUMED SYSTEM CHARACTERISTICS:

SPECIFIC FUEL CONSTINETION ILBM-FUEL/MP-MRT: GT AT SYSTEM HP: 0.860

STEAM TUABLINE SHARE OF THE LUADS 41.2 PERCENT

GT AT SYSTEM Nº: 2429.7 FILE CTYSHPOTION (LBM-FUEL/HP.):

GT AT SYSTEM HP: COGAS: 0.221 THERMAL EFFICIENCY:

RUN #41(0)

66/25/75 15.06.16

WASTE HEAT RECOVERY UNIT OFF-DESIGN RLN

GAS TLABINE

BRAKE HURSEPOLER: 8526.0, APPROXIPATE CORRESPONCING SHIP SPEEC: 16.0 KTS EXFAUST (AS TEMPERATURE: 742.0 F EDIALST GAS FLUR RATE: 328641.0 LBP/HP (91.3 LBM/SEC)

HEAT EXCHANGER GECHETRY

CVERALL CLYENSINS: LENGTH: 12.0 FT. MIDTH: 15.2 FT. HELGHT: 3.4 FT.

FIN TYPE: SEGNENTED FINS/IN-FIN PEACHES . 7.92 FINS/IN-FIN FELCENESS: 0.036 IN-1.4 1N. MEAT TRANSFER SUPFACE CITSIDE TUBE CLAMINISTUSE DIAM

LONGITUCTIAL TUNE SPACING: 2.92 IN. TRANSVERSE THRE SPACING: 3.38 IN.

NUMBER OF TUBES PER ROWS NUMBER OF REMS FER FASS: TUBE LENGTH 12. FT. INSIDE AREA/PASS: 237.3 SC. FT. FFENTAL AREA: 181.9 SQ. FT.

OUTSIDE AREA/PASS: 4132.2 SQ.FT.

(HEATING LENGTH 3.7 FT.) NUMBER OF PASSES: 14 (TOTAL)
HEATING SECTION: 4
BUILING SECTION: 3
SUPERFEATING SECTION: 3

HEAT EXCHANGER PERFURMANCE

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) PET 116 BCILING SUPE PHEATING SEC TI CN

96788.1

STEAP PRESSURE: 630.0 PSIA (SATURATION TEMPERATURE 486.3 F)

STEAM FLOW RATE: 21626.8 LBM MR.

GAS-SIJE PRESSURE CRCP: 2.4 IN H20

PINCE PRINT: 30.5 F

SYSTEM PERFERMANCE

COLDENSER PRESSURE: 4.00 IN HG STEAM TURBINE EFFICIENCY: 0.855 FW HEATER PRESSURE: 15.0 PSIA LHV CF FUEL: 18400 PTULE ASSUMED SYSTEM CHARACTERISTICS: STEAM TURBINE HUP SEP JWER : 2918.0 GT HCRSEPONERIREVISEDI: 8379.2

STEAM TLABINE SHARE OF THE LCAD: 25.8 PERCENT TOTAL SYSTEM HORSEPONER: 11297.2

SPECIFIC FUEL CONSUMPTION (LAN-FUEL /HP-HA): SYSTEM HP: FUEL CONSUMPTION ILBM-FUEL /HR-1:

0.285 GT AT SYSTEM HP: CDGAS: 0.352 THERMAL EFF IS IENS Y:

GT AT SYSTEM HP: 5399.6

RUN #40

MASTE HEAT RECOVERY UNIT DESIGN RUN

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	SPEEL	
	SHIP	SEC.)
	DING	184/
	CURRESPOR	EXPANSI (AS FLOW ATTE: 407589.0 LBM/HR (113.2 LBM/SEC)
	DXIMATE	LBM/HR
	J. APPR	0.585.0
	16421	11 E: 4
	POWER	FLONER
NE	E MCRS	13. TS
EAS TURBIN	BR AK	EXF
EAS		

20.0 KTS

	EATED S LIM AND 40/208-0 107-1 113-2 109/2501	
HEA	HEAT EXCHANGEN GETMETRY	
	OVERALL UL PENSIGNS:	NUMBER OF ROMS PER PASS: 1.
	MOTH: 15.2 FT.	NUMBER OF TUBES PER ROW: 54.
	יון איני וויינים אינים איני	TLBE LENGTH 12. FT.
	MAN STORY SUNTAINER TO STORY IS IN.	OLISIDE AREA/PASS: 4132.2 SQ.FT.
	TUBELL NARANGE HENTS	INSIGE AREA/PASS: 237.3 SQ. FT.
	FIN SPACING: 7.92 FINS/ IN.	FRONTAL AREA: 181.9 SQ. FT.
	FIA TAICANESS: 0.036 IN.	NUMBER OF PASSESS 14 (TOTAL)
	TRANSVERSE TUBE SFACING: 3.38 IN.	PUBLISH SECTION: 7 CHEATING LE
	LONGITUDINAL TUBE SPACING: 2.92 IN.	מתנצעונים זכרו זמוי כ ומודרו חף דו

ENGTH- 5.7 FT.

SECTION JAS TEMP. IN GAS TEMP, DUT FLUID TEMF. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) HEATING 731.5 \$13.4 \$60.3 \$467.5 \$20574.3 SUPERFERTING 850.6 \$737.5 \$486.3 \$650.0 \$179758.0 STEAM PRESSURE: 39093.2 LBM/RR. GAS-SIDE PRESSURE DRCP: 3.5 IN H20 PIACH PCINT: 45.8 F		REYNOLUS NUMBER (AVS.)	20574.3					
TION TION TING ERFEATING SLRE: 300.0 FATE: 3969 AESSURE DROP		FLUID TEMP. OUT	467.6 650.03					
TION TION TING ERFEATING SLRE: 300.0 FATE: 3969 AESSURE DROP		FLUID TENE. IN	200.00 467.59 486.33	E. 486.3 F1				
TION TION TING ERFEATING SLRE: 300.0 FATE: 3969 AESSURE DROP		GAS TEMP. DUT	513.4	RATICN TEMPERATUR		20		
SECTION HEATING HOLLING STEAM PRESSURE: 57EAP FLUW FATE: 645-510E PRESSURE PINCH PUNT: 45.	1,1	GAS TEMP. IN		UU.O PSIA ISATU	39693.2 LBM/IR.	URCP: 3.5 IN H		
	EALMANGER PERFURE	SECTION	HEATING BOIL ING SUPERFEAT IN	STEAM PRESSURES	STEAP FLEW FATE:	GAS-SIDE PRESSURE	PINCH PCINT: 45.	

ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP1 8237.9 GT AT SYSTEM HP: 0.357 STEAM TURNINE SHARE OF THE LOADS 24.3 PERCENT SPECIFIC FILE CONSUMPTION ILEN-FUEL/NP-HRIS GI AT SYSTEM NPS 0.387 FUEL CHSUMPT DM 1LBM-FUEL/HP. 1: GT dMLY: 7004.3 COGAS: 7004.3 THER WAL EFF ISTERY: COGAS: 0.420 STEAM FUREINE HORS EPCHERE 5167.7 TOTAL SYSTEM MASEDOWERS 21265.2 GT HORSEPINEMIREVISEDII 161 01.5 SYSTEP FEFF CPPANCE

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RUN #42(0)

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WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

		1:1 1:1
	<u>.</u> .	NUMBER OF TAXABLE SECTION: 3 (BOILING LENGTH= 4-1 FT.) SUPERFEATING SECTION: 3 (BOILING LENGTH= 1.8 FT.)
	NUMBER OF ROWS PER PASS: 1. NUMER OF TUBES PER ROW: 54. TLBE LENGTH 12. F1. OLTSIDE AREA/PASS: 4132.2 SC.FT. INSIDE AREA/PASS: 237.3 SQ. FT.	SECTION:
K IS	12. 16. PE	ATECT
	OF ROOF TO THE AREA. AREA.	PERT
SPEED	NUMBER OF ROWS PER PASS NUMER OF TUBES PER RE TLBE LENGTH 12. FT. OLTSIDE AREA/PASS: 41 INSIDE AREA/PASS: 23 FRONTAL AREA: 181.5	Y I SO
RRESPONDING SHIP		
BRAKE HCRSEPOWER: 1684.0, APPRIXIMATE CORRESPONDING SHIP SPEED: 9.0 KTS E MHAUST GAS TEMPÉRATURE: 689.0 F EXFAUST GAS FLIM RATE: 159731.0 LBM/HR (44.4 LBP/SEC)	DVERALL DIMENSIONS: DVERALL LEVIGHT 12.05 FT. LEVIGHT 12.0 FT. HEAT TRANSIET SUPFREE: 1.5 IN. TOPE FIN AT ANGER 11.5 IN. FIN SPACING: SCNEYTED. FIN SPACING: SCNEYTED. FIN SPACING: SCNEYTED.	TRANSVERSE TURE SPACING: 3.36 IN.
	4	

	GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER IAVG.)	4552.9				
	FLUID TEMP. DUT	4174.4 661.3				
	FLUID TEMP. IN	200.0	E= 486.3 F)			
	IN GAS TEMP, DUT	435.0 498.1 639.4	STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE= 486.3 F)	H.	IN H20	
	GAS TEMP.	639.4	O PSIA I	3685.4 LBM/HR.	9.0 :4:	
HEAT EXCHANGER PERFORMATCE	SECTION	BOLLING BOLLING SUPERHEATING	STEAM PRESSURE: 600.	STEAM FLOW RATE: 86	GAS-SIDE PRESSURE DRCP: 0.6 IN H2D	PINCE POINT: 24.3 F

ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 2418.4 GT AT SYSTEM HP: 0.160 SPECIFIC FUEL CONSUMPTION (LEM-FIEL/AP-HR): 61 AT SYSTEM MP: 0.863 STEAM TURNINE SHARE OF THE LOADS 40.7 PERCENT FUEL CCASUMETION ILEM-FUEL FAR. 1: 166.2 COGAS: 0.219 STEAM TURBINE HIRSEPOWER: 1140.0 TOTAL SYSTEM HORSEPONER: 2801.3 GT HORSEPOWERIREVISED): 1661.3 THESPAL EFFICIENCY: SYSTEM PERFORMANCE

RUN #41

27 W W W W

MASTE HEAT RECOVERY UNIT DESIGN RUN

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BRAKE HORSEPOWER: 8226.0. APPROXIMATE CURRESPONDING SHIP SPEED: 16.0 KTS EXFAUST 645 TEMPERATURE: 742.0 F EXHALST 645 FLOW RAFE: 328641.0 LBW/HR (91.3 LBW/SEC)

HEAT EACHANGER GECHETER

NUMBER OF RCMS FER FASS: 1.

NUMBER OF TUBES PER ROW: 54.

TUBE LENGTH 12. FT.

OLTSIDE AREA/PASS: 4132.2 SQ.FT.

INSIDE AREA/PASS: 237.3 SQ. FT.

FPCNTAL AREA: 181.9 SQ. FT.

NUMBER OF PASSES: 12 (TOTAL)

NUMBER OF PASSES: 12 (TOTAL)

SUPERFEATING SECTION: 2 (BOIL

(BOILING LENGTH: 2.3 FT.)

MEAT EXCLANGER PERFORMATCE

LONGITUDINAL TURE SPACINGS 2.92 IN.

FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER LAVS.) 97271.8 STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE= 486.3 F) GAS TEMP. DUT GAS TEMP. IN STEAM FLUE RATE: 21894.0 LBP/MR. BCILING BCILING SLPERHEATING SECTION

EAS-SIJE FRESSURE CROP: 2.0 IN HZD PINCH PINT: 31.6 F

SYSTEM PEPF DRMANCE

CONCENSER PRESSUPE: 4,08 IN. MG STEAM TURBINE EFFICIENCY: 0,85 FW HEAFR PRESSURE: 15.0 PSIA LHV CF FUEL: 18400 BTU/LBM A SSUMED SYSTEM CHARACTERISTICS : STEAP TUPBINE SHARE OF THE LOAD! 25.2 PERCENT STEAM TURYINE HURSEPCHER: 2832.3 TOTAL SYSTEM HORSEPCHERE 11217-8 ET PERSECUENTREVISELIS B385.5

SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HR): AT SYSTEM HP: 0.475
FLEL CONSUPTION (LBP-FUEL/HR.):
6 CONSUPTION (LBP-FUEL/HR.):
6 CONSUPTION (LBP-FUEL/HR.):

HERPAL EFFICIENCY: COLAS: 0.350 GT AT SYSTEM HP: 0.289

RUN #40(0)

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MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

LRBINE RAKE HORSEPOWER: EXHALST GAS TEMPE EXHALST GAS TEMPE		ARAKE HORSEPOWERS 16421. U. APPROXIMATE CURRESPONDING SHIP SPEEDS	KAIE: 40/589.0 LBP/HR (119.2 LPP/SEC)
	GAS TLRBINE	FEMANS HORSEPOWER 1 16421.0. APPROXI	EAHALSI WAS FLUE KAIE! 407589.0 LB

IP SPEED: 20.0 KTS	NUMBER OF ROWS PER PASS: 1. NUMBER OF TUBES PER ROW: 54. TUBE LENGTH 12. FT. OUTSIDE AREA/PASS: 237.3 SQ.FT. INSIDE AREA/PASS: 237.3 SQ.FT. FRUMAL AREA: 181.9 SQ.FT. NUMBER OF PASSES: 12 (TOTAL) HEATING SECTION: 2 (BOIL
ARAKE HOBSEPOWER: 14421.0. APPROXIMATE CURRESPONDING SHIP SPEED: 20.0 KTS EXHAUST GAS TEMERATURE: 407589.0 LBP/HP (113.2 LBP/SEC)	CVENTLE LIMENSIONS: FINE LENGTH: 12.0 FT. HICTP: 12.0 FT. HISTORIAN TONE OLA WEER: 1.4 IN. TOUGHER IN. FINE PELLOT SECHENTED FINE PEL

0TAL)	(TOTAL) (HEATING LENGTH-	(TOTAL) (HEATING LENGTH-	(TOTAL) 4 HEATING LENGTH- ION: 2 (BOILING LENGTH-		
OTAL) HEATING LENGTH:	(TOTAL) (HEATING LENGTH-	(TOTAL) (HEATING LENGTH-	(TOTAL) 4 HEATING LENGTH- ION: 2 (BOILING LENGTH-		FF.:
FOTAL) 4: 2 (HEATING LENGTH=	(TOTAL)	(TOTAL)	(TOTAL)		2.5
0TAL)	(TOTAL)	(TOTAL)	(TOTAL)		LENGTH.
10TAL)	CTION: 2	ICN: ION: SECTION: 2	SECTION: 6		HEATING BOILING
	- é	12 C 10N: 10N: SECT 10	SECTION:	LOTAL	, ;
PASSES: ING SECTION RHEATING SE	PASSES NG SECT NG SECT RHEAT ING	NA NA		5	PEL
NUPRER OF PASSES: 12 HEATING SECTION: BOTLING SECTION: SUPERHEATING SECT	CF PASSES: EATING SECT DILING SECT	EATING DILING PERHEA	PAN PAN	3	SES

	REYNCLDS NUPRER (AVG.)	19625.8				
	FLUID TEMP. OUT	4460.6 647.3				
	FLUID TEMF. IN	460.0 460.6 460.6	E= 486.3 F1			
	GAS TEMP. IN GAS TEMP. OUT FLUID TEMF. IN FLUID TEMP. OUT	\$22.8 730.7	ATURATION TEMPERATUR	٨.	N H20	
HEAT EXCHANGER PERFURPANCE	SECTION GAS TEMP. 1	HEATING 522.8 ROILING 730.7 SUFERHEATING 850.0	STEAM PRESSURE: 600.0 PSIA ISATURATION TEMPERATURE +86.3 F)	STEAM FLEW RATE: 38266.0 LBM/HR.	GAS-SIDE PRESSURE DROP: 3.0 IN H20	FINCE FCINI: 62.2 F
HEA 1						

	ASSUMED SYSTEM CHARACTERISTICS:	CONDENSER PRESSURE: 4.CE IN. HG	FW HEATER PRESSURE: 15.0 PSIA	LHV OF FUEL: 18400 810/18M			
	ASS				0.392	1.6528	0.353
				PERCENT	GT AT SYSTEM HP:	GT AT SYSTEM HP:	GT AT SYSTEM HP:
SYSTEP PEPFCHPANCE	GT HORSEPOWERIREVISEDI: 16116.8	STEAM TLABINE HURSEPCHER: 4972.8	TOTAL SYSTEM HORSEPOWER: 21089.7	STEAM TURBINE SHARE OF THE LOAD: 23.6 PERCENT	SPECIFIC FUEL CONSUMFTION (LBM-FJEL/MP-HR): 6.392 GT AT SYSTEM MP: 0.392	FUEL CCASUPPTICN (LBM-FUEL/HR.): 3T JNLY: 7066.4 COGAS: 7006.4 GT AT SYSTEM MP: 8259.7	Therefe efficiency: COGAS: 0.416 GT AT SYSTEM HP: 0.353

RUN #54(0)

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

	101 9.0	
	SPE	
	SHIP	SECI
	ND ING	181
	CJARESPO	++++
	APPRD X I MATE	EXPANST GAS FLOW RATE: 159731.0 LAM/HR (44.4 LBP/SEC)
	1084.0.	ATE: 15973
	EPOWER:	S FLOW A
NA.	E PCHS	UST GA
CAS TURBIN	FRAK	EXFA
3		

K 15

	NUMBER OF ROMS PER PASS:	NIMBER OF TLBES PER ROW: 80.	TLBE LENGTH 12. FT.	ER: 1.0 I.N. OUTSIDE AREA/PASS: 4081.2 SO.FT.	INSIDE AREA/PASS: 234.4 SO. FT.	1.48 FINS/IN. FRONTAL AREA: 179.6 SO. FT.		INS: 2-25 IN. HEATING SECTION: 2 (HEATING LENGTH 3-8 FT.)
HEAT EXCLANGER GETHETPY		15.00 FT	STANGE STANGE TO SE	OUTSIDE TON DIAMETER: 1.0 IN.	TUBERFINANCEPERTS	AN SPACINGS IN SECTION OF SECTION	Fir Thick less: 0.024	TRANSVERSE TURE SPACINGS 2.2

	REYNOLDS NUMBER LAVG. 1	4683.4				
	FLUID TEMP. DUT	6425 6614.6				
OR PANCE	GAS TEMP. IN GAS TEMP. DUT FLUID TEMF. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.)		STEAM PRESSURE: 400.6 PSIA (SATURATION TEMPERATURE= 444.6 F)	STEAP FLEW RATE: 9609.1 LBM/HR.	GAS-SIDE PRESSURE DROP: 0.4 IN H20	35.8 F
HEAT EXCHANGER PERFORMANCE	SECTEIN	HEATING ROLL 1 1G SUFERNEATING	STEAM PRESSURE	STEAP FLCH HATE	GAS-SIDE PRESSI	PINCE FCINT: 35.8 F

ASSUMED SYSTEM CHARACTERISTICS:	CONDENSER PRESSURES 4,08 IN. HG	FW HEATER PRESSURE: 15.0 PSIA	LHV UF FUEL: 18400 810/18M			
ASS				0.853	2452.6	0.162
				HP:	ě.	4
			_	SYSTEM	SYSTEM	SYSTEM
			RCEN	7	4	¥
			PE	₹5	5	5
	17.5	4.2	SFEAM TURSTINE SHARE OF THE LOADS 42.2 PERCENT	SPECIFIC FILE CONSUMPTION IL BY-FJEL/HP-HR): 1 UNLY: 1.063 COGAS: 0.615 GT AT SYSTEM HP: 0.853	FUEL CONSUMPTION IL BM-FJEL/HR.): GT AT SYSTEM HP: 2452.6	THERMAL EFFICIENCY: COGAS: 0.225 GT AT SYSTEM PP: 0.162
1991	7	287	104	AS:	NS.	AS 8
	ER:	R .	THE	200	400	200
GT HOP SEPOWERIRE VISEDI: 1661.7	STEAP THEBINE HOPSEPCHERE 1212.5	TOTAL SYSTEM HIRSEPONERS 2874.2	SHARE OF	CONSUMPT 1. C63	1766.3	EVC 1:
MERI	SINE	F. P	INE	HEEL.	Y:Y	3
SEP	1116	SYSI	108	CNL	SNO	L CAL
GT HOF	STEAD	TOTAL	SFEAM	SPECIE	FUELG	THERM

SYSTEP PENFCRMANCE

RUN #53

WASTE HEAT RECOVERY UNIT DESIGN RLN

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2
CAS
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WAKE HYRSEPOWER: 1 856.0, APPROXIMATE CORRESPONDING SHIP SPEED: 16.0 KTS Examine 63 Temberilye: 328646,0 1847HR (91.3 1847SEC) Examine: 45 Flum Rate: 328646,0 1847HR (91.3 1847SEC)

HEAT EXCHANGER GEOMETRY

HEAT TRANSFER SUPERCE FINESTIC CHRE DIANETER: 0.9 IN. THASTIC CHRE DIANETER: 0.9 IN. THASTIC CHRE DIANETER: 0.9 IN. FIN TYPE: SEMENTED FIN TYPE: SEMENTED FIN THE CHRE DIANETERS TRAISVEYSE TUBE SPICING: 2.25 IN. 00 tet 01 46:05 10 15:0 FT. HID HA: 15:0 FT. FELCEFF: 15:0 FT.

(HEAT ING LENGTH 0.3 FT.) DLTSIDE AREA/PASS: 4081.2 SQ.FT. INSIDE AREA/PASS: 234.4 SO. FT. NUMBER OF PASSES: 9 (19141)
HEATING SECTION: 4
BOILLING SECTION: 4
SUP ERHEATING SECTION: 2 FRONTAL AREA: 179.8 SO. FT. NUMBER OF TUBES PER ROWS NUMBER CF RCMS PER PASS: TURE LENGTH 12. FT.

HEAT EXCHAIGER PERFORMANCE

LONGITULINAL TUSE SPACING: 1.95 IN.

FLUID TEMP. IN FLLID TEMP. OUT REYNOLDS AUPRER (AVG.) STEAM PRESSURE: 430.0 PSIA (SATURATION TEMPERATURE. 444.6 F) GAS TEMP. DUT CAS-SIJE "YESSUKE GROPE 1.6 IN H20 GAS TEMP. IN STEAM FLUE MATE: 23698.0 LBM/HR. HEATTYG BY II FIG St.Pc Adeatt NS SECTION

115150.3

SYSTEM FEFF CAMPICE

PINCH PCINT: 30.9 F

CONCENSER PRESSURE: 4.08 IN BGS CONCENSER IN BRAILE FFICIENCY: 0.85 FFICIENCY: 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM ASSUMED SYSTEM CHARACTERISTICS: SPECIFIC FUEL CHISJMPTION (LAM-FUEL /HP-HR): CALY: 0.529 CULAS: 0.392 GT 4T SYSTEM HP: GT AT SYSTEM PP: STEAP TURBINE SHARE OF THE LOAD: 25.8 PERCENT FIR CTISHAPT ITH (LBM-FUEL/HR-1: 6:35.6 STEAM TURBINE HIR SEP JMER! 2913.9 TUTAL SYSTEM HOR SEPONERE 11306.5 LT HORSEPOWERINEVISEDIE 8392.6 THEADY EFFT IETEY:

GT AT SYSTEM HP:

COUAS: 0.352

RUN #52(o)

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

	20.	
	EEDS	
	SP	
	H	-
	6 5	/SE
	S	L BH
	PON	7
	BRAKE HORSEPONER : 16421.0. APPROXIMATE CORRESPONDING SHIP SPEED:	113.
	3	_
	MATE	WH/
	X	9
	PPR	20
		583
	0:	3
	1642	E S
		3
	MER	Ś
	SEP	S
	HO.	و. د
I VE	A.	Y S
TUR	88	E
GAS TUREIN		

.0 KTS

	•			FT.	•			CHEATING LENGTH 0.9 FT. 1	CONTENT TEMPINE 3.4 LI.
	NUMBER OF RCMS PER PASS: 1.	NUMBER OF TUBES PER ROWS 80.	TUBE LENGTH 12. FT.	OUTSIDE AREA/PASS: 4081.2 SQ.FT.	INSIDE AREA/PASS: 234.4 SQ. FT.	FRENTAL AREF: 179.8 SQ. FT.	NUMBER OF PASSESS 9 (TOTAL)	BOLLING SECTION:	SUPERFEATING SECTION : A
HEAT EXCHANGER GECHETHY	OVERALL CIMENSIONS:	FIGURE 15.0 FT	HEAT TOANSES CHUESCE	CUTSIDE TORE DIAMETER: 1.0 IN.	TUBELF IN AD ANGESTRATE	FIN SPACING II.88 FINS/IN.	FIN THICKNESS: 0.024 IN.	THANSVERSE THEE SPACINGS 2.25 IN.	LONGITUDINAL TUBE SPACINGS 1.95 IN.

	REYNOLDS NUMBER (AVG.)	18992.1				
	FLUID TEMP. DUT	444.6 690.0				
	FLUID TEMP. IN	439.0	. 444.6 FJ			
EMFORMANCE	ION GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.)	6(1L14) 501.4 501.4 501.4 501.4 501.4 501.4 501.4 501.4 501.4 50.8 50.8 50.8 50.8 50.8 50.8 50.8	STEAM PRESSURE: 400.0 PS IA (SATURATION TEMPERATURE- 444.6 F)	STEAM FLOW RATE: 38C86.5 LUM/HR.	GAS-SIDE FRESSURE CROP: 2.5 IN H20	PINCH POINT: 62.4 F
HEAT EXCLANGER PERFORMANCE	SECTION	SCAL	STEAM PRESS	STEAM FLOW	CAS-STUE FRE	PINCH POINT

A SSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEP HP: 8265.1 GT AT SYSTEM HP1 0.352 SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HR):
6T ANLY: 0.434 C3GAS: 0.334 GT AT SYSTEM HP: 0.393 STEAP TUFBINE SHARE OF THE LOAD: 23.2 PERCENT FLEL CUASUPPILICA (LBP-FUEL/HR.): GT 74LY: 7008.9 COGAS: 7008.9 CUCAS: 0.415 STEAM TURBINE HORSEPCHER: 4880.7 TOTAL SYSTEP HORSEPCHER: 21016.3 GT PERSEFCUERIREVISECI: 16135.3 THERMAL EFFICIENCY: SYSTEM PERFORMANCE

MASTE HEAT RECEVERY UNIT CFF-DESIGN RUN

CAS TURBINE

11P SPEED: 9.0 KTS	NUMBER OF RCWS PER PASS: 1. NUMPER OF TUBES PER ROW: 54. TLBE LENGTH 12. FT. OLTSIDE AREA/PASS: 4132.2 SC.FT. INSIDE AREA/PASS: 237.3 SC. FT. FROWTAL AREA: 181.9 SO. FT. NUMBER OF PASSES: 12 (TOTAL) HEATING SECTION: 6 (HFATING LENGTH# 4-1 FT.) SUPERHEATING SECTION: 6 (HFATING LENGTH# 1.7 FT.)
ERAKE HORSEPOVER: 1684.0, APPROXIMATE CORRESPONDING SHIP SPEED: 9.0 KTS Exhaust Gas temperature: 689.0 F Exhaust Gas flum gate: 159731.0 ERM/HR (44.4 LBM/SEC)	HEAT EXCHANGE GEOMETRY OVERALL CHAFASIDAS: 15.0 FT. 15.0 FT. 15.1 FT. HEAT TAYSEE'S SUFFICE THIST CHAFASIDA CHAFTER: 15.1 IN. 15.1 FT. 16.1 FT. 16

HEA	T EXCH	HEAT EXCHANGER PERFUNMANCE	A VC E											
		SECTION	GA S	TE MP	=	GAS	TEMP.	TOO	FLU ID	TEMP.	Z	GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER LANG.	REYNOLDS NUMBER	(AVG.
		BCILENS SUPERHEATING	2	639.4			435.0		4470	474.4		486.3	4552.9	
	STEAP	STEAP PRESSURE: 630.0 PSIA (SATURATION TEMPERATURE= 486.3 F)	9 0.009	VI S	IS ATUR	AT ION	TEMPE	RATURE	+ 486	.3 F.				
	STEAM	STEAM FLOA RATE: 6685.4 LBM AHR.	6685.4	1841	HR.									
	6A 5- 5	GAS-SIUE PRESSURE CRCP: 0.6 IN H20	CRCP:	9.0	IN HZ	0					•			
	P INC P	PINCE PAINT: 24.3 F	. J F											

ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP : 2418.5 0.160 SPECIFIC FIEL CHIS MPT TON (LBM-FUEL /HP-HB): GT AT SYSTEM HP: 0.863 GT AT SYSTEM HP: STEAM FURBINE SHARE OF THE LOAD: 40.7 PERCENT FUEL CTYSUMPT INV LLBM-FUEL VHR. 1: 766.2 CUGAS: 0.219 STEAM TURBINE HORSEPONER: 1141.0 TOTAL SYSTEM HJRSEPOWER: 2802.3 GT HORSEPOWERIREVISEDI: 1661.3 THERM'L CFF IC IENCY: SYSTEM PERFURMANCE

C# 14.74 14.34.30

WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

GAS TURBINE

THE FIRST DAS TEMPERATURE: 1895.0, APPROXIMATE CORRESPONDING SHIP SPEED: 10.0 KTS

HENT EXCHANGER GEUMETRY

CVLHALL ULMENSLINS: FT. LENGTH: 12.C FT. HIDTH: 15.2 FT. hELCHT: 2.9 FT.

LONGITUDINAL TURE SPACING: 2.92 IN. TRANSVERSE TUBE SFACINGS 3.38 IN.

54. NUMBER OF TUBES PER ROW: NUMBER OF ROMS PER PASS :

TUBE LENGTH 12. FT.

NUTSI DE AREA/PASS: 4132.2 50.FT. INSIDE AREA /PASS: 237.3 SQ. FT.

FRONTAL AKEA: 181.9 SC. FT.

HEATING LENGTH- 2:4 FT. NUMFER OF PASSES: 12 (TOTAL)
HEATING SECTION:
3
SUPERHEATING SECTION: 3

HEAT EXCHANGER PERFURMANCE

SECTION

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNDLDS NUMBER (AVG.) 4.0389.B 631.5

STEAM PRESSURE: 630.0 PSIA (SATURATION TEMPERATURE# 486.3 F) HEATING ROILING SUPERHEATING

STEAM FLIM HATE: 9084.8 1947HR.

GAS-SIDE PRESSURE UKCP: 0.6 IN H20 FINCE POLITE 25.3 F

SYSTEM PERFORMANCE

STEAM TURBINE HOWSEPCWER: 1191.3 TOTAL SYSTEM HURSEPOWER: 306C.6 GT HORSE POWERIREVISEDIE 1869.2

CONDENSER PRESSURE: 4.08 IN HC STEAM TURBINE EFFICENCY: 0.85 FW HER PRESSURE: 15.0 PSIA LHV OF FLEL: 18400 BTU/LBM

ASSUMED SYSTEM CHARACTERISTICS:

SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HR): 0.829 GT AT SYSTEM HP: 0.829 STEAM TURBINE SHARE OF THE LOAD: 38.9 PERCENT

GT AT SYSTEM IP! FUEL CALY: 1915.7 - COGAS: 1910.7

GT AT SYSTEM HP: 0.167 THEY MALE FOR ICIENTY: COGAS: 0.222

(8/16/19 12.50.27

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

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GAS TUREINE

ВААКЕ НЈАSEPJWER 1 3150.0. APPROXIMATE CORRESPONDING SHIP SPEED: 12.0 KTS Kataust Gas Temperature: 1669.0 F Ephalsi Gas Flüm Ratie: 221990.0 LBW/HR 1 62.2 LBM/SEC)

HEAT EXCHANSER GECHETRY

OVERALL CIMENSINS: LENGTH: 12.0 FT. MIDTH: 15.2 FT. HEIGHT: 2.9 FT.

TRANSFER SURFACE
COST LOWER LIMETER: 1.5 IN.
1.015 JE THUB LIMETER: 0.00 J HEAT

LONGITUDITAL TURE SPACINGS 2.92 IN. 3.36 IN. TRANSVERSE THUE SPACINGS

NUMBER OF TUBES PER ROW: NLMBER OF ROWS PER PASS:

OUTSIDE AREA/PASS: 4132.2 SO.FT. INSIDE AREA/PASS: 237.3 SQ. FT. TUBE LENGTH 12. FT.

FRANTAL AREA: 181.9 SO. FT.

(BOILING LENGTH 3.1 FT.) NUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION:
3
BOILLING SECTION: 6
SUPERFEATING SECTION: 3

HEAT EXCHANGER PERFORMATICE

FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) GAS TEMP. DUT GAS TEMP. IN BCILING SCPERHEATING SEC TION

STEAM FRESSURE: 630.0 PS IA (SATURATION TEMPERATURE. 486.3 F) 439.5 501.8 627.0

54035.3

STEAM FLOW RATE: 12028.9 LBMAIR.

GAS-SIUE PRESSURE CRCP: 1.0 IN H20 PINCE PINT: 29.9 F

SYSTEM PERFORMANCE

CONDENSER PRESSURE: 4.08 IN HI STEAM TURBINE EFFICENCY: 0.85 THOUSE PRESSURE: 15.0 PSIA LHV GF FUEL: 18400 BTU/LBM A SSUMED SYSTEM CHARACTERISTICS: STEAM TURBINE HOR SEPCHER: 1568.9 TOTAL SYSTEP HORSEPONER: 4681.2 CT PERSEFEWERINEVISEES 3112.3

SPECIFIC FUEL CURSUMPTION (LBM-+UEL/HP-HR):
CT 74LY: 0.824 C76AS: 0.551 GT AT SYSTEM HP: 0.672 STEAM TUBBINE SHANE CF THE LOAC: 33.5 PERCENT

GT AT SYSTEM HP: 3143.8 FLEL CONSUMETION ALB" FUEL YHR. 1: 577.1

GT AT SYSTEM HP: 0.206 COGAS: 0.251 THEF OF SEFFICIENCY:

CB.116.75 15.47.C7

WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

GAS TURBINE

HOAKE FORSEPJHER: 4316.0, AFPROXIMATE CORRESPONDING SHIP SPEEC: 13.0 KTS EXFAIST EAS TEMPERATURE: 2699.0 F EAHAIST GAS FLOW RATE: 262546.0 LBW/HR (72.9 LBM/SEC)

HEAT EXCHANGER GEOMETRY

CVERALL CIMENSIONS:
LENGTH: 12.0 FT.
MIDIM: 15.2 FT.
h. Lohf: 2.9 FT.

PEAT TRANSFER SUFFICE

OUTSIDE THUS DIAMETER: 1.4 IN.
THUSELFIT DAR ALGERERITE
FIN TORE: SEGMENTED
FIN TORE: SEGMENTED
FIN SPACING: 0.92 FINS/IN.
FIN THICKNESS: 0.036 IN.

LCAGITUDIVAL TUBE SPACING: 2.92 IN. TRANSVERSE TUBE SPACING: 3.38 IN.

(HEATING LENGTH= 5.1 FT.) OLTSIDE AREA/PASS: 4132.2 SQ.FT. INSIDE AREA/PASS : 237.3 SC. FT. NIMBER OF PASSES: 12 (TOTAL)
HEATING SECTION:
301LING SECTION:
50PERFEATING SECTION:
3 FRONTAL AREA: 181.9 SQ. FT. NUMBER OF TUBES PER ROW: NLMBER OF ROWS PER PASS : TUBE LENGTH 12. FT.

HEAT EXCHANGES PERFORMANCE

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE= 486.3 F) \$02.1 \$20.5 GAS-SIJE PRESSURE GROP: 1.3 IN H20 STEAM FLEW RATE: 14806.4 LBM/HR. 620.6 699.3 PINCE FCINT: 35.2 F FEAT ING ROTE ING SUFERHEAT ING SEC FLON

7675.4 67796.6

SYSTEP PEFFCREAMCE

ASSUMED SYSTEM CHARACTERISTICS: SPECIFIC FLEL CONSUMFTION ILBM-FJELCHP-HRI: 67 AT SYSTEM HP: 0.589 STEAM FURBINE SHARE OF THE LOAD: 31.2 PERCENT STEAP TUFBINE HORSEPCWER: 1924.2 TOTAL SYSTEM HIRSEPOLERE 6175.0 GT HOP SEPONER (REVISED): 4250.8

CONDENSER PRESSURE: 4.00 IN. HG FM HETER PRESSURE: 0.0510 LHV OF FUEL: 18400 BTU/EM

GT AT SYSTEM HP: 3639.4 GT AT SYSTEM HP: FUEL CONSUMPTION (LBW-FJEL/H9.); GT JALY: 3018.3 COGAS: 3018.3 COGAS: 0.283 THERMAL LEFFICIETORS

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

HRYKE HTRSIPTHER! 5474.0, APPROXIMATE CORRESPONDING SHIP SPEED: 14.0 KTS EXPAIST GAS TEMPERATURE! 709.0 F EXHAIST GAS FLOW BATE! 279070.0 LBW/HR 177.5 LBW/SEC! GAS TURBIAE

;

OLISIDE AREA/PASS: 4132.2 SQ.FT. INSIDE AREA/PASS: 237.3 SC. FT. FRONTAL AREA: 181.5 SO. FT. NUMBER OF TUBES PER ROWS NUMBER OF ROWS PER PASS: TURE LENGTH 12. FT. TRANSFER SUFFICE

CLISTON TO BE DIAMETER: 1.5 IN.
195 DIAMETER: 1.4 IN.
195 DIAMETER: 1.5 IN.
196 FIN TOFF SCHOOL TO BE THE SPACE TO BE THE SPACE TO BE THE SPACE TO BE THE STANSFER THE STANSFER THE STANSFER THE SPACE THE SPACE THE STANSFER THE SPACE THE S LENGITUDINAL TURE SPACING: 2.92 IN. CVERAL EINENSINNS: TENDINS: H. 12.0 FT. H. 15.2 FT. FEICHT: 2.9 FT. HEAT EXCHANGER GEUMETRY

(HEATING LENGTH= 5.2 FT.) NUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION: 3
SUPERFERTING SECTION: 3

FLJID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) 74819.9 STEAP FRESSLRE: 600.0 PS IA (SATURATION TEMPERATURE 486.3 F) GAS TEMP. IN GAS TEMP. OUT GAS-SIDE PRESSURE DRCP: 1.5 IN H20 STEAM FLOW RATE: 16381.9 LAMMR. PINCE PINT: 36.7 F FEAT ING BCILING SUPERIFATING HEAT EXCEANGES PERFORMENCE NC 11 335

CONDENSER PRESSURE: 4.00 IN STEAN YORINE EFFICIENCY: 0. THE MEATER PRESSURE: 15.0 LHV OF FUEL: 18400 BTULEN ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 4100.7 GT AT SYSTEM HP 1 0.254 SPECIFIC FUEL CONSUMPTION ILBM-FUEL /HP-HR13 STEAM TLABING SHARE OF THE LOADS 28.4 PERCENT FILE CONSUMPTION (LRM-FUEL/HR-1: 3404.5 COGAS: 0.306 STEAM TURBINE HORSEPOWER: 2140.5 INTAL SYSTEM HORSEPONER: 7530.0 GT HORSE FChERINEVISEDIS 5389.5 THERMAL EFF ICIENCY: SYSTEM PEFFORMANCE

MASTE HEAT RECOVERY UNIT CFF-DESIGN RUN

GAS TUREINE

(B) ILLING LENGTH 2.4 FT.) OUTSIDE AREA/PASS: 4132.2 SO.FT. INS 10E AREA/PASS: 237.3 SQ. FT. NUMBER OF PASSES: 12 . (TOTAL)
HEATING SECTION: 4
BOILING SECTION: 6
SUPERHEATING SECTION: 2 FRONTAL AREA: 181.5 SO. FT. NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS: TUBE LENGTH 12. FT. BRAKE HOMSE POWER: 6947.0, APPROXIMATE CORRESPONCING SHIP SPEED: 15.0 KTS EXFLIST GAS TEMPERATURE: 733.0 F EXFAUST CAS FLOW RATE: 312118.0 LBM/HR (86.7 LBM/SEC) CE 108E CIAPETER: 1.4 IN.
FIN YOR SEATURED
FIN SPACING: 7.92 FINS/IN.
FIN FINCESS: 3.036 IN. LONGITUDINAL TUBE SPACING: 2.92 IN. TRANSVERSE TUBE SPACING: 3.38 IN. HEAT TRAUSE SUPPOCE TO THE STATER ! Tyerall DIMENSIONS: LENGTH: 12.0 FT. NJ 14: 15.2 FT. HEIGHT: 2.5 FT. HEAT EXCHANGES GECHETRY

FLUID TEMP. IN FLLID TEMP. OUT REYNOLDS NUMPER (AVG.) 10757.3 89617.3 STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE 486.3 F) GAS TEMP. DUT 513.8 673.4 GAS-SIDE PRESSURE DROP: 1.8 IN H20 GAS TEMP. IN STEAM FLCM RATE: 20172.7 LBM/HR. PINCH PCINT: 28.8 F HEAT EXCHANGER PERFORMANCE PETTING PETTING SEPERIFATING SECTION

CONDENSER PRESSURE: 4.08 IN HG STRAM TURBINE EFFICIENCY: 0.05 FM HEATER PRESSURE: 15.0 PSIA LIV OF FIEL: 18400 BTU/LBM A SSUMED SYSTEM CHARACTERISTICS: 0.505 GT AT SYSTEM HP: 0.274 SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HR):
61 77LY: 0.553 GT AT SYSTEM HP: STEAP TURBINE SHARE OF THE LOADS 27.6 PERCENT FLEL CJASLMPTION (48P-FIEL/HR.): 3892.0 CUGAS: 0.335 STEAM TURHINE HJR SEPCHER: 2604.9 TUTAL SYSTEM HORSEPONER: 9440.0 6835.2 GT HERSEFCHERIREV IS EC 1: THERPAL EFFICIENCY: SYSTEM PERFORMANCE

MASTE HEAT RECOVERY UNIT DESIGN RUN

D: 16.0 KTS	NUMBER OF RCWS FER PASS: 1. NUMPER OF TUBES PER ROW: 54. TUBE LENGTH 12. FT. OLTSIDE AREA/PASS: 4132.2 SO.FT. INSIDE AREA/PASS: 237.3 SQ. FT. FRONTAL AREA: 181.9 SQ. FT. NUMBER OF PASSES: 12 (TOTAL) BOILING SECTION: 2 (BOILING LENGTH. SUPERFEATING SECTION: 2 (BOILING LENGTH.	IN FLUID TEMP, DUT REWNOLDS NUMBER (AVG.) 484.4 486.3 641.3 97271.8	ASSUMED SYSTEM CHARACTERISTICS: CONDENSER PRESSURE: 4.08 IN # HG STEM TURBINE EFFICIENCY: 0.85 A FW HEATER PRESSURE: 15.0 PSIA LHV CF FUEL: 18400 BTU/LBM 3.6 85
IIP SPEE(NLM NUM TUBS TUBS TUBS FRC	FLUID TEMP. IN 200.0 484.4 486.3 = 486.3 F)	6.4
SPONDING SI		OUT FLUI	T SYSTEM HP: SYSTEM HP: SYSTEM HP:
E CORRE		435.0 435.0 516.2 683.2 ON TEMPE	PERCEN HRI 1 GT AT GT AT
GAS TURRINE PRAKE HORSEPUMER: 8526.0, APPROXIMATE CORRESPONDING SHIP SPEED: 16.0 EXALUST GAS TEMPERATURE: 742.0 F EXTAUST (AS FLOW RATE: 528641.0 LBM/HR 1 91.3 LBM/SEC)	CVERAL EMEYSTONS: LENDIN: 12.0 FILENIN: 12.2 FILENIN: 12.3 FIL	HEAT EXCLANGER PEHFORMAICE SECTION GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. FATHER STATES 516.0 435.0 486.3 STEAM PHESSIER: 5.00.0 PS 14 (SATURATION TEMPERATURE 486.3 F) STEAM FLOW RATE: 21894.0 LBM/HR. EAS-SIDE FRESSURE EROP: 2.0 IN H20	SYSTEM PEPFNANNICE GT HCFSEFCHERINEVISE(1: 8385.5 STEAM TURAINE HONSEPOWER: 2832.3 TUTAL SYSTEM HONSEPOWER: 11217.8 STEAM TURAINE SHIRE OF THE LOAD: 25.2 PENCENT SPECIFIC FUEL CONSUMPTION (1804-FUEL/HP-HR): FUEL CONLY: 0.52.9 THERMAL EFFICIE: 4.34.8 THERMAL EFFICIE: COLOS: 0.350 GT ONLY: 0.221 COLOS: 0.350 GT ONLY: 0.221 COLOS: 0.350 GT ONLY: 0.221

2.5 FT. }

WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

ERME FOR EPINER: 10421.0, APPRIXIMATE CORRESPONDING SHIP SPEED: 17.0 KTS EXHALS GAS TEMPERATURE: 786.0 F EXFAUST GAS FLOW RATE: 350673.0 LBM/HR (97.4 LBM/SEC) GAS TURBINE

NI TRANSFER SURFACE
INCISIONE TUBE DIAMETER: 1.5 IN.
INCISIONE CLAREFER: 1.4 IN.
INCISIONE CLAREFER: 1.4 IN.
INCISIONE CLAREFER: 1.4 IN.
INCISIONE CLAREFER: 1.5 IN.
FIN TYPE: 56 GMENTED
FIN SPECIALS: 7.92 FINS/ IN.
FIN HELOMIS 0.8 IN. OVERALL DIMENSIONS: FT. LEGGHI: 12.0 FT. WIDTH: 15.2 FT. HE IGHI: 2.9 FT. HEAT EXCLANGER GETMETRY

(NEATING LENGTH 3.5 FT.) OUTSIDE AREA/PASS: 4132.2 SO.FT. INS 10E AREA/PASS: . 237.3 50. FT. NUMBER OF PASSES: 12 (TOTAL)
HEATING SECTION: 4
NOTEING SECTION: 6
SUPERHEATING SECTION: 2 FRONTAL AREA: 181.9 SO. FT. NIMBER OF TUBES PER RONS NUMBER OF ROWS PER PASS: TLBE LENGTH 12. FT.

HEAT EXCHANGER PERFORMANCE

FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) 14414.3 123750.3 STEAM PRESSUMES 600.0 PSIA (SATURATION TEMPERATURE. 486.3 FI GAS TEMP. IN GAS TEMP. DUT 425.0 516.6 636.5 HEATING BAILING SEPERFEATING S ECT 10N

SYSTEM PERFCREANCE

2.3 IN H20

STEAM FLOD RATE: 27527.7 LBM/HR.

GAS-SIDE PRESSURE DROPE

PINCH PCINTS 43.5 F

A SSUMED SYSTEM CHARACTERISTICS: SPECIFIC FUEL CCASUMFTION ILBM-FJEL/AP-HRJ: 67 AT SYSTEM HP: 0.449 STEAM TURBINE SHARE OF THE LOAD! 25.8 PERCENT FILE CCASLMETICN (LPT-FILEL/FR. 1: 5088.5 STEAP TLABINE HCFSEPCHER: 3564.3 TOTAL SYSTEM HORSEPOWER: 15408-1 CT HORSEPOWER (REVISED): 10243.8

CONDENSER PRESSURE: 4.06 [N. HK STEAM TURNINE EFFICENCY: 0.85 HM HA TER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 BTU/LBM

0.308

GT AT SYSTEM HP: GT AT SYSTEM HPS

COUAS: 0.375

THERPAL LEFTIC IENCY:

LONGITUDINAL TUBE SPACING: 2.92 IN.

TRANSVERSE TLAE SPACING: 3.38 IN.

WASTE HEAT RECOVERY UNIT OFF-DESIGN RLN

GAS TURBINE

	•	21 33				
	SS: 1. ROW: 54. 4132.2 SO.FT.	37.3 SG. FT. SG. FT. (TOTAL) (HEATING LENGTH= 4.4 FT.) TICN: 2 (ENILING LENGTH= 4.2 FT.)				
DING SHIP SPEED: 18.0 KTS Lep/Seci	NUMBER OF ROWS PER PASS: 1. NUMBER OF TUBES PER ROW: 54. TUBE LENGTH 12. FT.	INSIDE AREA/PASS: 237.3 SG. FT. FRONTAL AREA: 181.9 SG. FT. NUPBER OF PASSES: 12 (TOTAL) HEATING SECTION: SUPERFEATING SECTION: SUPERFEATING SECTION:				
RRAKE HUSEPINER: 12105-0, APPROXIMATE CORRESPONDING SHIP SPEED: 18.0 KTS Exhaust Gas temperature: 809.0 f BP/HR (106.1 LEP/SEC) Exhaust Gas flow Rate: 381885.0 LBP/HR (106.1 LEP/SEC)	CVERALL CHENSIONS: CVERALL CHENSIONS: LEVERAL STORMS: LEVERAL STORMS:	TISSION TUBE CLAMPERS: 1.4 IN. TUBECTI ATANUENTI: SEGMENTED FIN TRAILING: 0.92 FINS/IN. FIN THICKNESS: 0.036 IN. TRANSVERSE TUBE SFACING: 3.38 IN.	HEAT EACTINGER PERFURMANCE			

IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) 468-1 16677-8 462.0 145423.7					A SSUMED SYSTEM CHARACTERISTICS:	CONDENSER PRESSURE: 4.08 IN MG EL LA TERBINE EFFICIENCY: 0.85	LHV CF FUEL: 18400 RTU/LBM			
1D TEMP. 200.0 468.1 486.3	486.3 FI				A SSU			0.431	6.9169	0.321
CAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN 7519-1 423-0 519-1 468-1 108-4 486-3	RATURE.							YSTEM HP :	YSTEM HP:	YSTEP HPE
423.0 519.1 705.8	ON TEMPE						PERCENT	HRI S	GT AT S	GT AT S
2	(SATURATI	IN H20			9.	1.84	0: 25.9	-FUE L/HP.	1,5640.5	0, 193
5 19.1 105.8	D PSIA	3: 2.6			1: 11889	WER: 41	F THE LOA	TION LLBH	-FUEL AIR.	COGAS
SECTION FEATING ACLING SCPERIEATING	STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE 486.3 F)	GAS-SIDE PRESSURE DKOP: 2.6 IN H2D	PINCH PCINTS 51.0 F	SYSTEM PERFORMANCE	GT HERSEFOWERIREV IS ECH: 11889.6	STEAM (URRINE HORSEPOWER: 4148.1	STEAM THERINE SHARE OF THE LOAD: 25.9 PERCENT	SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HR): CT CALY: 0.414 CACAS: 0.352 GT AT SYSTEM HP: 0.431	FUEL COTSUMPTION (LBM-FUEL ANR.): GT TMLY: 5640.5 CJG4S: 5640.5 GT AT SYSTEM MP: 6916.9	THERPAL EFFICIENCY: COGAS: 0.393 GT AT SYSTEP HP: 0.321
				Š						

MASTE HEAT RECCYERY UNIT OFF-CESIGN RUN

GAS TURRINE

- The Market Pa

	• :	NLPBER OF PASSES 12 (TOTAL) HEATING SECTION: 6 (HEATING LENGTH= 4.7 FT.) SUPERHEATING SECTION: 2 (BCILING LENGTH= 4.3 FT.)
OF ROMS PER PASS: 1. OF TUBES PER ROW: 54.	AREA/PASS: 4132.2 SQ.I AREA/PASS: 237.3 SQ.F.	OF PASSES : (TOTAL) ATING SECTION: 6 ILING SECTION: 6 IPERHEATING SECTION: 2
NUMPER	OUTSIDE INSIDE	NLFBE RES
NEAT EXCENDER GENEEPPY OVERALL DIMENSIONS: FT. WELCH: 15.2 FT. HELGH: 2.9 FT.	HEAT TRANSFER SUPFACE CLESTON TO THE TREE 1.5 IN. INSTITUTE CLARETER: 1.4 IN. INSTITUTE TO A SHANDENENT: THE TRANSFER TO THE T	FIN THICKNESS: 0.036 IN. FANSYERSE TUBE SPACING: 3.38 IN. LONGINGINAL TUBE SPACING: 2.92 IN.
	FT. NUMBER OF ROMS PER PASS: FT. NUMBER OF TUBES PER ROW: FT.	FT: FT: FT: NUMBER OF ROWS PER PASS: FT: FT: NUMBER OF TUBES PER ROW: TUBE LENGTH 12. FT. TUBE LENGTH 12. FT. OUTSIDE AREA/PASS: 4132.2 LUMBERT: 1.4 IN. SECHNIS REA/PASS: 237.3 S. SECHNIS REA/PASS: 237.3 S.

REYNOLDS NUPPER (AVG.)	17400.5					
REYNOLDS						
F. 001	200					
GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMF. OUT	466.3 486.3 640.0					
MP. IN	omm	2				
FLUID TE	200.0 466.3 486.3	. 486.3				
out.		ERATURE				
TEMP.	\$19.9 519.9 712.1	N TEMPE				
GAS		URATIO		н20		
2	0-2	(SA T	RATE: 33631.7 LBM/HR.	Z		
15	519.9 712.1 819.2	VIS	87 /	2.1		
		0.0	1631.	10P :	•	
ER FURMANCE ION	ING ING REEAT ING	103	. 33	RE JA	53.7	
SECTION	HENTING BOIL ING SLPERNEA	STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE. 486.3 FI	FLC RATE	GAS-SIJE PRESSURE JROP: 2.7 IN H2D	FINCH POINT: 53.7 F	30 man 20 30 man 30 30 man 30 30 30 30 30 30 30 30 30 30 30 30 30
HEAT EXCHANGER P		STEAM	STEAM FLCS	545-SI.	FINCH	20 30
-		•				21.0

A SSUMED SYSTEM CHARACTERISTICS: 7566.7 0.327 SPECIFIC FUEL CENSUMFILON (LBM-FJEL/PP-HR): SYSTEM HP: 0.423 GT AT SYSTEM HP: GT AT SYSTEM HP: STEAM TURBLUE SHARE OF THE LOAD: 24.3 PERCENT FIJEL CCASLPETTICN JLEN-FIJELY NO STORY COUAS: 0.401 STEAM TURBINE HOPSEFCHER: 4346.7 TOTAL SYSTEM HURS EPOWER: 11889.2 LT HEFSEPOWERIREVISEDI: 13542.5 THER OF CALVE U. 304

MASTE HEAT RECOVERY UNIT OFF-DESIGN RLN

	20
	47
	•
	===
	BRAKE HIRSEPINES: 16421.0. APPR EXHAUST GAS TEMPERATURE: 849.0
	PINER
	T GAS
GAS TLABINE	EX HAUS
CAS	

ROXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS EMALST GAS FLOW RATE: 407589.0 [BP/HR (113.2 18P/SEC) CVERALL GIMENSIONS: LENSTH: 12-C W 10Th: 15-2 HEIGHT: 2-9 HEAT EXCHANGER GEOMETRY

(HEATING LENGTH= 5.5 FT.) OUTSIDE AREA/PASS: 4132.2 SQ.FT. INSIDE AREA/PASS: 237.3 SO. FT. NUMBER OF PASSES: 12 · (TOTAL)
HEATING SECTION: 4
ROLLING SECTION: 2
SUPERHEATING SECTION: 2 F PCNTAL AREA: 181.9 SQ. FT. NUMBER OF TLBES PER ROWS NUMBER OF ROMS PER PASS : TUBE LENGTH 12. FT.

106 701 74 AMETER: 1.5 IN.
01 TORG JIMETR: 1.4 IN.
01 TORG JIMETR: 1.4 IN.
11 SAKANGENETTE
11 SPECIAL: SEGNENTED
11 SPECIAL: 0.93
11 INITIAL: 0.036 IN.

FEAT

HEAT EXCHANGER PERFORMANCE

LCALITUDINAL TUBE SPACING: 2.92 IN.

TRANSVERSE TUBE SFACING: 3.38 IN.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVG.) 19625.8 173910.7 STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE 486.3 F) GAS-SIDE PRESSURE DRCP: 3.0 IN H20 STEAM FLOA RATE: 38266.0 LBM MR. 522.8 730.7 849.8 FINCE POINT: 62.2 F BELLING SUPERFERTING SEC FLON

SYSTEM PEPFORMANCE

CCNDENSER PRESSURE: 4.08 IN HG STAM TURBINE EFFICIENCY: 0.85 FW HEATER PRESSURE: 15.0 PSTA LHV OF FLEL: 18400 BTU/L8M ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 8259.5 SPECIFIC FUEL CONSUMPTION (184-FUEL/HP-HR): SYSTEM HP: 0.392 STEAM TLABINE SHARE OF THE LCAD: 23.6 PERCENT FUEL COMSUMPTION (LBM-FUEL /HR.): 7006.4 COGAS: 0.416 STEAM TUMBINE HORSEPONER: 4968.3 TOTAL SYSTEM HORSEPONER: 21085.1 GT HCRSEFUNERIREVISEDI: 16116.8 THEP YAL EFF IC IENCY:

GT AT SYSTEM HP: 0.353

WESTE HEAT RECOVERY UNIT CFF-DESIGN RUN

** ** ** ** **

:

(15 TUREIN

POTATE TO SEPTIME TO SECOND APPROXIMATE CORRESPONDING SHIP SPEED: 21.5 KTS EXPENSE LAS PLAN FATE: 410630.3 LEMINE 11.2.4 LEMISES.

PERCENTAGE A DWG 1014

OUTSIDE AREA/PASS: 4132.2 50.FT. INSIDE ANEA PASSI. 237.3 SC. FT.

FFCNTAL AREA: 181.9 SC. FT.

-

ALMEER OF TLBES FEE ROWS NLMBER OF KOMS PER FASS:

TIEF LENGTE, 12. FT.

ALPPEQ OF PASSES: 12 (TOTAL)
HEATING SECTION:
SUPERFEATING SECTION: 2
SUPERFEATING SECTION: 2 CENSTRUCTURE THE PREPIUS 2.92 IN. RAMINERSE TUES JANG INGS 3.34 14.

(FETTING LENGTH: 5.3 FT.)

HEAT EACHWISE PERFORM CE

SECTION

GAS TEAP. I'S GAS TEMP, DUT FLUID TEME, IN FILLID TEME, CUT REVNCLOS ALMFER LAVG.) 24552.5 210054.9 545.8 756.4 255 SUBLINE INS

STRAT 2-FS JUTE: 630.0 PSIA (SATURATION TEMPERATURE 486.3 F) STEAM FLEE FATE: +5949.3 LBMZHR.

3.5 114 1123 GAS-SIJE A.FSSJAF JACO:

FINCE FURETE SO.3 F

SISTEM PEPE JAMANCE

ASSLINED SYSTEM CHAPACTERISTICS: STEAM THREINE SHANE OF THE LCAD: 23.3 PERCENT STEEL TORSING 41.5.PLAERS 5971.3 TATAL SESTEM HEREPERER: 25581.8 et persepertantister: 19613.5

CONTENSES FRESCUPF: 4.08 14
STEAN TURBINE FFF (LENCY: 0
FA HER NEW FRESCUPE: 15.0
HAV CF FUEL: 18400 FTU/LPH

SPECIFIC FULL STRUTTION (LAN-10LL/HP-11R); CALY: 3.41/ P.C.AS: 0.520 GI AT SYSTEM HOS FORL COTTENENT LEW-FORLANCES

GT AT SYSTEM HP: **** C16/5: 4.432 hite. W. Fridalish

GT AT SYSTEM HP:

C8/21/75 15.48.33

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUA

The state of the s

GAS TURBINE

5.0 KTS BRANE MERSEPCMENT 1684.0. APPROXIMATE CORRESPONCING SHIP SPEEDS EXPANSE (SETEMERATURE: 689.0 F EDHANTS GAS FLOW RATE: 159731.0 LBM/HR (44.4 LBM/SEC)

HEAT EXCHANGER GECHETRY

OVERALL DIVE 151705: LENG H: 12.1 NOTH: 12.1 HEIGHT: 3.2

HEAT TOWERE SUFFICE THE TISTERS LAST IN-TASIDE THE CLAMER IS LAST IN-TASIDE THE CLAMERY IS TASIDE THE SECRETED FIN TYPE SECRETED FIN TYPE SECRETED FIN TYPE SECRETED FIN THE CHARLES TOWERS THE

LENGITUE FIRE SP.C. ING: 2.92 IN. THAN "VERSE TIBE " PACING: 3.38 IN.

(BOILING LENGTH: 4.8 FT.) OLISIDE AREA/PASS: 3290.5 SO.FT. INSIDE AREA/PASS: 189.0 SO. FT. 43. FROMTAL AREA: 144.8 SO. FT. NUMBER OF TUBES PER ROWS TUBE LENGTH 12. FT.

NUMBER OF RCWS PER PASS:

NUMBER OF PASSES: 13 (TOTAL)
HEATING SECTION: 3
BOLLING SECTION: 4
SUPERFEATING SECTION: 4

HEAT EACHANGES PESFIRMANCE

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMBER (AVS.) 5643.0 49203.8 BCILING BCILING SLPF 2 HEATING SEC TI ON

STERM PRESCURE: 630.0 PSIA (SATUPATION TEMPERATURE 486.3 F) STEIM FLON RATE: B612.9 LBM/HR.

CAS-SIJE FRESSIRE CROPE 0.9 IN HZD PINCH PULMIT: 27.6 F

SYSTEM PEPEDRAMICE

A SSUMED SYSTEM CHARACTERISTICS: SP EC 1115 FUEL CURSUMPTION ILM FILEL/ HP-HRI: SYSTEM HP: STEAP THEBLAE SHARE OF THE LABOR 40.0 PERCENT STEAM FURBINE HORSEPOWER: 1135.5 INTAL SYSTEM HORSEPCHER: 2795.6 ET PERSEFE JERIREVISECH: 1660.1

CONDENSER PHESSURE: 4.08 IN. HI FILEM TURNING EFFILLENCY: 0.85 FILEM TATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 RTU/LAM

GT AT SYSTEM HP: 2415.7 FUEL (ONSUPETION ILB" - FUEL /HR. 1: 1765. 9 MERPEL EFFICIENCY:

CUGAS: 0.219

GT AT SYSTEM HP: 0.160

WASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

GAS TURRINE

NUMPER OF ROMS PER PASS : EMAKE HCESEPJMER: 1895.0, APPRIXIMATE CJRRESPONDING SHIP SPEED: 10.0 KIS EXHALSI GAS TEMPERATURE: 683.0 F EXFAUS: GAS FLIM CATE: 16703.0 LBM/MR (46.4 LBP/SEC) UVERALL DI MENSIONS: FIGURE 12.0 FT. HUTTH: 12.1 FT. HUTTH: 3.2 FT. HEAT THANSER SUMFACE OLISINE TUBE DIA INSTANTANCE TLALFIN ANAMOR HEAT EXCREIGES GEIMETRY

CHEATING LENGTH OUTSIDE AREA/PASS: 3290.5 SQ.FT. INSICE AREA/PASS: 189.0 SO. FT. NUMBER OF PASSES: 13 (TOTAL)
HEATING SECTION: 3
BOIL ING SECTION: 6
SUPERHEATING SECTION: 6 FPANTAL AREA: 144.8 SG. FT. NLYBER OF TLBES PER ROWS TLBE LENGTH 12. FT.

5.0 FT.

HEAT EXCHANSER PERFORPANCE

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS NUMPER (AVG.) 52032.4 MALLING MALLING MALLING SECTION

STEAM PRESSURE: 600.C PSIA (SATURATION TEMPERATURE= 486.3 F) STEAM FLEW HATE: 9055.2 LB4/HR.

GAS-SIDE PRESSURE DROP: 1.0 IN 120 FINCE FCIN: 29.0 F

SYSTEP FEFFCRMANCE

CONDENSER PRESSURE: 4.08 IN HG STEAM TURBINE EFFICIENCY: 0.855 FW HEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 RTU/LBM ASSUMED SYSTEM CHARACTEPISTICS: 0.829 SPECIFIC FIEL CONSIMPTION (LB4-FJEL/HP-HR): STEIN TUISINE SHARE OF THE LOAD: 39.0 PERCENT STEAP TUFUINE HIRSEPCHEN: 1193.8 TOTAL SYSTEM HIRSENGER: 3061.7 GT HITH SEPUMER (REVISED): 1867.8

2537.0 0.167 THEO WELL EFFECTE ILY:

285

GT AT SYSTEM HP! FIEL CTASHIPPLITY (LB4-FIELTH . 1: 1913.4

GT AT SYSTEM HP:

C1645: 0.222

TOTAL STANFACE 1.5 IN.

JUE TOR LANGE EF 1.4 IN.

JUE TOR LANGE EF 1.4 IN.

FIN ANGERENTE

FIN SPACIAL SECURITED

FIN FILE TO TOTAL

FIN FILE TO T

THANSVEHSE TUNE SPICINGS 3.34 IN.

LONGITLEINAL TUSE PACING: 2.92 IN.

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

GAS TUREINE

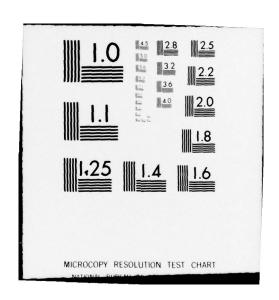
OLISIDE AREA/PASS: 3290.5 SQ.FT. INSIDE AREA/PASS: 189.0 SC. FT. NUMBER OF PASSES: 13- (TOTAL)
HEATING SECTION: 4
BOJLING SECTION: 6
SUPERHEATING SECTION: 3 FRONT AL AREA: 144.8 SQ. FT. NUMBER OF TUBES PER ROW: NUMBER OF ROMS PER PASS : TUBE LENGTH 12. FT. BY AKE HINSEPIMER: 2105.0, APPROXIMATE CORRESPONDING SHIP SPEED: 11.0 KTS EXFAUST (AS TEMPERITIRE: 689.0 F EXHALSI GAS FLOW RATE: 170747.0 LBW/HR (47.4 LBW/SEC) FIN 1772: "EGIETED FINS/IN-LONGITUDITIAL TUNE SPACING: 2.92 IN. TRAISVERSE THRE SPACING: 3.38 IN. PEAT TAYSFER SURFACE CVERAL CIAEISLINS: LENGTH: 12-0 MINIM: 12-1 FEIGFT: 3-2 HEAT EXCHANGER GEOMETRY

FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS HUMBER (AVS.) 6262.5 53336.6 STEAP FRESCURE: 600.0 PSIA (SATURATION TEMPERATURE= 486.3 F) GAS TEMP. IN GAS TEMP. DUT 1.0 IN H20 STEAM FLOW RITE: 9332.5 LBM/HR. GAS-SIDE PRESSIBLE ORCP: PINCH PUBLIE 15.4 F HEAT EXCREMEER PERFIR ANICE HEAT ING BELLING SLOTRHEATINS SEC TI UN

CONDENSER PRESSURF: 4.08 IN. HC STEAN TURBLINE FFFICENCY: 0.85 FW HEATER PRESSURE: 15.0 P STA LHV CF FUEL: 18400 BTU/LBM A SSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 2632.4 0.173 SPECIFIC FUEL CONSUMPTION (LBM-FUEL/HP-HR): CT PILY: 0.985 CRGAS: 0.622 GT AT SYSTEM HP: GT AT SYSTEP HP: STEAP TURBINE SHARE OF THE LAND: 36.8 PERCENT FUEL CAMSUMPTION (LBM-FUEL/HR.): 2042.8 COSAS: 0.222 STEEN TURBINE HOR SEPONER: 1210.6 TO TAL SYSTEM HUR EPOWER: 3285.3 207-17 GT HCRS EFUJERIREV L'ECH THER PAL EFFICIENCY: SYSTEM PERF INMANCE

(HEATING LENGTH= 0.3 FT.)

NAVAL POSTGRADUATE SCHOOL MONTEREY CA
WASTE HEAT RECOVERY UNIT DESIGN FOR GAS TURBINE PROPULSION SYST--ETC(U)
SEP 79 R M COMBS AD-A078 154 UNCLASSIFIED NL 4 of 4 ADA 078154 END DATE FILMED -80



WASTE HEAT RECOVERY UNIT OFF-DES ICH RUN

CAS TURBINE

K

OUTSICE AREA/PASS: 3290.5 SO.FT. INSTOE AREA /PASS: 189.0 SQ. FT. NUPBER CF PASSES: 13 (TOTAL)
HEATING SECTION:
3
SUPERHEATING SECTION:
3 FRONTAL AREA: 144.8 SC. FT. NUMBER OF TUBES PER ROWS NUMBER OF ROWS PER PASS! TLEE LENGTH 12. FT. FRAKE P.CF'S EPCMER: 3158.0. APPRIXIMATE CHRRESPONDING SHIP SPEED: 12.0 K15 EMHALST GAS TEMPERATURE: 683.0 F HHMR (62.2 LBW/SEC) HEAT THAN I ER SUFFACE CUTSING TURE DIA METER: 1.5 IN. TUSEFER ARRANGEMENT: 1.4 IN. TUSEFER SECHENTIA FIN SPET SECHNIED FIN SPET SECHNIED FIN HEIGHT 3.8 IN. OVERALL SIMENSIUMS: LEATH: 12.0 FT. KIGTH: 12.1 FT. HELGHI: 3.2 FT. HEAT EXCENICES GEMETEY

GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMF. OUT REYNOLDS NUMBER LAVG.) 7809.7 66615.3 STEAM PRESSURE: 600.0 PSIA (SATURATION TEMPERATURE# 486.3 F) 1.7 IN H20 STEAP FLEW FATE: 12305.2 LBW/HR. CAS-SIJE PRESSURE URDP: FINCH PCINT: 34.3 F HEAT EXCHANSER PENFORMANCE HEATING BOIL 116 CUPLATEATING S ECT 174

CONDENSER PRESSURE: 4.08 1% HG STEAN TURBLINE EFFICIENCY: 0.85 FW HEATER FRESSURE: 15.0 PSIA HHV OF FUEL: 18400 RTULLEN ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 0.20¢ SPECIFIC FUEL CONSIMPTION (LBM-FIEL/HP-HR):
CD:AS: CD:AS: 0.551 GT AT SYSTEM HP: 0.672 GT AT SYSTEM HP: STEIN TURBLINE SHARE OF THE LOAD! 33.6 PERCENT FUEL CCASUPE 15N 11 84-FUEL/FR . 1576.9 COGAS: 0.251 STEAP TUREINE HCHSEPCHER: 1572,9 TOTAL SYSTEM MOSEPOWER: 4680.8 3104.0 GT PARSEP SWERIREVISEDS: THER AL EFF ICIENTY: SYSTEP FEFFCHMANCE

LINGITUDINAL TUBE SPACING: 2.92 IN.

TPAYSVERSE TUBE SPICINGS 3.38 IN.

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CHEATING LENGTH-

CB127.75 14.14.13

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

PRINTER HIPSEPHIMER: 4316.0. APPRIXINATE CURRESPONDING SHIP SPEED: 13.0 KTS
EXISTES 645 TEMPERATURE: 262546.0 LBP/HR (72.9 LBP/SEC) GAS TLABINE

. 92 FINS/IN. FIN TYPE: "EUMENTED FINS/IN FIN FILMS TO 3 0.036 IN. TRANSVERSE TIME SPACINGS 3.34 IN. CVERALL CIMENS 1015: 1 LENGTH: 12.0 FT. HINTH: 12.1 FT. HEIGH: 3.2 FT. DUTSIDE TUBE DIAM HEAT EACHANGER GEOMFTRY HEAT

(HEATING LENGTH 5.2 FT.) DLTS1DE AREA/PASS: 3250.5 SO.FT. INSIDE AREA/PASS: 189.0 SC. FT. NUMBER OF PASSES: 13 (TOTAL)
HEATING SECTION: 7
SUPEPHEATING SECTION: 3 FRCHTAL ANEN: 144.8 SO. FT. NUMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS : TUBE LENGTH 12. FT.

FLJID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) 19304.0 STEAM PRESSURE: 600.0 PSIA ISALJRATION TEMPERATURE. 486.3 F) GAS TEMP. IN GAS TEMP. OUT HEAT EXCHANGES PERFORMATICE BCILING BCILING SIPETENT INS SECTION

GAS-SIDE PRESSURE DRCPs 2.3 IN H20 STEAM FLOW PATER 14403-9 LB4/HR. PINCE PILITE 39.3 F

FULL CHASUAPTION (LHM-FUEL/NR.): 3018.1 GT AT SYSTEM HP: 3628.2 SPECIFIC FUEL CHYSLAPTION (LB4-FUEL/HP-HR) 3 SYSTEM PP. STEAP TLASINE SHARE (F THE LOAD: 30.9 PERCENT 1899.0 TITAL SYSTEM HOP SEPOWER: 6141.5 GT HUF SEFONE AIREVISEUI: 4242.5 STEA" THREETE HIP SEPTWERS SYSTEM PERFORMANCE

GT AT SYSTEM HP # 0.234

COG15: 0.241

THEP WELL EFFICIENCY:

CONCENSER PRESCURE: 4.08 IN. HG STEAN TURSINE EFFICIENCY 0.055 FW AFFER PRESCURE: 15.0 PSIA LIY OF FEEL: 18400 BTU/LRM ASSUMED SYSTEM CHARACTERISTICS!

LONGITUDITIAL TUSE SPECINGS 2.92 IN.

WASTE HEAT RECOVERY UNIT CFF-DESIGN RUN

BRAKE HONSEPONER: 5474.3, AFPROXIMATE CORRESPONDING SHIP SPEED: 14.0 KTS AFILS GLY TEMPERATURE: 709.0 F EXFAUST GRY FLOW RATE: 279070.0 LBW/HR I 77.5 LBW/SE3) GAS TUREINE

HEAT TAANSE SUBFACE TO TO SHEEK 1.5 IN. INSTITUTE OF THE TO THE T OVER ALL DIMENSIONS FT. LENGTHS 12.0 FT. NO THE SECOND FT. NO THE HEAT EXCHANGES GECHETRY

NUMBER CF ROUS PER PASS:

I DESTING LENGTH 4.3 FT.) OLTSIDE AREA/PASS: 3290.5 SO.FT. INSIDE AREA/PASS: 189.0 SO. FT. NUMBER OF PASSES! 13 (TOTAL)
HEATING SECTION:
SUPERHEATING SECTION: FFONTAL AREA: 144.6 SO. FT. NUMBER OF TUBES PER ROWS TUBE LENGTH 12. FT.

GAS TEMP. IN GAS TEMP, DUT FLUID TEMP. IN FLUID TEMP. DUT REYNOLDS MUPPER LAVG. 1 STEAM PRESSULE: 600.0 PSIA ISATURATION TEMPERATURE 486.3 F) BOIL 16 SUPERHEATING SECTION

10756.5 92012.9

> GAS-SIDE PRESSURE UP TP: 2.4 IN H20 STEAM FLOW RATE: 16089.2 LBM/HR. PINCH PCINTE 25.9 F

ASSUMED SYSTEM CHARACTERISTICS : SPECIFIC FILE CGASTIFFTION ILBY-FUEL PP-HAIS SYSTEM HPS 0.546 STEAM TURBLIE SHARE OF THE LOADS 20.0 PERCENT FUEL CCNSCHPTION LLBP-HIEL/HR. 1: 404.2 STEAM TURBLAE HORSEPCHER: 2096.5 TOTAL SYSTEM HIRS EPHAERE 1475.4 CT HEPSEPTHEP IREVISEDI: 5378.9 SYSTEM PERFORMANCE

GT AT SYSTEM HP: 4081.8 GT AT SYSTEM HP: 0.253

COUAS: 0.304

THENPAL LEFT IC 16" 279

CONDENSER PRESSURE: 4,08 IN STEAM TOBBINE EFFICIENCY: 0. EM MEATER PRESSURE: 15,000 BTU/LOM

LOYGITUDITAL TURE SPACING: 2.92 IN.

HEAT EXCHINGER PERFORMANCE

TRAUSVERSE TUBE SOLC MSE 3.36 IN.

WASTE HEAT RECOVERY UNIT OFF-DESIGN RLN

GAS TLABINE

The state of the

OUTSIDE AREA/PASS: 3290.5 SO.FT. INSIDE AREA /PASS: 189.0 SQ. FT. NUMBER OF PASSES: 13 (TOTAL)
HEATING SECTION: 7
SUPERHEATING SECTION: 2 43. FRONTAL AREA: 144.8 SC. FT. NLMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS . TUBE LENGTH 12. FT. TEANSFEE STREAGE 15 IN.
OLTSIDE TUBE CLARFER 1.4 IN.
TUBELT ARENOVERENTED
FIT STREAM AND THE TOPE
FIT OVERALL CIMENSIONS: FT. WIDTH: 12.0 FT. HE INCHES 12.1 FT. HEAT EXCHANGES GEOMETRY HEAT

GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER LAVG.) 13259.6 109833.1 STEAM PRESSURE: COU.D PSIN (SATURATION TEMPERATURE. 486.3 F) GAS-SIJE PEESSIJAE DRIPE 3.0 IN H20 GAS TEMP. I'I STEAM FLCE RATE: 19968.0 LB"/HR. PINCH PCINT: 33.5 F FEATING BILL FIG SUPERHEATING SECTION

CONDENSER PRESSURE: 4.00 IN HG STEAM TURNINE EFFICIENCY: 0.055 FW HEAR PRESSURE: 15.0 PSIA LHV OF FUEL: 18400 RTULRA ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 4760.0 GT AT SYSTEM HP: 0.273 0.506 SPECIFIC FUEL CONSUMPTION (LBM-FIEL/PP-HR): SYSTEM MP: GT AT SYSTEM MP: STEAT TURBLUE SHARE OF THE LOADS 27.6 PERCENT FUEL C. JUSTING 118P-FUEL/HR. 1: 890. 8 COUAS: 0.335 STEAM TURBLAE HCRSEPCHER: 2594.9 9413.3 GT HIFSEPTHE IPENISFORE 6818.4 TETAL SYSTEM HOMSEPOWERS THENPAL EFFICIENCY: SYSTEM PERFURMANCE

LONGITUDINAL TUBE PREIMG: 2.92 IN.

HEAT EXCHANGER PEPFURMANCE

TRANSMEASE TUBE SFACINGS 3.39 IN.

(MEATING LENGTH= 2.3 FT.)

MASTE HEAT RECOVERY UNIT DESIGN RUN

2. 01.

PRINTED 185 EPIMED 1 6540.0, APPRIXIMATE CORRESPONDING SHIP SPEED: 16.0 KTS EXPILST GAS TEMPERATURE: 742.0 F WHITE (91.3 LBP/SEC) GAS TURBIAE

THANKER SUFFACE 11.5 IN.
OUTSIDE TUBE CLEATER: 1.4 IN.
ILBERTH ARE NUCEFIER 1.4 IN.
ILBERTH ARE NUCEFIER 1.9 INS. IN.
FIN STATES 3.0 3.036 IN. TRANSVERSE TUSE SUSCINGS 3.39 IN. CVERALL DIMENSIONS: FT. LENSTH: 12.6 FT. HISPFE 12.1 FT. HEAT EXCENDER GFOMETRY

(MEATING LENGTH- 3.5 FT.) OUTSIDE AMEA/PASS: 3290.5 SU.FT. INSIDE AREA # 155: 189.0 50. FT. NIPSER OF PASSES: 13 (TOTAL)
HEATING SECTION: 7
SUPERHEATING SECTION: 7
SUPERHEATING SECTION: 2 FRONTAL AREA: 144.8 SC. FT. NLMBER OF TUBES PER ROWS NUMBER OF ROMS PER PASS : TUBE LENGTH 12. FT.

GAS TEMP. IN GAS TEMP. DUT FLUID TEMF. IN FLUID TEMP. CUT REYNOLDS NUMBER IAVG.) 14512.9 122600.3 STEAM PRESSIFE: COU.C PSIA (SATURATION TEMPERATURE 486.3 F) 3.3 IN H20 STEAM FLOW RATE: 21999.0 LBM/HR. GAS-SIJE PRESSURE JUNP : PINCH POINTS 31.1 F HEAT EXCHANSER PERFCHMANCE HEATING BAIL ING SUPERFEAT ING SEC. 1 1'1

SYSTEM PERFURANCE

ASSUMED SYSTEM CHARACTERISTICS: SPECIFIC FUEL CONSUPETION (LBM-FJEL/PP-HR): SYSTEM HP: 0.479 STEAM TURBLUE SHIRE OF THE LOADS 25.3 PERCENT STEAM TURSINE HORSEPCHER: 2838.1 TOTAL SYSTEM HORSEPOWER: 11201.3 ET HIMSED IMED (4EVISED)1 8363.3

CONDENSER PRESSURE: 4.00 14 HG STEAM TURBINE EFFICIENCY: 0.085 FW HEATER PPESSL2E: 15.0 PSIA LINY OF FUEL: 18400 BTU/LBM

GT AT SYSTEM HP1 5368.2 FILE CENSING 101 JLB"-FILE / FP - 1: THEMPAL EFFICIENTY:

COUAS: 0.349

GT AT SYSTEM HP: 0.289

291

LONGITUDINAL TUBE PACING: 2.92 IN-

WASTE HEAT RECOVERY UNIT OFF-DESIGN RLN

BARNE HTGSEPTWER: 10421.0, APPROXIMATE CORNESPONDING SHIP SPEED: 17.0 KTS
EXHALST GAS TEMPLAFINE: 786.0 F
EMALST GAS FLOW RATE: 35.0673.0 LBP/HR # 97.4 LBP/SEC)
HEAT EXCPINGES GEOMETRY

GAS TLREINE

HEAT EXCPINGER GENMETRY

CVERALL DIMENSIONS:

LEGGIN: 12-0

MIDTH: 12-0

FT.

MEIGHT: 13-0

MIDTH: 13-0

MIDT

NUMBER OF ROWS PER PASS: 1.

NIMBER OF TUBES PER ROW: 43.

TUBE LENGTH 12. FT.

NUTSIDE AREA/PASS: 3250.5 SO.FT.

INSIDE AREA/PASS: 189.0 SC. FT.

FPONTAL AREA: 144.0 SC. FT.

NUMBER OF PASSES: 13 (TOTAL)

NUMBER OF SECTION: 7 (MEATING LENGTH: 5.7 FT.)

SUPERFREM ING SECTION: 7 (MEATING LENGTH: 3.5 FT.)

645 TEMP. IN GAS TEMP. DUT FLUID TEMF. IN FLUID TEMP. DUT REWOLDS NUMBER (AVG.) 103-5 425-0 463-8 466-3 466-3 635.0 155577.3

STEAP PRESSURE: 600.0 PSIA (SATURATION CEMPERATURE= 486.3 F) STEAF FLOA 94TE: 27527.7 LBM/AR.

STEAN FLAT BATE: 27221.7 LHW/HR.
GAS-SIDE PRESSURE DROP: 3.7 IN HZO
PINCE PILIT: 49.4 F

SYSTEP FEFFEPPANCE
GT HIPSEDIWENTRUISEUD: 10213.1
STEAP TUREINE HUPSEPCWER: 3544.8
TOTAL SYSTEM HIPSEPCWER: 13757.9

CONDENSER PRESSURE: 4.08 1N. MC STEAM TURBINE EFFICIENCY: 0.85 FW MFATER PRESSURE: 15.0 PSIA LIM OF FUEL: 18400 BTU/LEM

ASSUMED SYSTEM CHARACTERISTICS:

SPECIFIC FIEL CHASTMPT IN IL NY-FUEL/NP-HO 1: SPECIFIC FIEL CHASTMPT IN IL NY-FUEL/NP-HO 1: SYSTEM HP: 0.459

FILE CCASIMETEN (LEW-FILELYP -): GT AT SYSTEP HP: 6179.8 THER ME SELICIETY: 5045.2 COGAS: 5085.2 GT AT SYSTEP HP: 6179.8 THER ME STEPLY: 5.274 COGAS: 0.314 GT AT SYSTEM HP: 0.308

292

LONGITIOINAL TUBE : PACITIES 2.92 IN.

MEAT EXCHANGER PERFURPANCE

SECTION

SUPETING SUPETING

06/27/19 14.34.31

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

HAARE JORGEDOWER: 12105.). AFPROXIMATE CORRESPONDING SHIP SPEED: 10.0 KTS EXELUST GIS TEMPERITURE: 809.0 F MATH (104.1 LBM/SE)! EXHALST GAS FLOW HATE: 381885.0 LAM/HR (104.1 LBM/SE)! GAS TURRINE

PEAT TRIEFER SUPERING TO THE TRIEFER TRAISVERSE TUBE COVE PICE 3.38 IN. (1962-11, 21-18-12-10, FT. blo 11:1 12-10, FT. blo 11:1 12-1, FT. He I Gai: 3.2 FT. HEAT EXCHANGES GECHETRY

(BUILING LENGTH 4.3 FT.) DLTSIDE AREA/PASS: 3290.5 SQ.FT. INSIDE AREA/PASS: 189.0 SO. FT. 43. NEMBER OF PASSES! 13 (TOTAL)
HEATING SECTION:
5 UPERHEATING SECTION:
5 UPERHEATING SECTION:
5 : FP:INT & AREA: 144.8 SQ. FT. NIMBER OF TUBES PER ROWS NUMBER OF ROWS PER PASS: TUBE LENGTH 12. FT.

HEAT EXCHINGER PEPF 18 441F

LONGITURITY TUNE SPACING: 2.92 IN.

FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER LAVS.) 21363.3 181258.3 STEAM PRESSURE: A00.0 P. IA (SATURATION TEMPERATURE 486.3 F) LAS TEMP. IN GAS TEMP. DUT SUPFEMENTING SUPFEMENTING SECTION

STELL FL 34 0.1TE: 31836.1 L9HAR.

GAS-SICE PHESSURE DRCP: 4.3 IN H20 PINCE PARTE 44.2 F

SYSTEM FEMERAMINCE

CONCENSER PRESSURE: 4.06 IN HG STEAM TURNINE EFFICIENCY: 0.85 FW HEATER PRESSURE: 15.0 PSIA LIV OF FUEL: 18400 RUVLRM ASSUMED SYSTEM CHARACTERISTICS: GT 47 SYSTEM HP: 6884.0 0.432 SPLC IL IC TUEL CITTOM TON THE TO 1354 HP-HR I T SYSTEM IPE STEAP TURNINE SHARE OF THE LOADS 25.7 PERCENT FUEL C 1715UMPT 134 (LRF+UEL/HR-1; 5636.4 THERMAL EFFICIENCY: COSAS: 0.391 STEAN TURBLILE BIL SED INER: 4052.1 . SYSTEM HORSEPONERE 15940.5 GT MURSE POWERINE VITE DIS 11848.5

GT AT SYSTEM HP # 0.32C

18.11.51 15.11.41

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

The Market

GAS THRE INE

PRAKE HIRSEPOWEN: 13790.0, APPROXIMATE CORRESPINDING SHIP SPEED: 19.0 KTS
EXHALST STEPPING ANUMER: 342393.0 FRM/HR (107.6 LBM/SE)

MEAT EXCHANGE GEOMETEY

1946 11 0146 451345 FT. 12-0 FT. 12-1 FT. 12-1 FT. 12-1 FT. 12-1 FT. 12-1 FT.

HEAT TRANSFER SUFFACE THREE TO THE TOTAL DISTRIBUTION TO THE TOTAL THREE TO THE TOTAL THREE THRE

THANSWERSE TUBE : PACING: 3.38 IN.

NUMBER OF TUBES PER ROWS 43.

TUBE LENGTH 12. FT.
OUTSIDE AREA/PASS: 3290.5 SQ.FT.
INSIDE AREA/PASS: 189.0 SQ. FT.

NUMBER OF PASSES: 13 (TOTAL)

NIMBER OF PASSES: 13 (TOTAL)
WEATING SECTION: 5 (HEATING LENGTH= 0.2 FT.)
SUPERHEATING SECTION: 2 (BOILING LENGTH= 3.8 FT.)

MEAT EXCHANGED PEFFORMAICE

GAS TEMP. IN GAS TEMP. DUT FLUID TEMP. IN FLUID TEMP. OUT REYNOLDS NUMBER (AVG.) SECTION

PEATING 730.9 426.1 200.0 486.3 486.3 486.3 641.3

187362.6

STEAM PRESSURES 600.C PSIA (SATURATION FEMPERATURE + 486.3 F)

STEAM FLOW AATE: JBUTO.9 LBMAIR. GAS-SIJE PRESSURE JRCP: 4.4 IN H20

PINCE PARITE 44.6 F

SYSTEP FERECAMANCE

GT HOF SEPTIMER (REVISED) 1 13494.2

STEAP THEN INE HONSEPOWER: 4279-2.0
TOTAL SYSTEM HORSEPOWER: 17772-1

CONDENSER PRESSURE: 4.08 IN HG STEATURN NE EFFICIENCY: 0.85 FW HEATER PRESSURE: 15.0 PSIA IN OFFICE: 18400 BIULEM

ASSUMED SYSTEM CHARACTERISTICS:

STEAP TURBLINE SHARE OF THE LOADS: 24.1 PERCENT SPECIFIC FIEL COASSMPTION (LB4-FJEL/PP-HB): G1 CALVI 0.45 COGAS: 0.347 G7 AT SYSTEM HP: 0.423 FIREL C. 1451 1PT INT ILRA-FUEL /IR . 11 G. 2 GT AT SYSTEM HP 1 7525.7

THEMML EFF TCTENCY: CHGAS: 0.399 GT AT SYSTEM MP: 0.327

MASTE HEAT RECOVERY UNIT OFF-DESIGN RUN

645 Tune lue

DING SHIP SPEED: 20.0 KTS .AM/SEC!	NLMBER OF RCUS PER PASS: 1. NIMBER OF TUBES PER ROW: 43. TUBE LENGTH 12. FT.	OUTSIDE AREA/PASS: 3290.5 SQ.FT. INSIDE AREA/PASS: 189.0 SQ. FT. FRCNTAL AREA: 144.8 SQ. FT.	NUPREM OF PASSES: 13 (TOTAL) HEATING SECTION: 6 (HEATING LENGTH= 1.5 FT.) SUPERHEATING SECTION: 2 (BOILING LENGTH= 4.3 FT.)
BRAME HONSEPOLER: 16421.0, APPROXIMATE CORRESPONDING SHIP SPEED: 20.0 KTS EXHALST GAS TEMPERATURE: 849.0 F FM/HR (113.2 LAM/SEC) EXHALST GAS FLOM RATE: 4.07589.0 LAM/HR (113.2 LAM/SEC) HEAT EXCHANGEN GEOMETRY	CVEMAL CIMENSINS: 12.0 FT. WITH: 12.1 FT. FT. FT.	PEAT TRANSFER SUFFICE 1.5 IN. 11.51.0 TOUR DIAMETER: 1.5 IN. 11.51.1 TOUR DIAMETER: 1.5 IN. 11.51.1 TOUR DIAMETER: SEGNENTED 11.1 SECTION:	FIN THENE'SS! 0.036 IN. TRANSVERSE TUBE PACING: 3.34 IN. LCNGIT.JGIAAL TUBE SPACING: 2.92 IN.

	(AVG.)					
	REYITOLOS NUMBER	25259.9				
	GAS TEMP. IN GAS TEMP. OUT FLUID TEMP. IN FLUID TEMP. JUT REVISILDS NUMBER (AVG.)	4 de 6.3				
	2		-			
	LUID TEMP.	200.0 480.6 486.3	STEAM PRESSURE: 630.0 PEIA (SATURATION TEMPERATURE + 486.3 F)			
	_		TURE-			
	3	7-0	IP ER A			
i	TEM	534.1	N TE			
1	CAS		ATIO		Ü	
	Z		SATU		IN HZ	
	E MP.	534 -1 742 -8 848 -4	4	1467	6.	
	CAS	×-=	2	6.2		
		9.	630.0	3750	ORC	53.5 F
MEAT EXCHANGE FEFFORMETCE	=	S. Jo Carest 1:16	YE :	STEAM FLOA AATE: 37562.9 LAMANA.	GAS-SIDE PRESSURE DRCP: 4.9 IN HZC	
	SE [] 35	115	ESSU	* *	PRE	PINCE PAINTS
1000	7		AM PR	AM FL	- \$1DE	C+ 13
EXC			STE	STE	645	4
HEA						

CONCENSER PRESSURE: 4.00 IN. HG STEAM JURGINE EFFICIENCY: 0.085 LM FEATER PRESSURE: 15.0 PSIA LHV OF FUEL: 18430 BTU/LBM ASSUMED SYSTEM CHAPACTERISTICS: GT AT SYSTEM HP: 8268.2 SPECIFIC FUEL CINSUMPTION (LAM-FUEL/MP-HA): CALY: 0.445 CACK: 0.336 GT AT SYSTEM HP: 0.395 GT AT SYSTEM HP : 0.35C STEAP TURBINE SHARE OF THE LOAD: 23.4 PERCENT FIRE C. CALV: 0.997.8 CICAS: 6997.8
THE OHLL FFF I TENTY COGES: 0.414 STEAM FUTHINE HIPSEPINERS 4902-1 TOTAL SYSTEM HIRSEPOWER: 20955.9 GT MCK SEFCKERIREVISEDI: 16053.9 SYSTEM FERFUP IN CE

36.11.21 21.11.50

WASTE HEAT RECEVERY UNIT CFF-LESIGN RUN

The State of the

GAS TURITAE

tidet tifitalifer: 2000000 APPAINTE CHRRESPHAING SHIP SPEED: 21.5 famils is fempleating: 807.0 fbm/H (122.4 LEN/SEC)

CVENTLE LIMENSTONS: TENTE LEGISTER LEGI Pfell tachation sentery

NETHER OF POMS FER FASS:

HEAT LASH SHE COPFICE TEACH INSTITUTE TO SHE INSTITUTE TO

LUNGITLE TOUR SECTIONS 2.92 IN. PARISHEYET ILVE SPACINGS 3.34 IN.

(PFILING LENGTHE 5.6 FT.) CLTSILE ANTONISS: 3290.5 SO.FT. 169.0 50. FT. NUMERA OF PASSES: 13 (TCTAL)
HEATING SECTION: 5
501L INC SECTION: 5
50 EPHEATING SECTION: 2 FPINIAL AREA: 144.6 SC. FT. NIMBER OF TURES FEF FORE TLBE LENGTH 12. FT. INSIDE PREEZE ASS:

HEAT EACHSHIER SEAF INPANCE

545 TEMP. IN GAS TEMP. DUT FLUID TEMF. IN FILLE TEMF. DUT REVICEDS NUMBER (AVG.) STITM ATESSULE: 630.0 PSIA (SATURATION TEMPERATURE: 486.3 F) 5.7 IN H2C STERY FIEL 247 E: +5357.0 LB"/IR. 615-513c 2: 65567t 3RCP: FIRCE FC117: 60.3 F PEATING CALLING 36.717.1

26586 F.2

SYSTEM PERITURGICE

CGNDENSER PRESSERE: 4.03 IN HG SFEAT FURTHE LFFICIENTY J. 55 FA HE FLEET 1843C STEVEN ASSUMED SYSTEM CHARACTERISTICS: GT AT SYSTEM HP: 1132.8 STITLY HEAVILL SHARE OF THE LEAST 23.2 PERCENT FIEL CINCINSTAL (LP4-FIEL/P2-): 4178-4 STEAD THEIR MANSEPONES: 5485.3 FUTAL SESTEM PUTSCHONET 25405.9 4f H 14 572 13F3 LAT VISCOIT 19520.6

GT AT SYSTEM HP: 3.102

Ch635: 1.430

Cal Cal Child IS St.

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